

INFLUENCE OF FLUX AND COMPOSITION ON LOOP'S NATURE IN NICKEL DURING ION IRRADIATION

Lisa Lefort¹, Brigitte Décamps², Guilhem Sagnes¹, Thomas Jourdan¹, Marie Loyer-Prost³

¹Université Paris-Saclay, CEA, Service de Recherche en Corrosion et Comportement des Matériaux, SRMP, 91191 Gif-Sur-Yvette

²Laboratoire de Physique des 2 infinis Irène Joliot-Curie (IJCLab), CNRS/IN2P3, Université Paris-Saclay, 91400 Orsay, France

³Université Paris-Saclay, CEA, Service de Recherche en Matériaux et procédés Avancés, 91191 Gif-Sur-Yvette

Industrial context

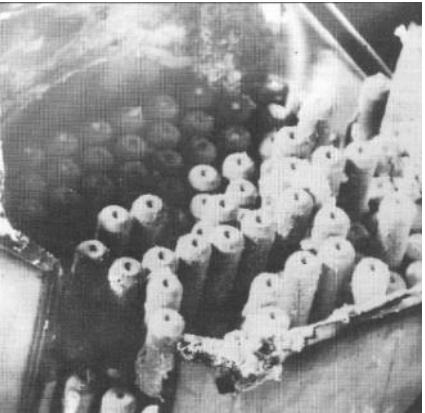
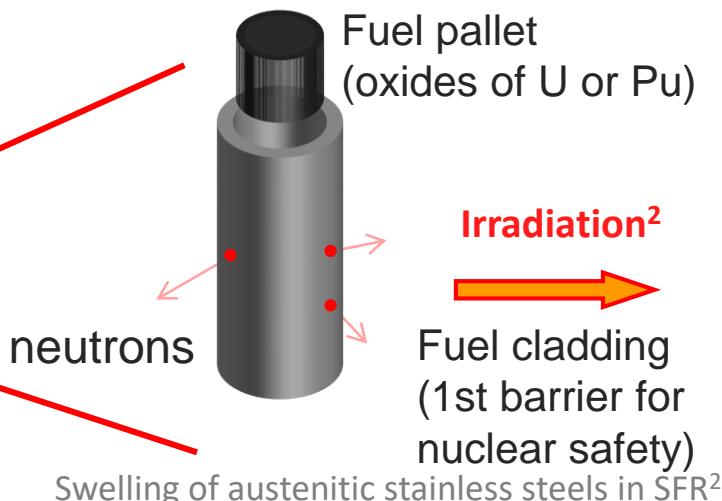
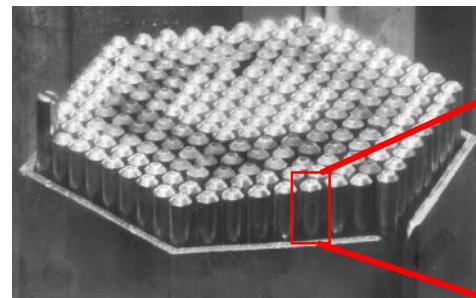
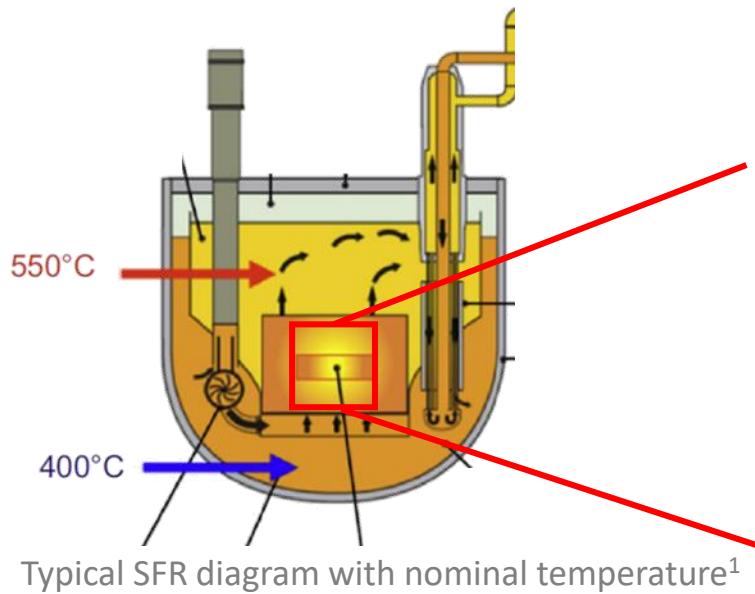
Development of next generation reactors (Sodium-cooled Fast Reactor, SFR-Gen IV)

Huge challenge for fuel cladding materials = harsh environmental conditions

- High irradiation > 100 dpa (displacement per atom)
- High temperature 450-600°C

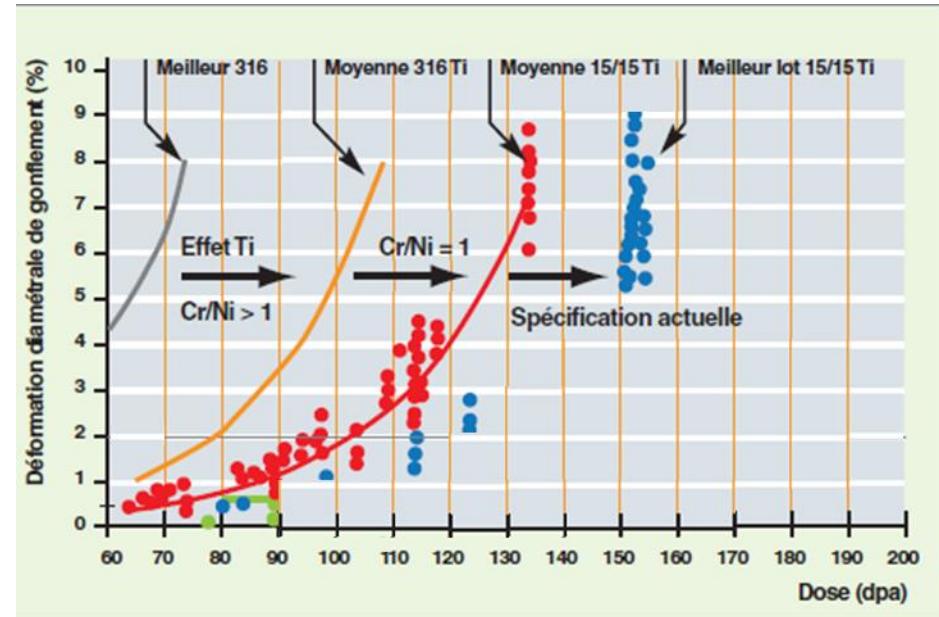
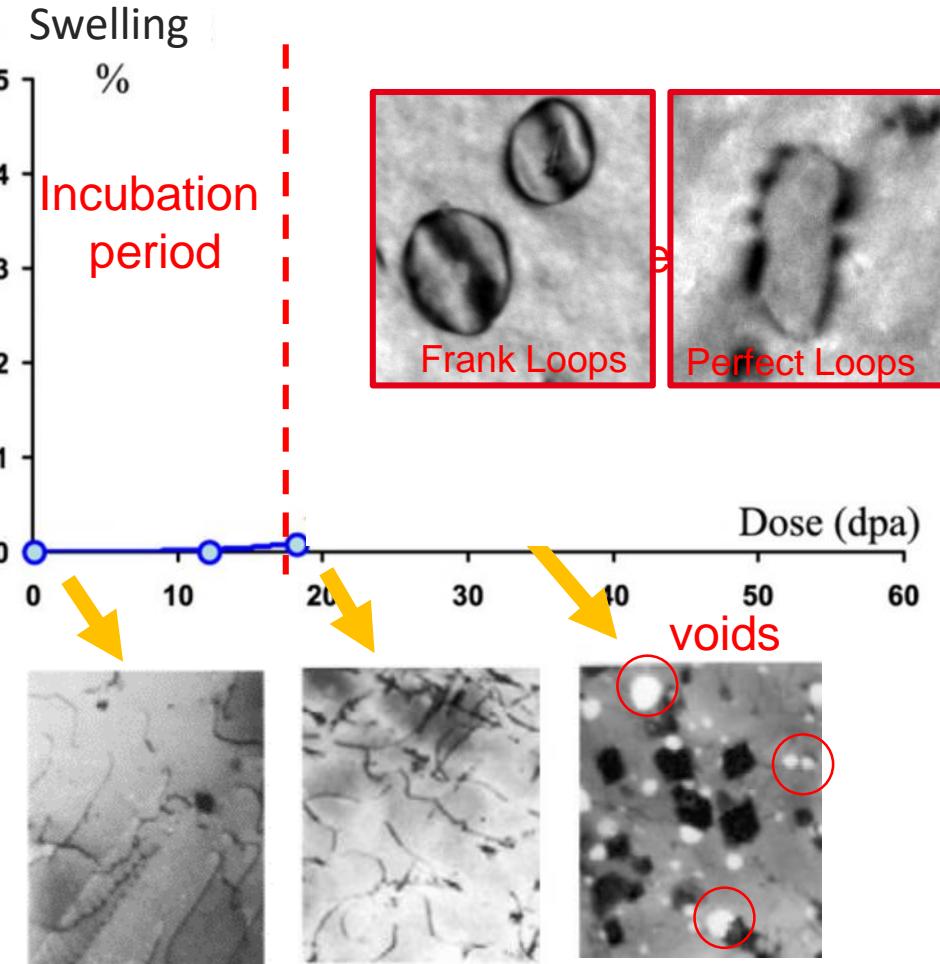
Austenitic Materials

- Foreseen as the first candidate for fuel cladding of SFR-Gen IV
- Well-known major issue : 3D volume extension => irradiation-induced **void swelling**



Radiation-induced void swelling in austenitic steels

Swelling of 316 ASS in function of irradiation dose at 600°C in Phénix¹.



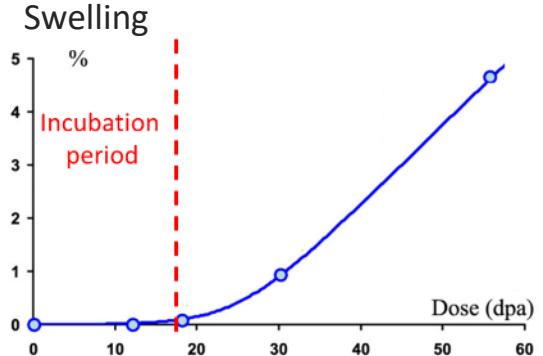
Swelling of different cladding candidates of Gen-IV reactors³

➤ Influence of composition ?

Approach

1. Objective

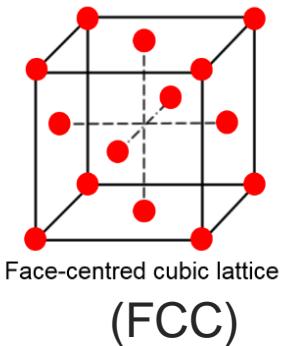
Better understand the mechanisms governing the early-stage irradiation behavior of austenitic structure (FCC) structure



2. Approach

Simplification of studied materials

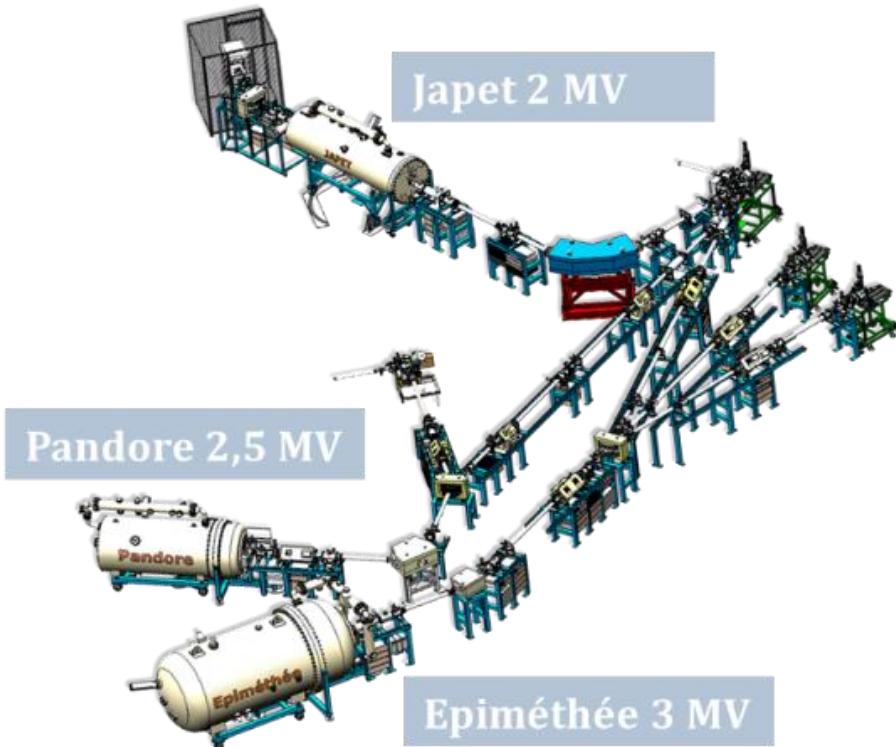
Ni and nickel alloys (Ni0,8Ti)
→ FCC structure



Simplification of experiment conditions

- Ion irradiations on JANNuS platforms
- Good control of various flux and irradiation temperatures

→ Influence of flux ?

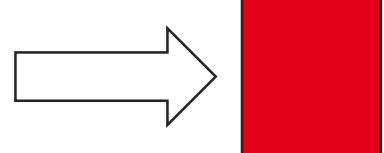
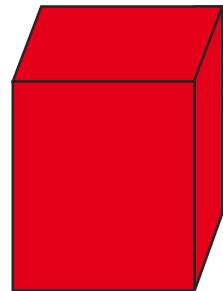


Approach – sample preparation

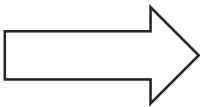
Ni - Prepared at Ecole des Mines St. Etienne

Element	Wt%(ppm)	C	S	O	N	Ti/Cr	Ni
Ni		8	2	3	2	\	Bal.

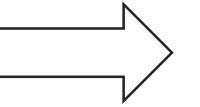
Ni_{0,8}Ti (99,2% Ni + 0,8% Ti) - Prepared in CEA Saclay



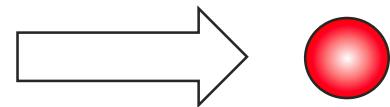
Mechanical polishing
100 µm



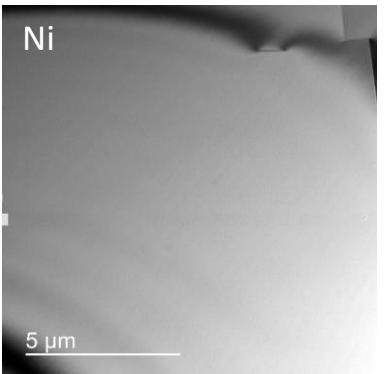
3 mm disc
punching



Heat treatment
(annealing 1000°C)



Electrolytic
polishing



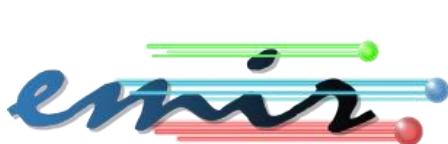
Microstructure characterization
before irradiation

Irradiations

Observations by TEM,
Thin foil characterization



Approach – irradiations



université
PARIS-SACLAY

iJC Lab
Irène Joliot-Curie
Laboratoire de Physique
des 2 Infinis

mosaic

cnrs IN2P3
dépasser les frontières
Les deux infinis



JANNuS facilities Saclay and Orsay

Material	Platform	Temperature	Flux
Ni	JANNuS Orsay ARAMIS Ni2+ 2MeV	450°C	High 3.10-4 dpa/s
Ni	JANNuS Saclay Japet Ni2+ 5MeV	450°C	Intermediate 6.10-5 dpa/s
Ni	JANNuS Saclay Epiméthée Fe9+ 22,5MeV	450°C	Low 6,7.10-6 dpa/s
Ni 0,8 Ti	JANNuS Orsay ARAMIS Ni2+ 2MeV	450°C 510°C ; 560°C	High 3,1-3,5.10-4 dpa/s

Iradina:

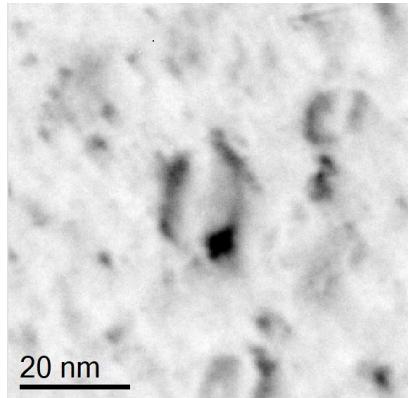
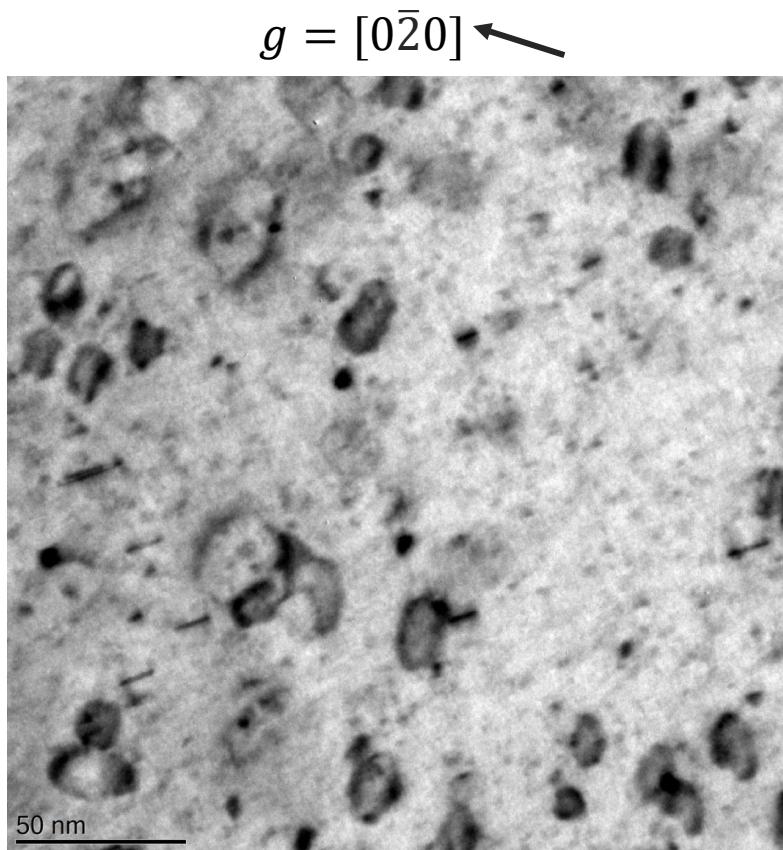
- SRIM like, quick calculation,
 $E_{displacement} = 40 \text{ eV}$



1 ■ Influence of flux

High flux

Ions = Ni²⁺ 2MeV (JANNuS Orsay)
Ion flux = 4e11 ions/cm²/s $\Leftrightarrow \mathbf{G = 3.10^{-4} \text{ dpa/s}}$
T = 450°C
Dose = 0.18 dpa



→ Vacancy type loops





High flux

- At steady state, **standard rate theory** predicts a radius variation of a vacancy loop :

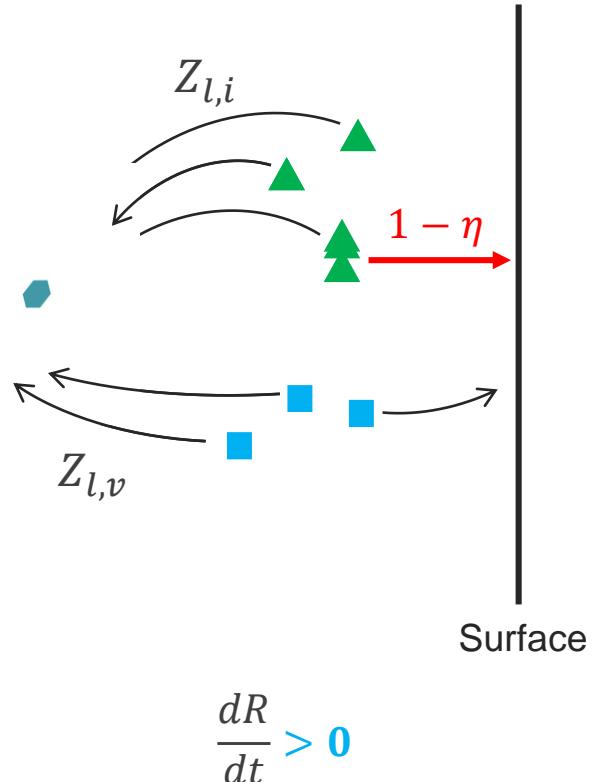
$$\frac{dR}{dt} = \frac{\Omega}{b} \left(Z_{l,v} - Z_{l,i} \frac{k_v^2}{k_i^2} \right) D_v C_v < 0$$

- Vacancy-type loops should not grow**

- Introduction of production bias $1 - \eta$ (surface effect)

$$\frac{dR}{dt} = \boxed{\frac{\Omega}{b} \left(Z_{l,v} - Z_{l,i} \frac{k_v^2}{k_i^2} \right) D_v C_v} + \boxed{\frac{\Omega Z_{l,i}}{b k_i^2} G(1 - \eta)}$$

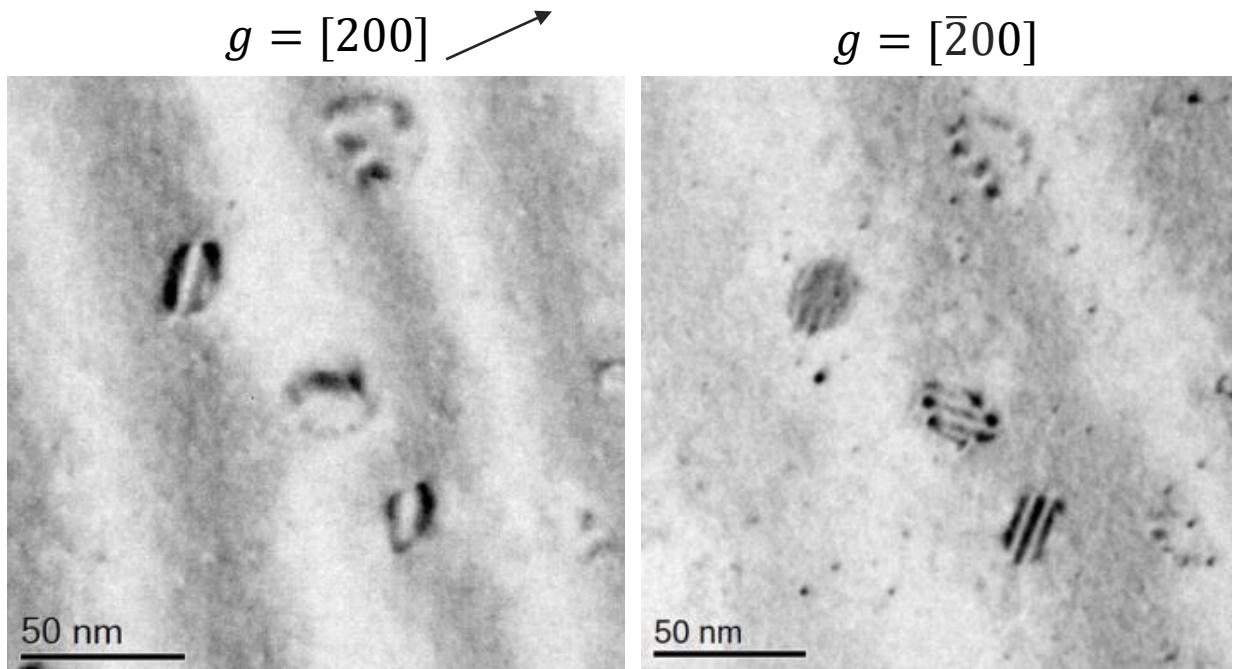
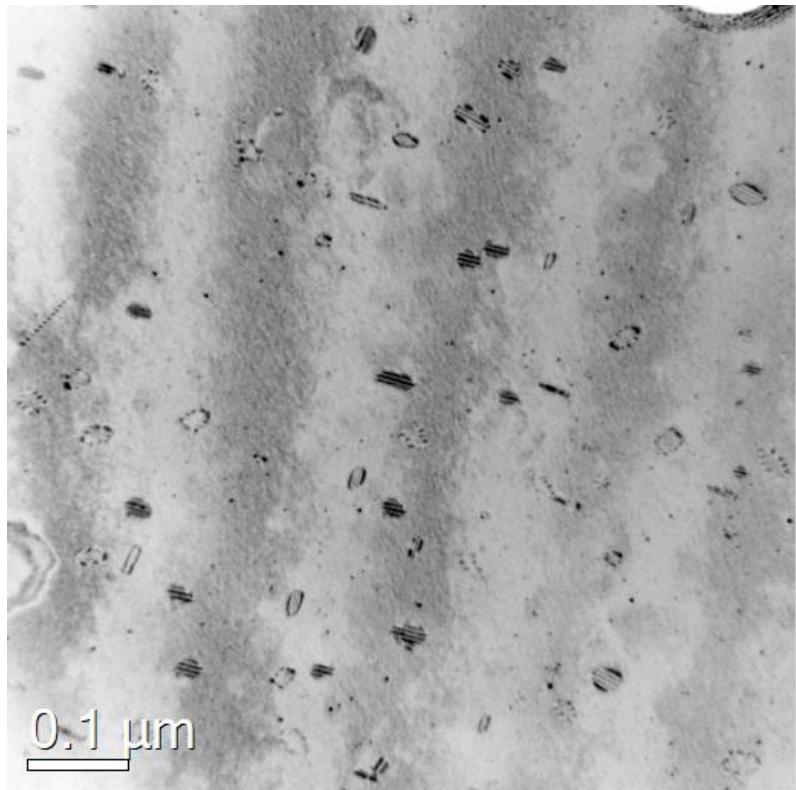
Dislocation bias term < 0 Production bias term > 0



K. Ma, B. Décamps, T. Jourdan, M. Loyer-Prost & al., Acta Materialia 212 (2021)*

Low flux

Ions = Fe⁹⁺ 22,5 MeV (JANNuS Saclay)
Ion flux = 7.93e10 ions/cm²/s $\Leftrightarrow \mathbf{G = 6.7.10^{-6} \text{ dpa/s}}$
T = 450°C
Dose = 0.06 dpa



→ Interstitial type loops

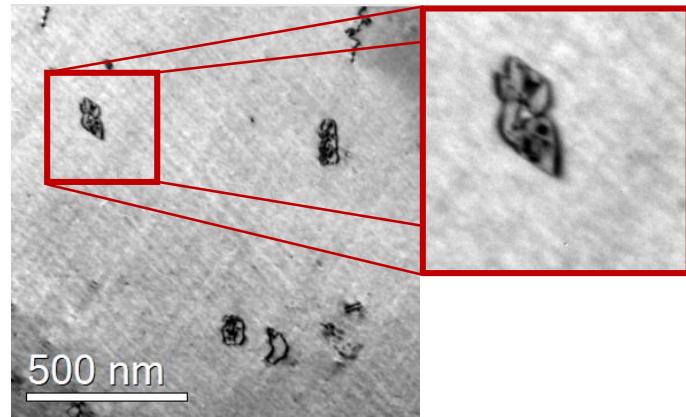
Intermediate flux

Ions = Ni²⁺ 5MeV (JANNuS Saclay)

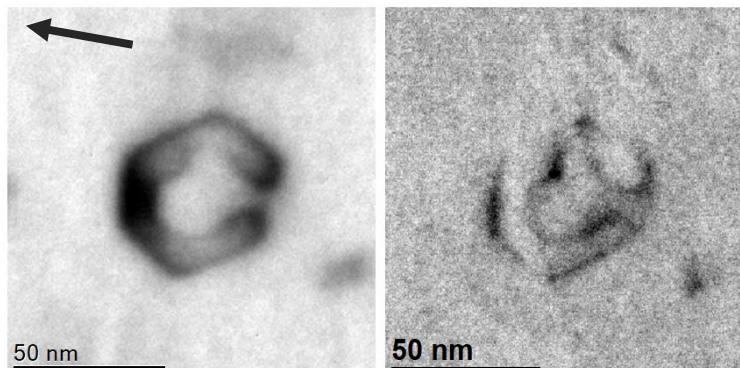
Ion flux = 2.2e11 ions/cm²/s \Leftrightarrow **G = 6.10⁻⁵ dpa/s**

T = 450°C

Dose = 0.06 dpa

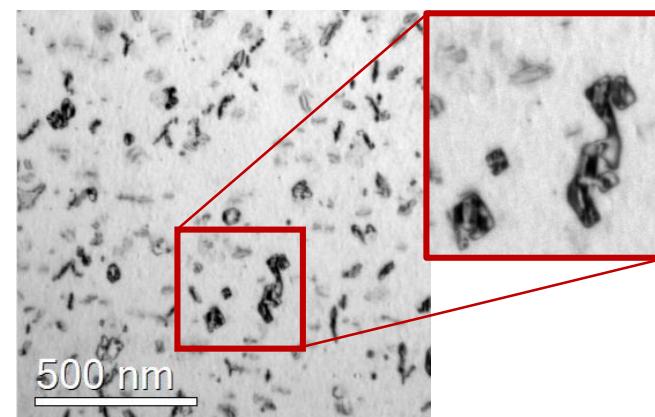


$Z = [121], g = [1\bar{1}1]$

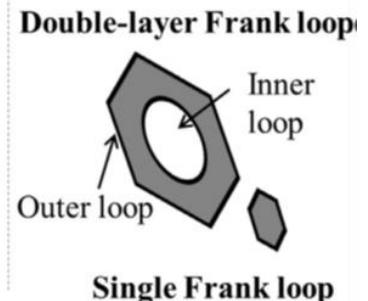
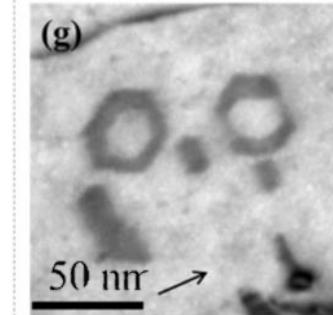


→ Vacancy type loop

Dose = 0.7 dpa

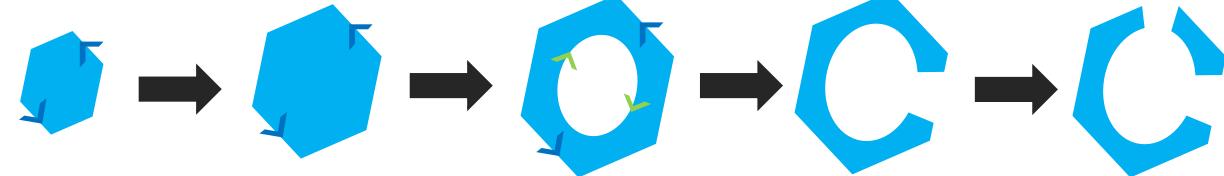


Zone axis [112]
 $g = 111$



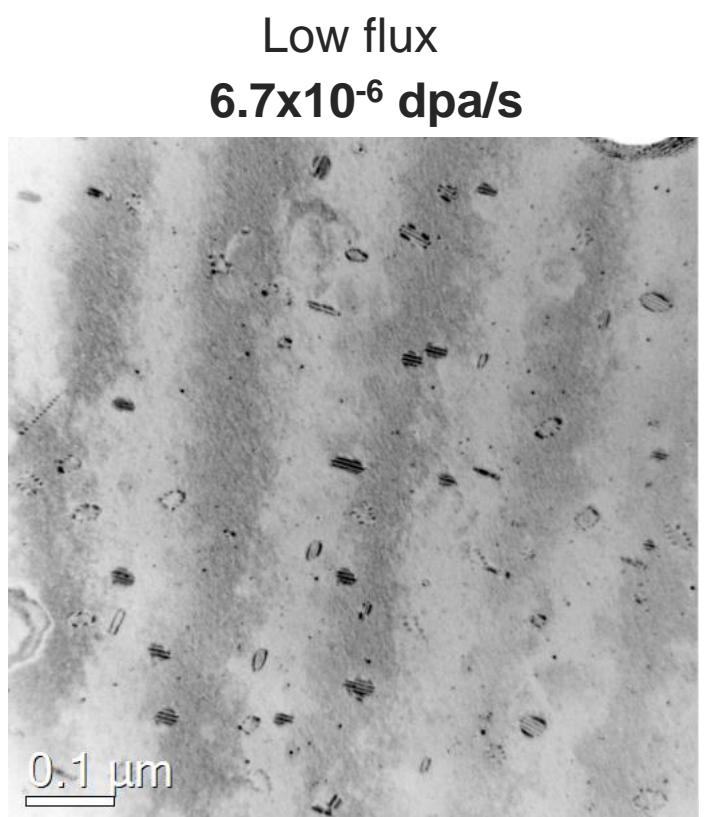
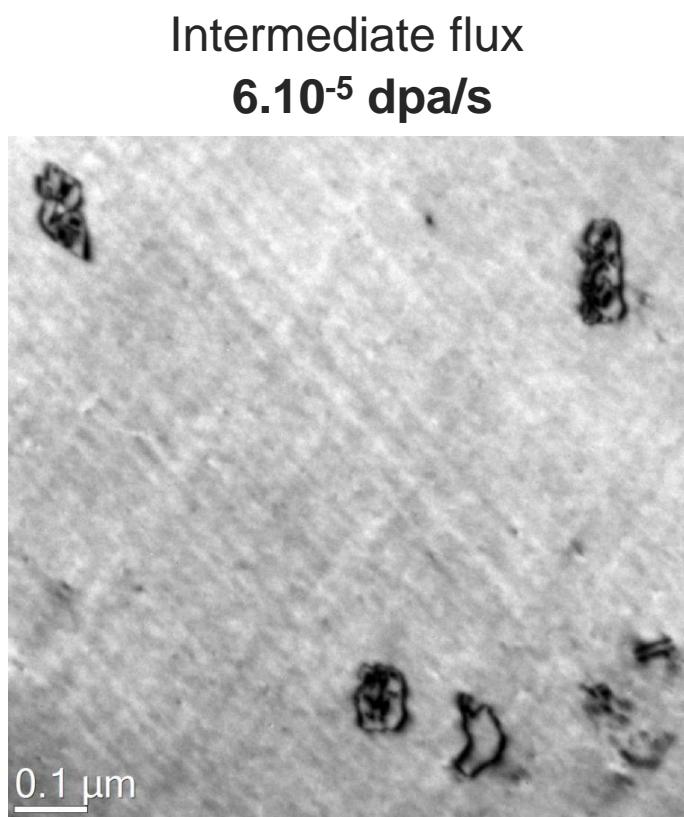
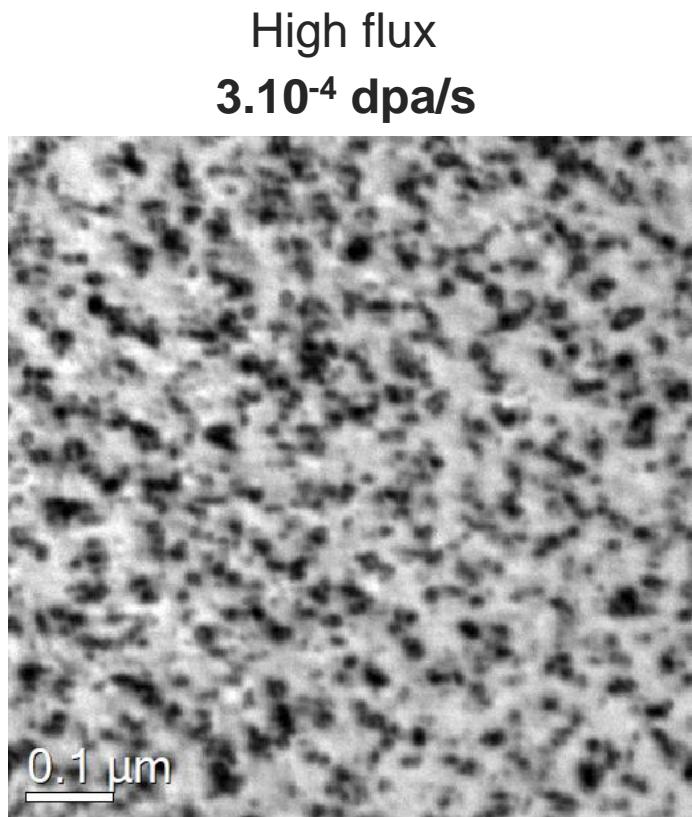
K. Ma & al., Inversion of dislocation loop nature driven by cluster migration in self-ion irradiated nickel. Scripta Materialia 208 (2022).

$$b = \frac{1}{3}[1\bar{1}\bar{1}]$$



To sum up

0.06 dpa, 450°C



Vacancy type

Interstitial type



2 ■ Influence of composition

Influence of composition

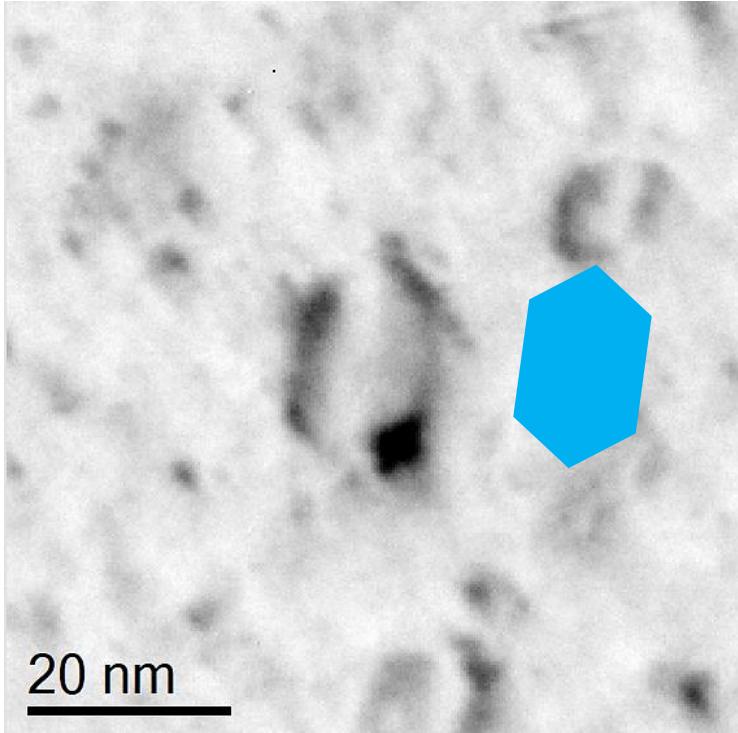
Ions = Ni²⁺ 2MeV (JANNuS Orsay)

Ion flux = 4e11 ions/cm²/s \Leftrightarrow G = 3.10⁻⁴ dpa/s

T = 450°C

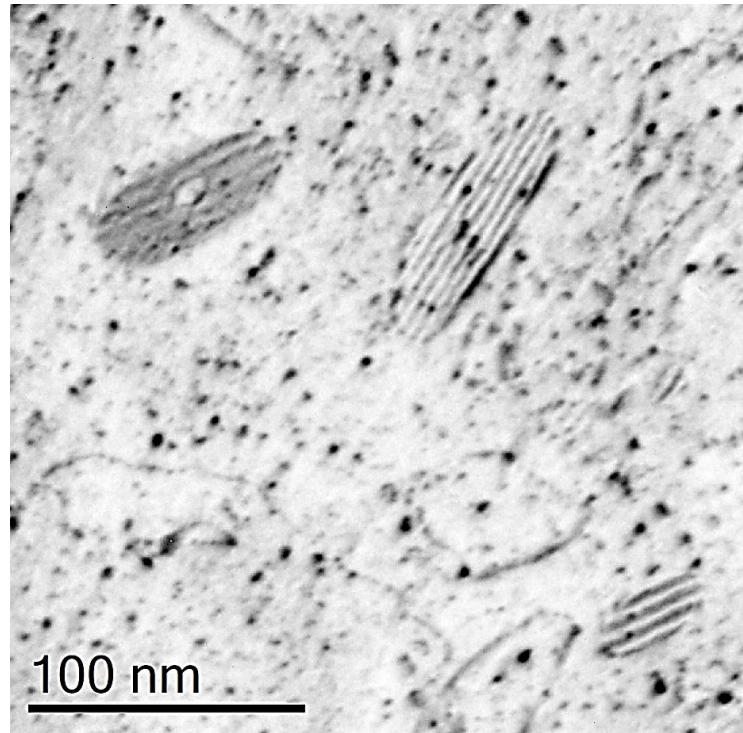
Ni

0,18 dpa



Ni0,8Ti

0,66 dpa



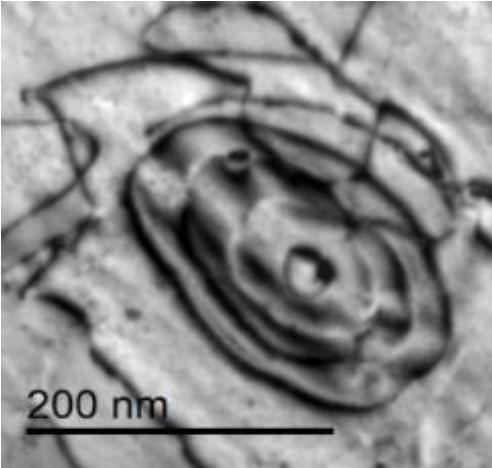
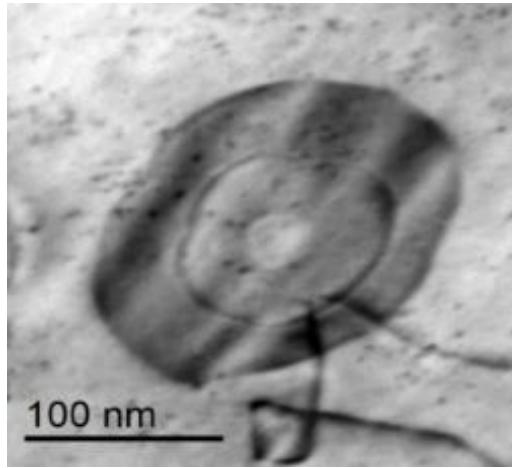
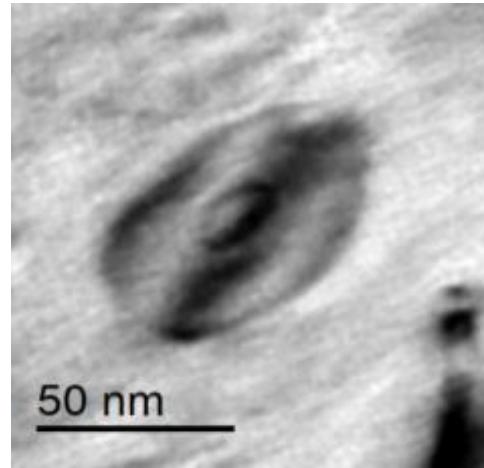
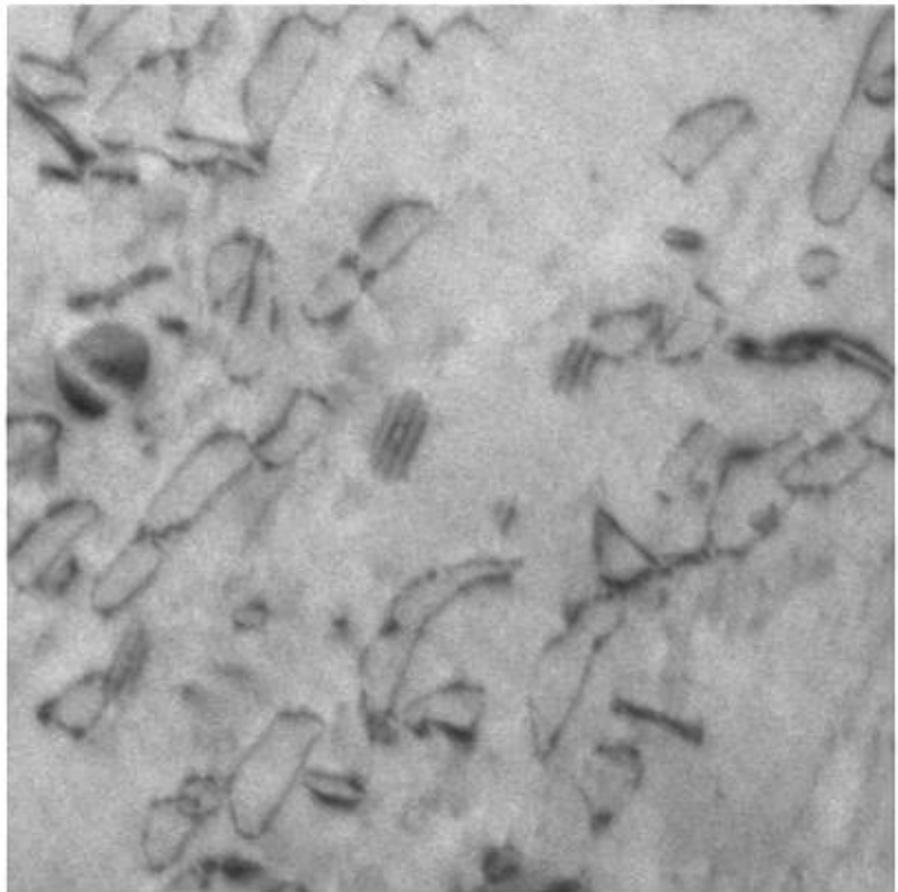
→ Vacancy type loops

→ Interstitial type loops

→ 1- η lower in Ni0,8Ti

Multi-layer loops

560 °C

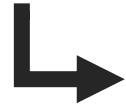


→ Very close to each other

→ Same Burgers

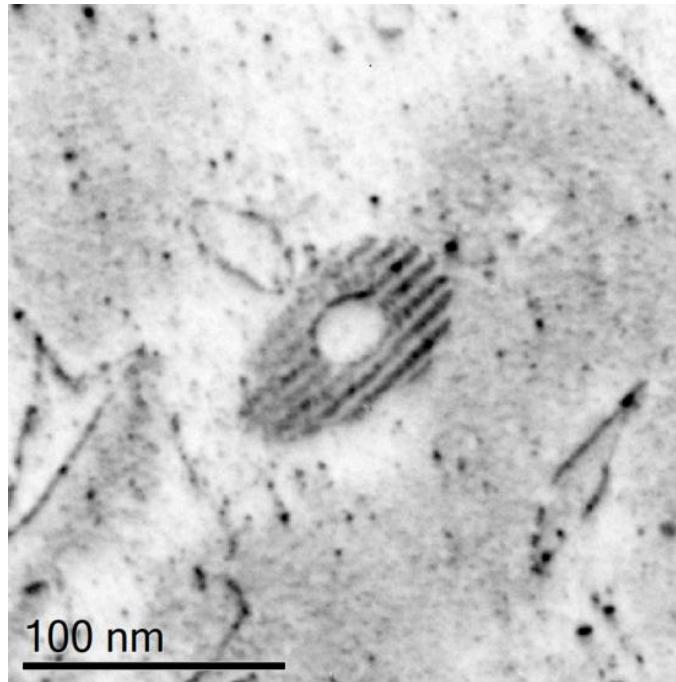


Frank loop with perfect crystal inside

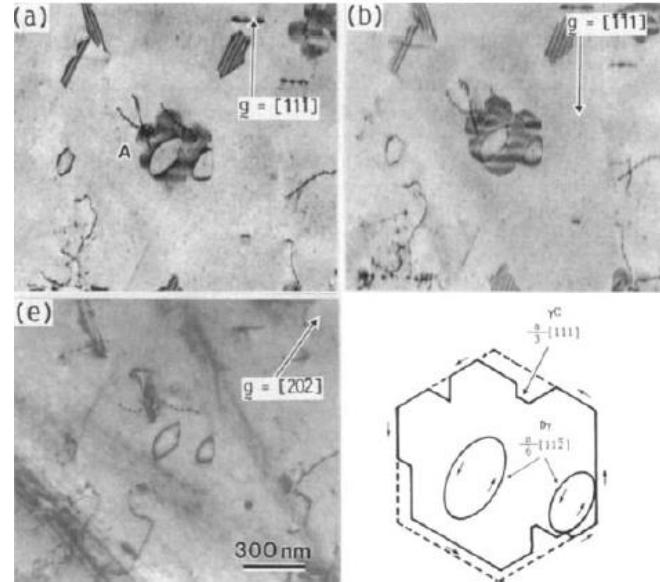


faulted/unfaulted

510°C

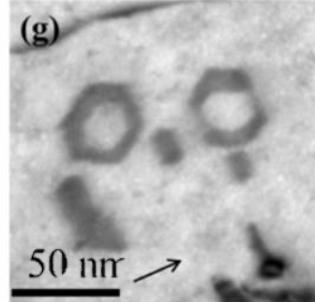


→ Shockley partial ?

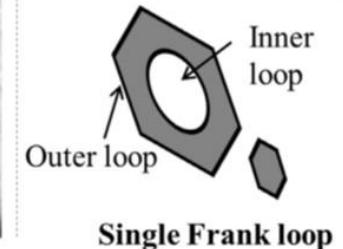


Suzuki et al., Philosophical Magazine A (1992) 1309

Zone axis [112]
 $g = 111$



Double-layer Frank loop

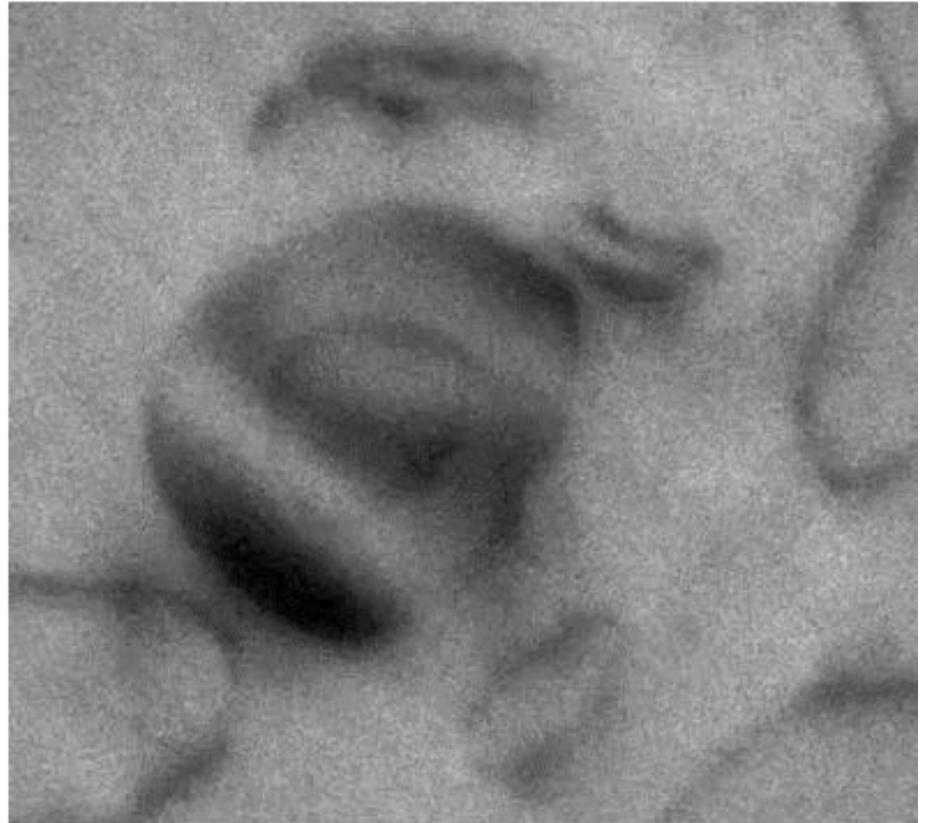


K. Ma & al., Scripta Materialia 208 (2022).

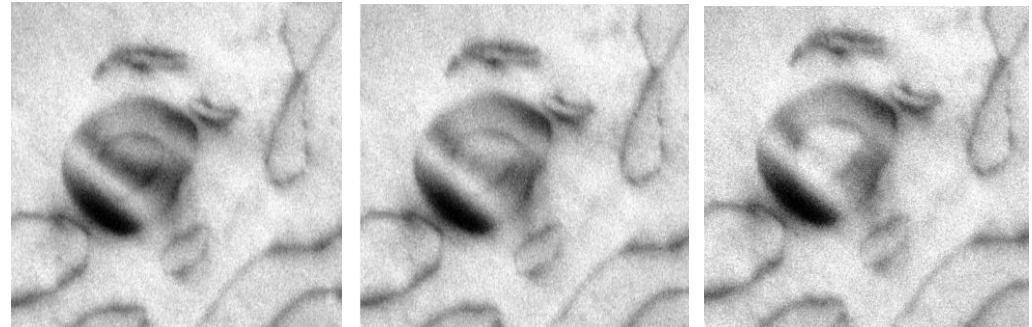
25/09/2024

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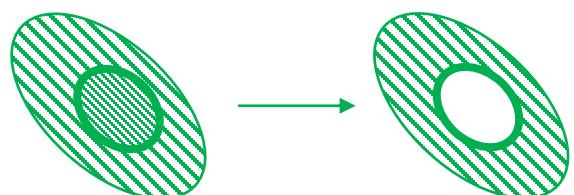
Frank loop with perfect crystal inside



[020]



$\Delta t = 0,25\text{s}$

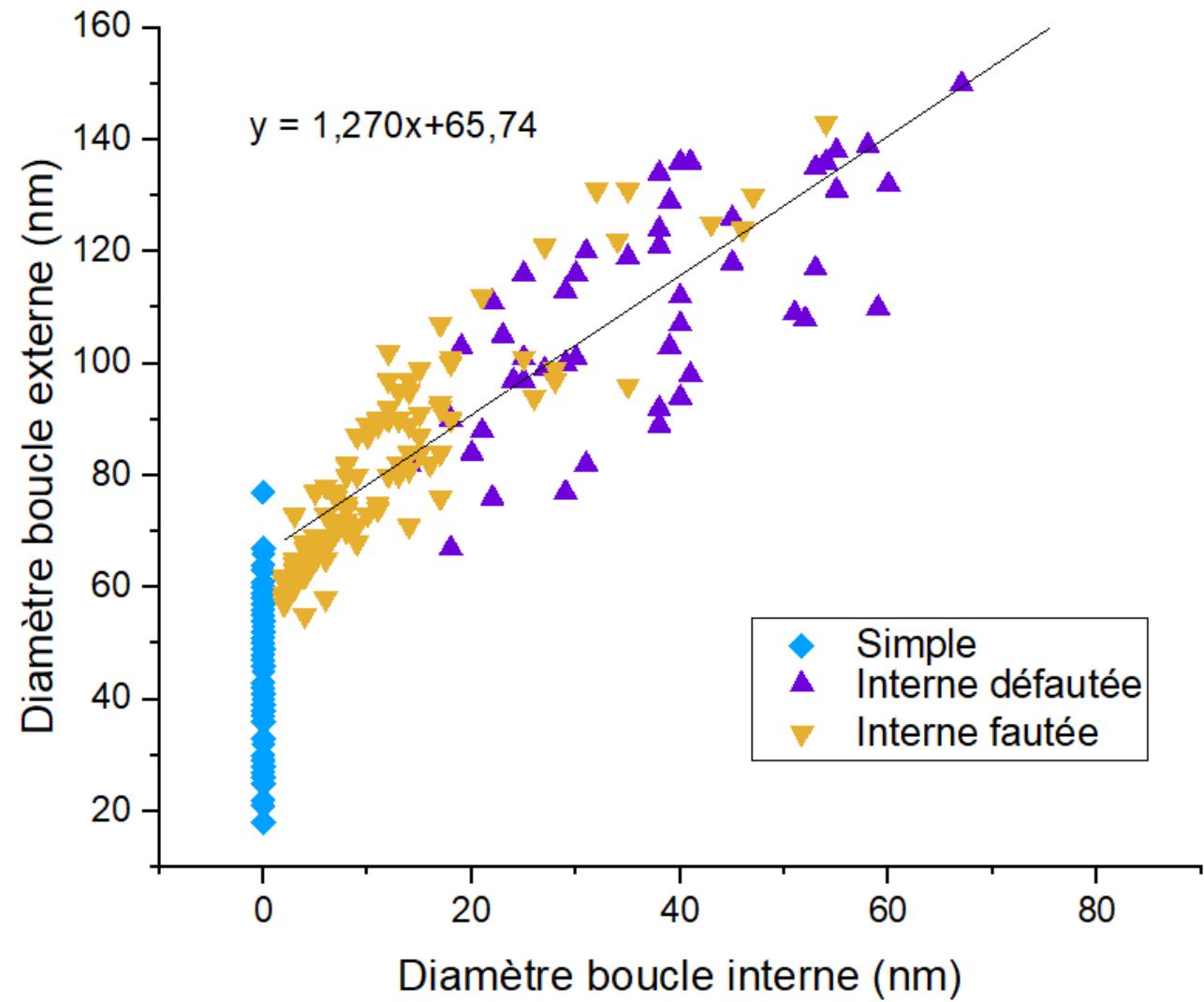


→ Shockley partial ?

→ Inner vacancy loop ?



Frank loop with perfect crystal inside



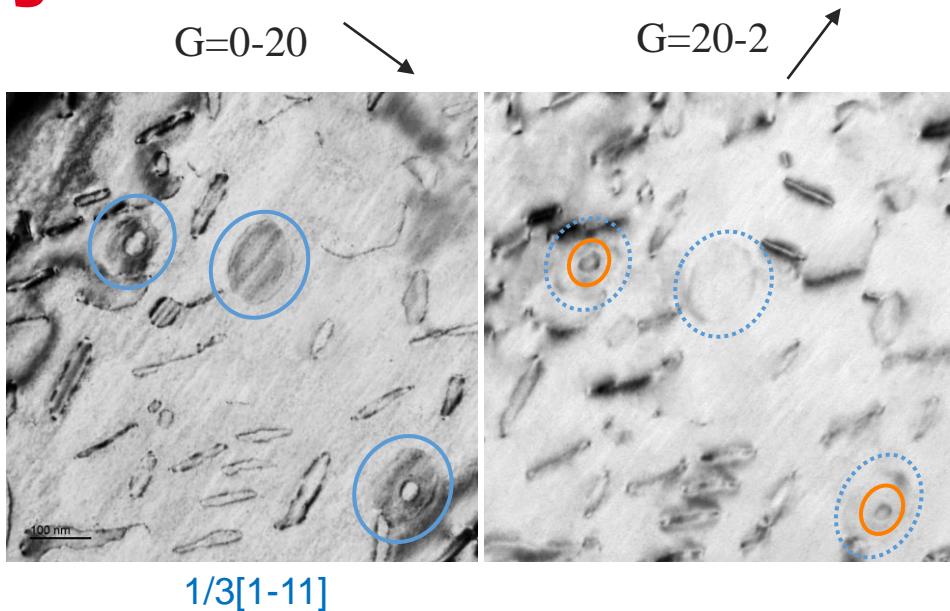


Frank loop with perfect crystal inside

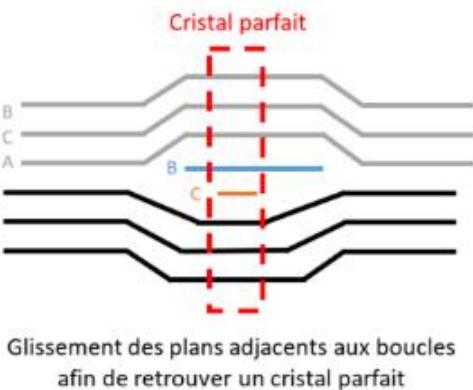
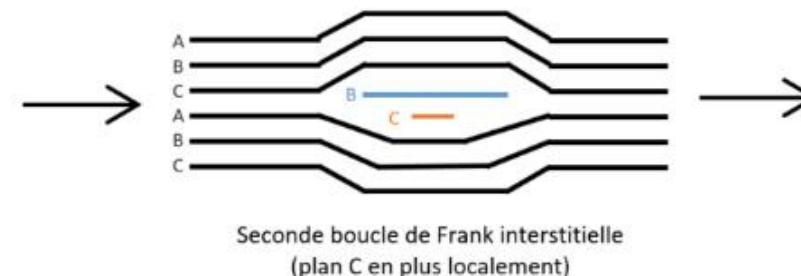
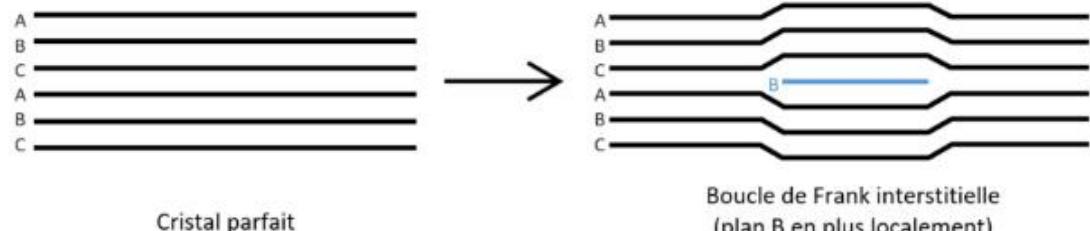
Visibility of external and internal loops (560°C)

→ internal loop Burger vector = $1/a[1-12]$

$$2/3[1-11] + 1/6[-112] = \frac{1}{2}[1-12]$$



Mechanism of internal loop unfaulting by Shockley partial

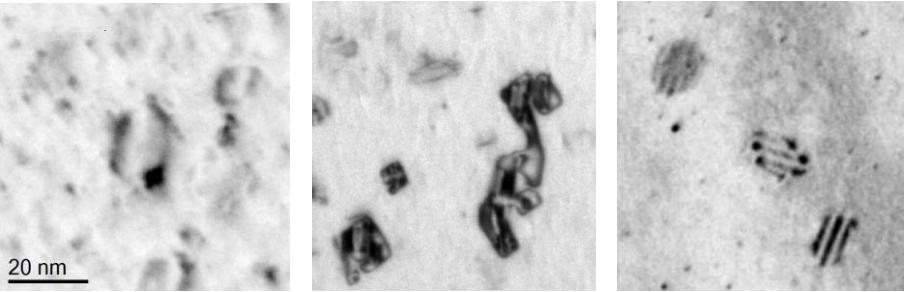




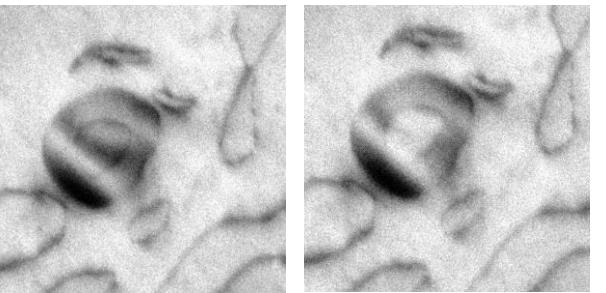
3. Conclusion

Conclusion

- Flux variation can change loop's nature
- Complex microstructure for intermediate flux
- Relation between shape and nature's loop for Frank loop



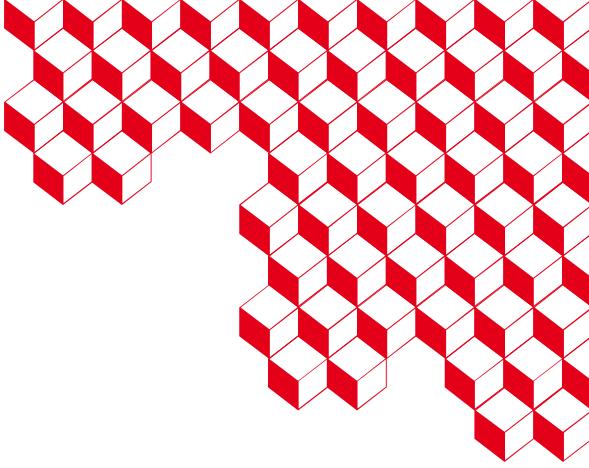
- Titanium significantly reduces interstitial losses at surfaces
- Multiple loops can unfault partially, becoming faulted/unfaulted





Prospects

- Further study on multiple loops
- Removal of temporal variation of the flux : effect of defocused beam



Thank you

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