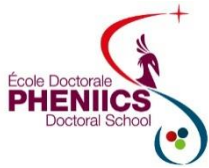


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# *Related Technologies :*

## *1) Radiofrequency*

## *and*

## *2) cryogenics and superconductivity*

Akira Miyazaki

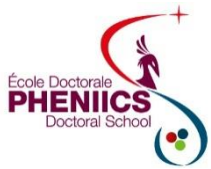
Laboratoire de Physique des 2 infinis Irène Joliot-Curie

Pôle Physique des Accélérateurs

[akira.miyazaki@ijclab.in2p3.fr](mailto:akira.miyazaki@ijclab.in2p3.fr)

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# *Part 1: Radiofrequency Technologies for Particle Accelerators*

Akira Miyazaki

Laboratoire de Physique des 2 infinis Irène Joliot-Curie  
Pôle Physique des Accélérateurs  
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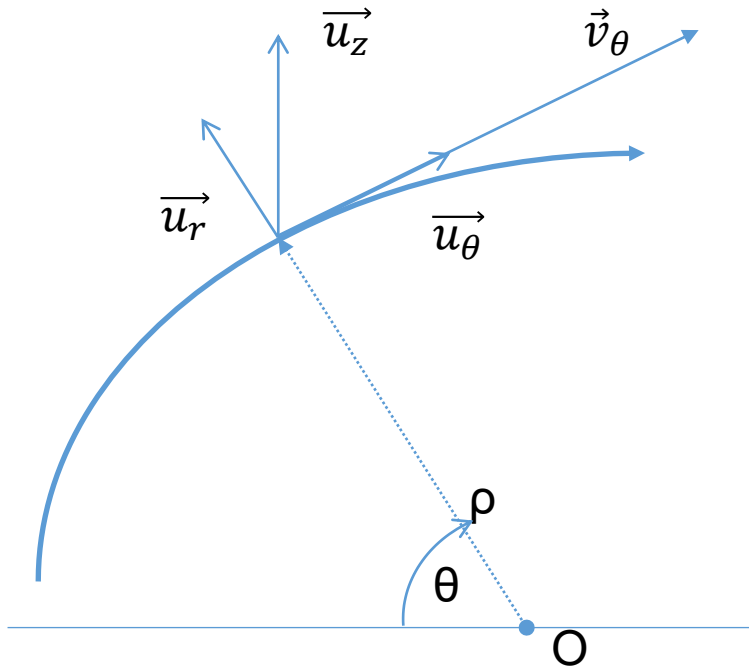
- Introduction: from DC to RF accelerator (15 min)
- Fundamental of RF (15 min)
- A simple example of an RF cavity (15 min)
- Break (10 min)
- RF around cavities (10 min)
- Wake field (10 min)
- Various shapes of RF cavities (10 min)
- Conclusion



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# Lorentz force



Assuming  $\vec{E} \rightarrow E_\theta$  and  $\vec{B} \rightarrow B_z$

$$\text{Lorentz Force: } \frac{d\vec{p}}{dt} = e\vec{E} + e\vec{v} \times \vec{B}$$

By developing in the coordinate system:

$$\frac{d(mv_\theta)}{dt} \cdot \vec{u}_\theta - m \frac{v_\theta^2}{\rho} \cdot \vec{u}_r = eE_\theta \cdot \vec{u}_\theta + ev_\theta B_z \cdot \vec{u}_r$$

Then, by identification on unit vectors:

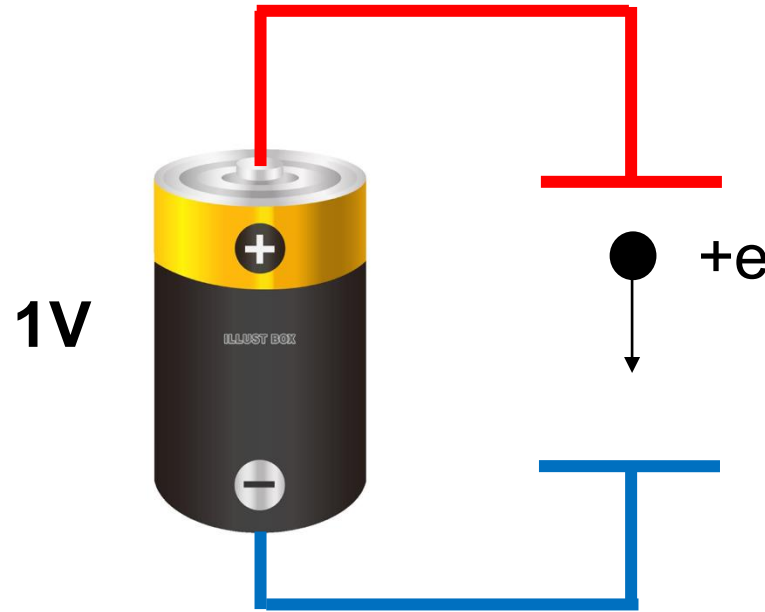
$$\begin{aligned} \frac{dp_\theta}{dt} &= eE_\theta \\ \frac{p_\theta}{e} &= \rho B_z \end{aligned}$$

In conventional particle accelerators, we need

1. **Magnetic fields** to bend the trajectory (magnets)
2. **Electric fields** to accelerate and decelerate the beam (cavities)



# How to accelerate charged particle by DC

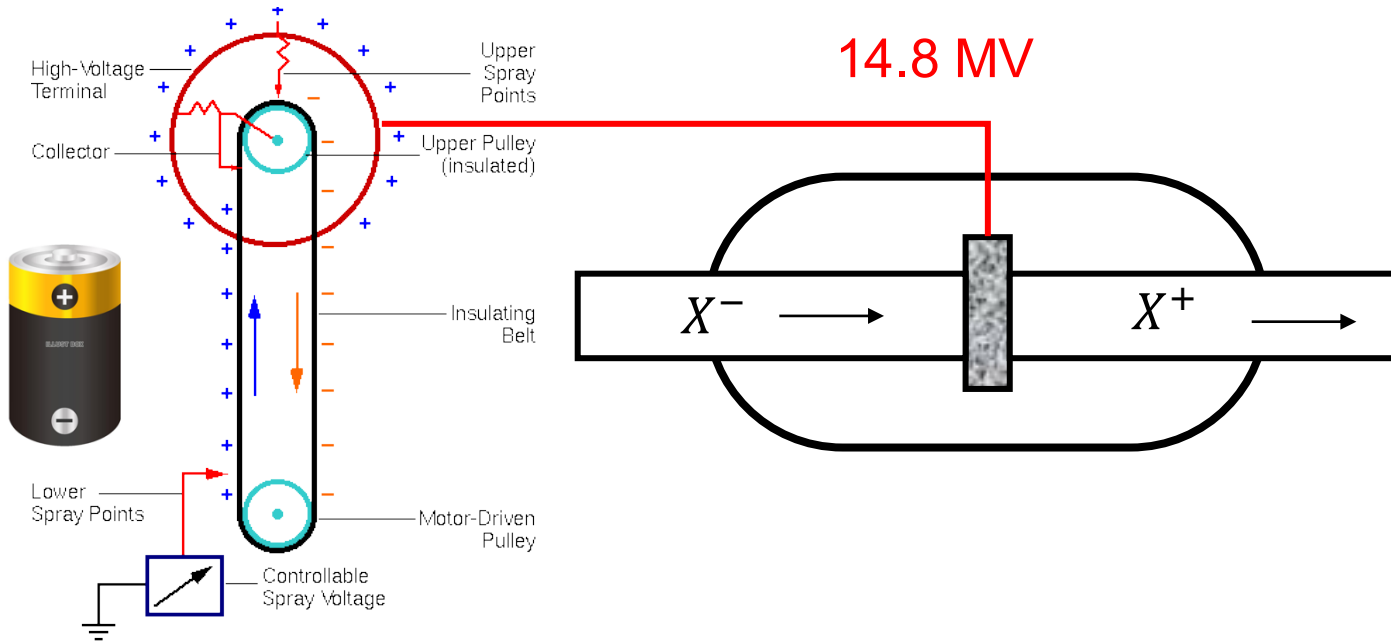


Electron's rest mass  
in the natural unit  
 $m(c^2) = 511 \text{ keV}$

Kinetic energy of a charge  $+e$  ( $1.6 \times 10^{-19} \text{C}$ ) accelerated by 1 V

$$E = 1 \text{ eV}$$

Modern science  $\gg$  MeV (Neutrons  $> 1 \text{ GeV}$ , hard X-rays  $> 10 \text{ GeV}$ , Higgs boson  $> 125 + 90 \text{ GeV}$ )

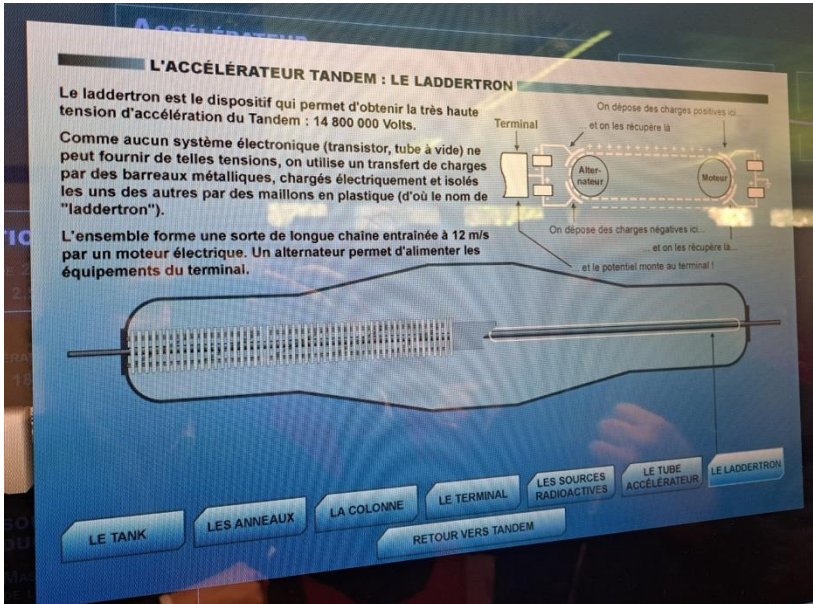


<https://alto.ijclab.in2p3.fr/en/facility/alto-heb-en/tandem-2/>

<https://www.eag.com/app-note/rutherford-backscattering-spectrometry-rbs-tutorial/>

- Rubber belt transport charges → very high voltage
- 1<sup>st</sup> accelerate negative ions → charge stripped → re-accelerate positive ions
- One can reach > 10 MV charged particles

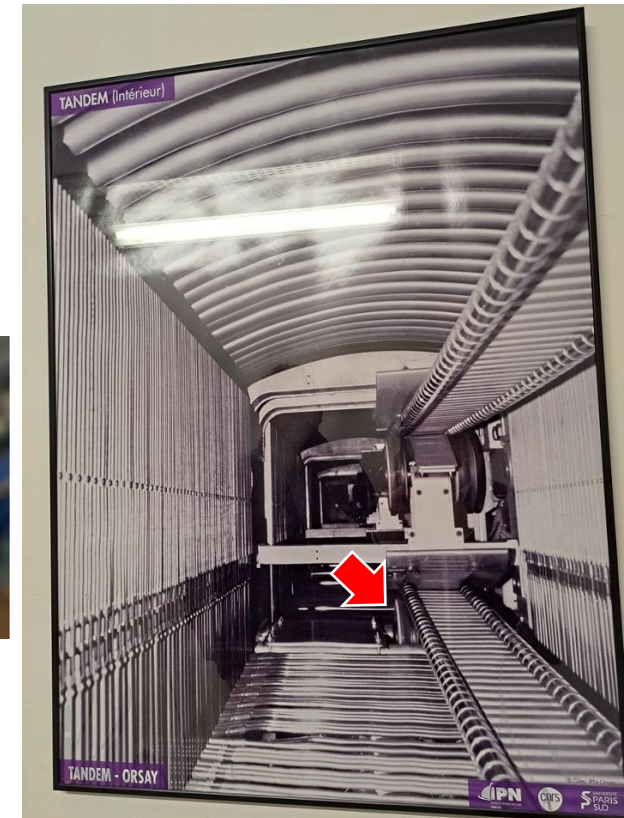
## Schematic



## Old belt



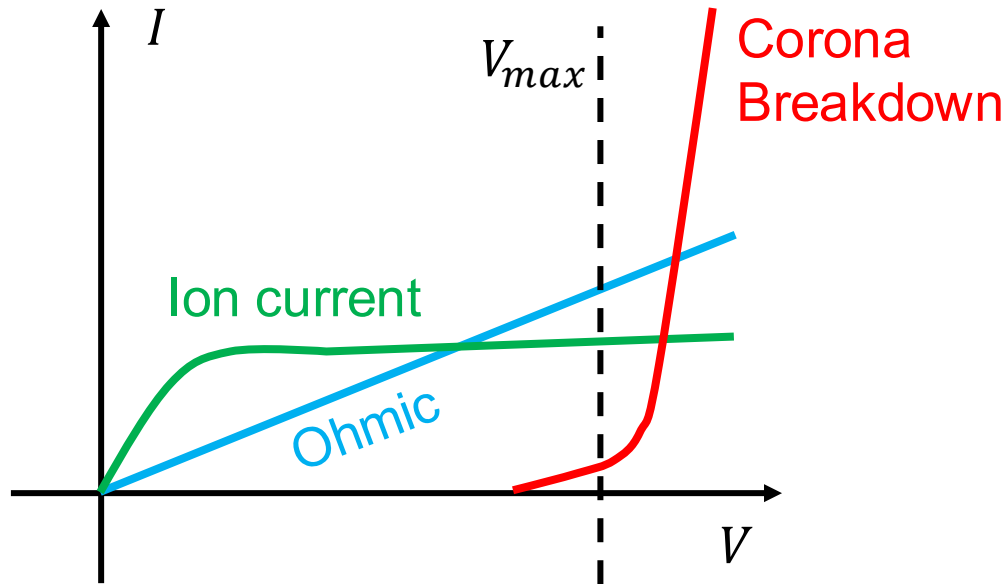
## New belt



ALTO Tandem has been operated since 1973 for physics with heavy ions → excellent user facility at Orsay  
(cf. A friend of mine in University of Tokyo wrote PhD thesis out of the nuclear physics result of the ALTO Tandem 12 years ago)



# Limitation of DC accelerator



- HV is limited to O(10 MV)  $\rightarrow$  break down even in insulating gas ( $\text{SF}_6$ )
- One cannot study GeV physics with a DC accelerator  
 $\rightarrow$  Breakthrough is necessary at this point



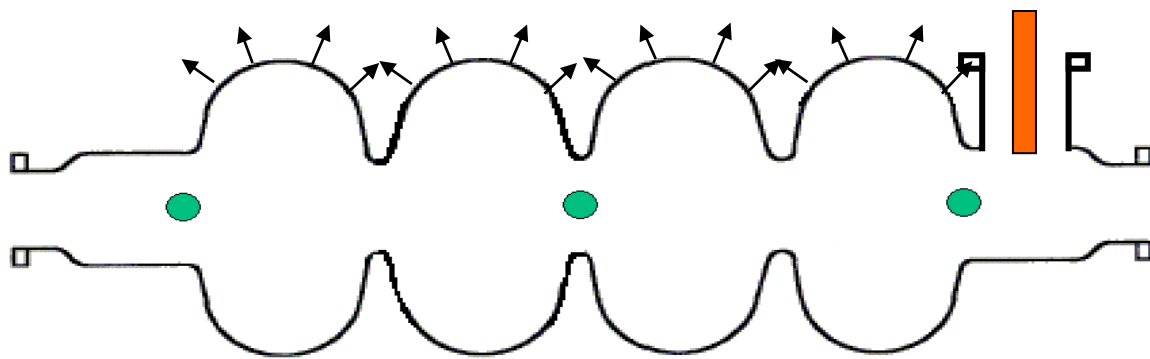
## Maxwell equation

$$\begin{cases} \nabla \cdot \mathbf{E} = 0 \\ \nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} \\ \nabla \cdot \mathbf{B} = 0 \\ \nabla \times \mathbf{B} = \frac{1}{c^2} \frac{\partial \mathbf{E}}{\partial t} \end{cases}$$

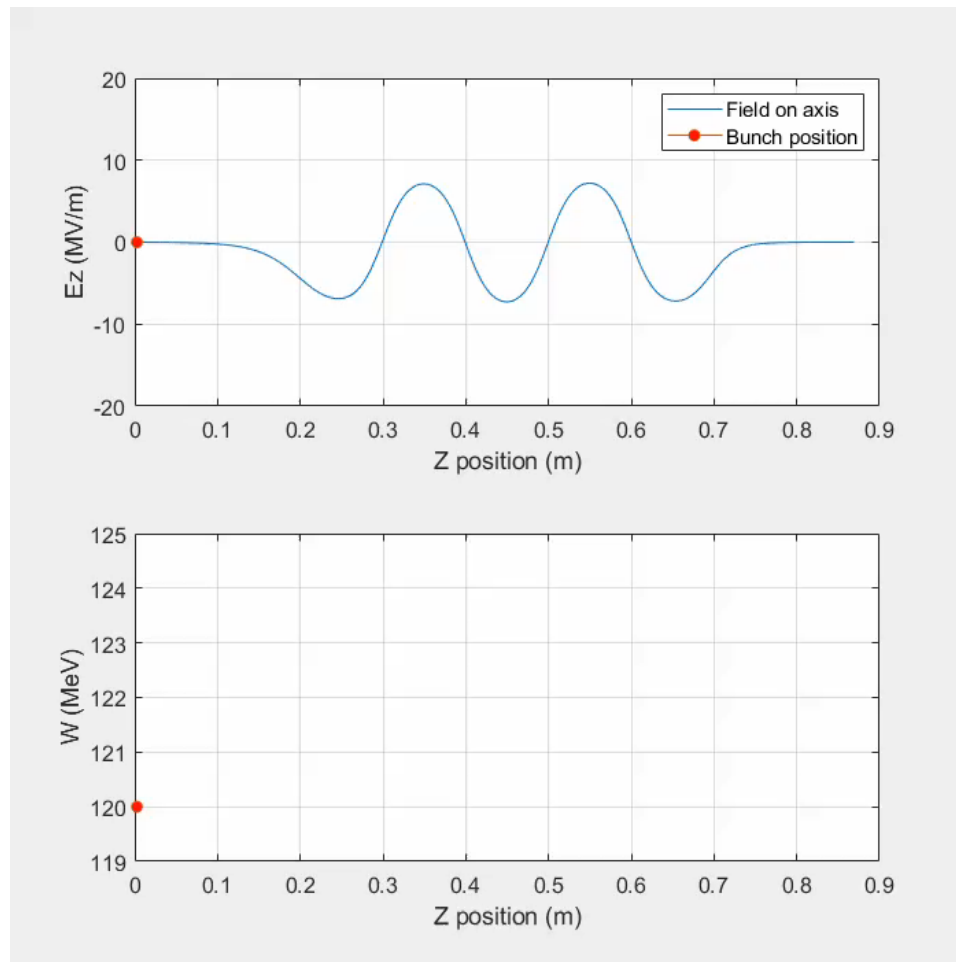
## Boundary condition

$$\begin{cases} \mathbf{n} \times \mathbf{E} = 0 \\ \mathbf{n} \cdot \mathbf{B} = 0 \end{cases}$$

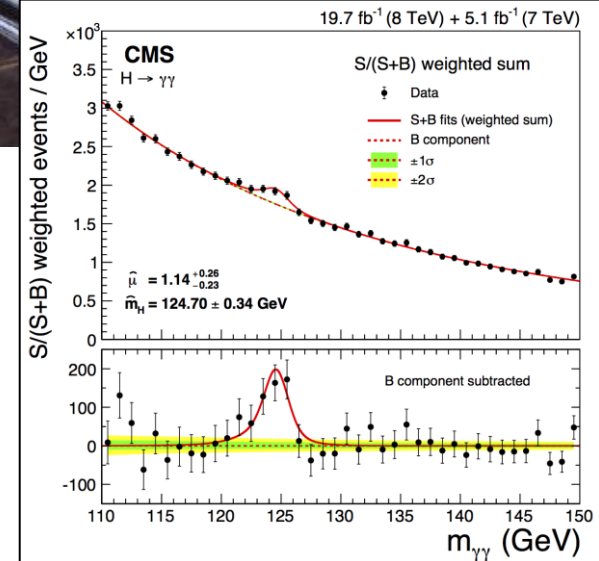
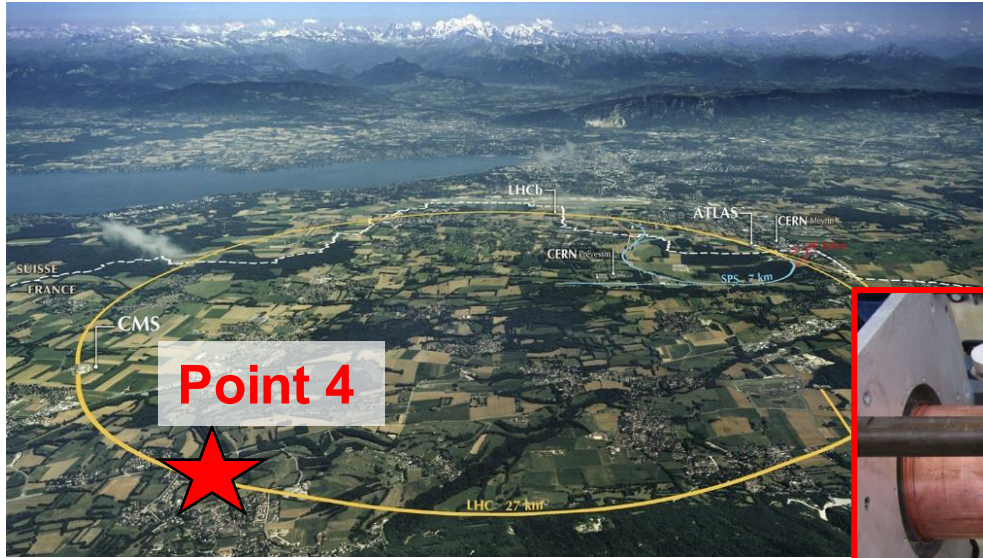
Courtesy: F. Bouly



Cascade of field  $\rightarrow \gg$  GeV in total



# Example of RF accelerators: LHC at CERN

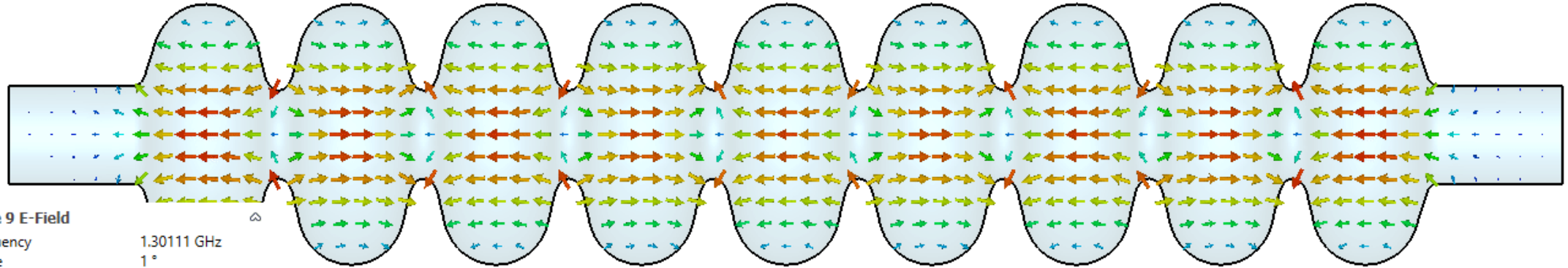


- 8 superconducting RF cavities for each ring (in total 16 cavities)
- 2 MV per each → +16 MV per turn for protons
- 11245 lap/s → 0.18 TeV/s → 7 TeV within 20 minutes
- Center mass energy 14 TeV → accessible to TeV physics
  - $ggH \rightarrow \gamma\gamma$  at 125 GeV  $\ll$  14 TeV due to parton distribution function



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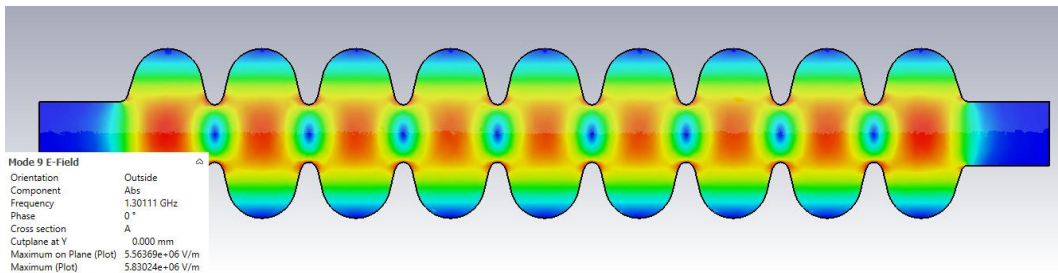
## E-field vector



**TESLA-type cavity**

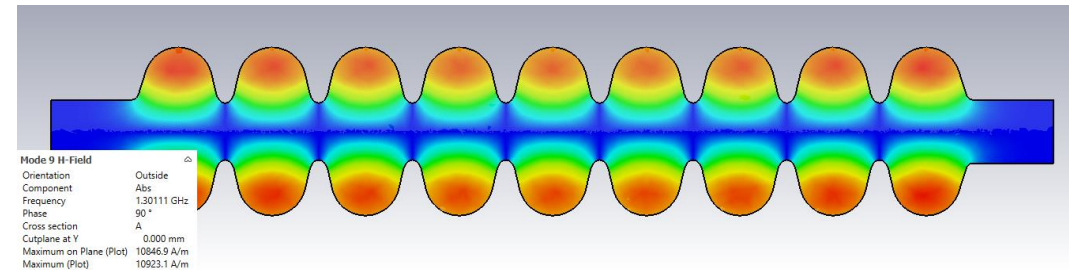
Mode 9 E-Field  
 Frequency 1.30111 GHz  
 Phase 1°  
 Cross section A  
 Cutplane at Y 0.000 mm  
 Maximum on Plane (Plot) 5.56369e+06 V/m  
 Maximum (Plot) 5.83024e+06 V/m

## E-field contour



Mode 9 E-Field  
 Orientation Outside  
 Component Abs  
 Frequency 1.30111 GHz  
 Phase 0°  
 Cross section A  
 Cutplane at Y 0.000 mm  
 Maximum on Plane (Plot) 5.56369e+06 V/m  
 Maximum (Plot) 5.83024e+06 V/m

## B-field contour



Mode 9 H-Field  
 Orientation Outside  
 Component Abs  
 Frequency 1.30111 GHz  
 Phase 90°  
 Cross section A  
 Cutplane at Y 0.000 mm  
 Maximum on Plane (Plot) 10846.9 A/m  
 Maximum (Plot) 10923.1 A/m

→ For better understandings, a bit of mathematics is helpful 😊



# Starting point: Maxwell equations

With charges and current

In vacuum

**Gauss Law**

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho}{\epsilon_0}$$

$$\vec{\nabla} \cdot \vec{E} = 0$$

**No monopole**

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

**Ampere law**

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{j} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$



$$\vec{\nabla} \times \vec{B} = \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

**Faraday law**

$$\vec{\nabla} \times \vec{E} = - \frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \times \vec{E} = - \frac{\partial \vec{B}}{\partial t}$$



**Wave equation**

$$\left( \nabla^2 - \mu_0 \epsilon_0 \frac{\partial^2}{\partial t^2} \right) \begin{Bmatrix} \vec{E} \\ \vec{H} \end{Bmatrix} = 0$$

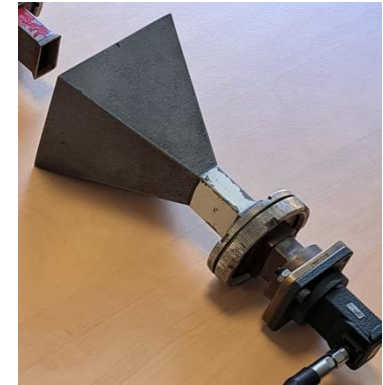
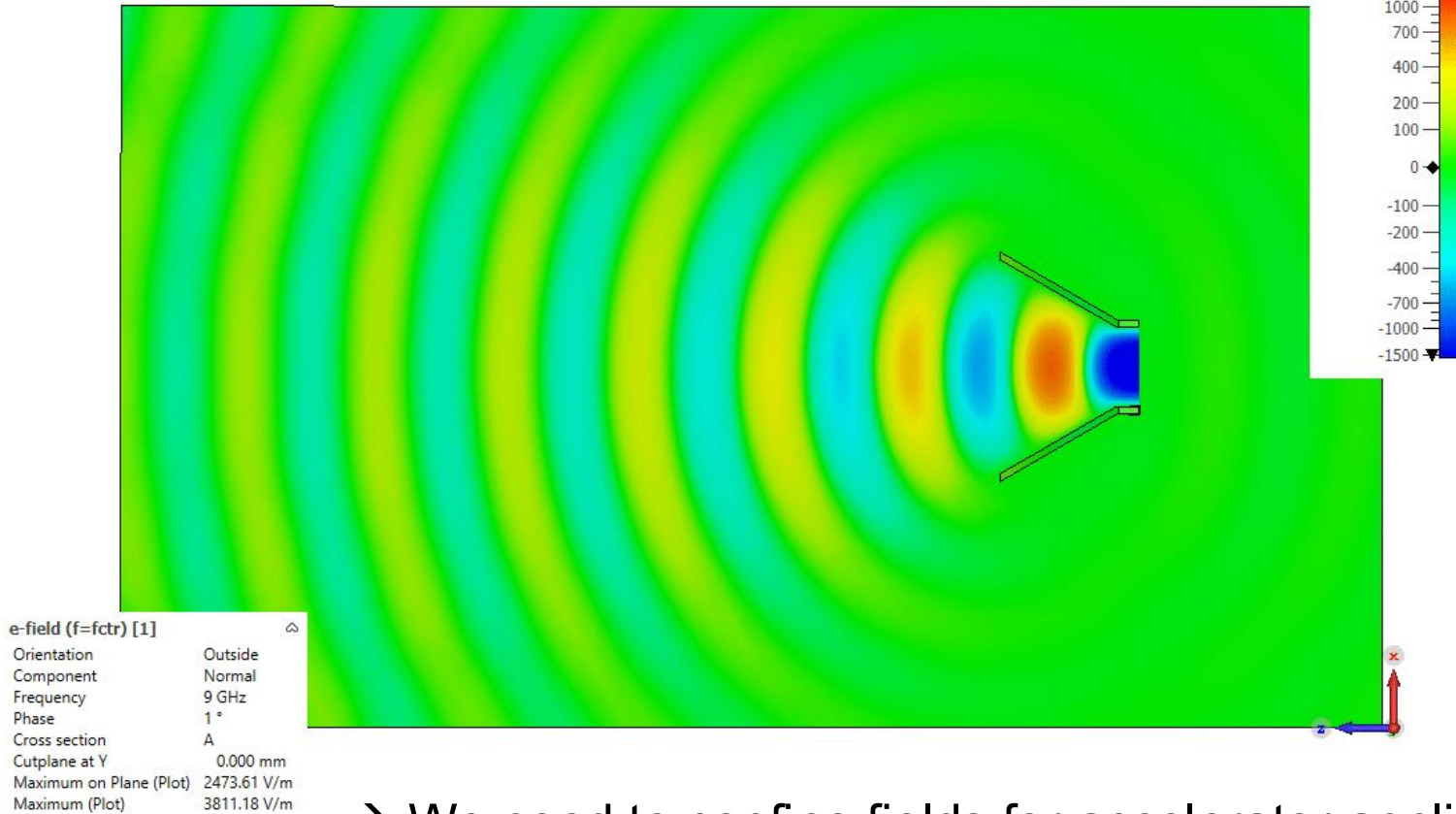
$$c = \frac{1}{\sqrt{\mu_0 \epsilon_0}}$$

➤ The boundary condition is necessary to solve these partial differential equations



# A solution in free space

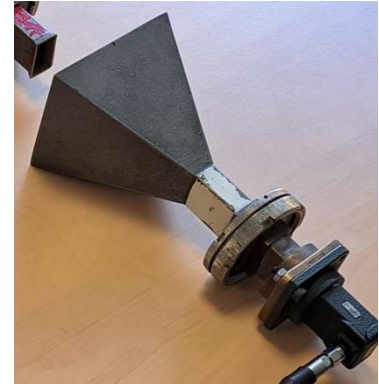
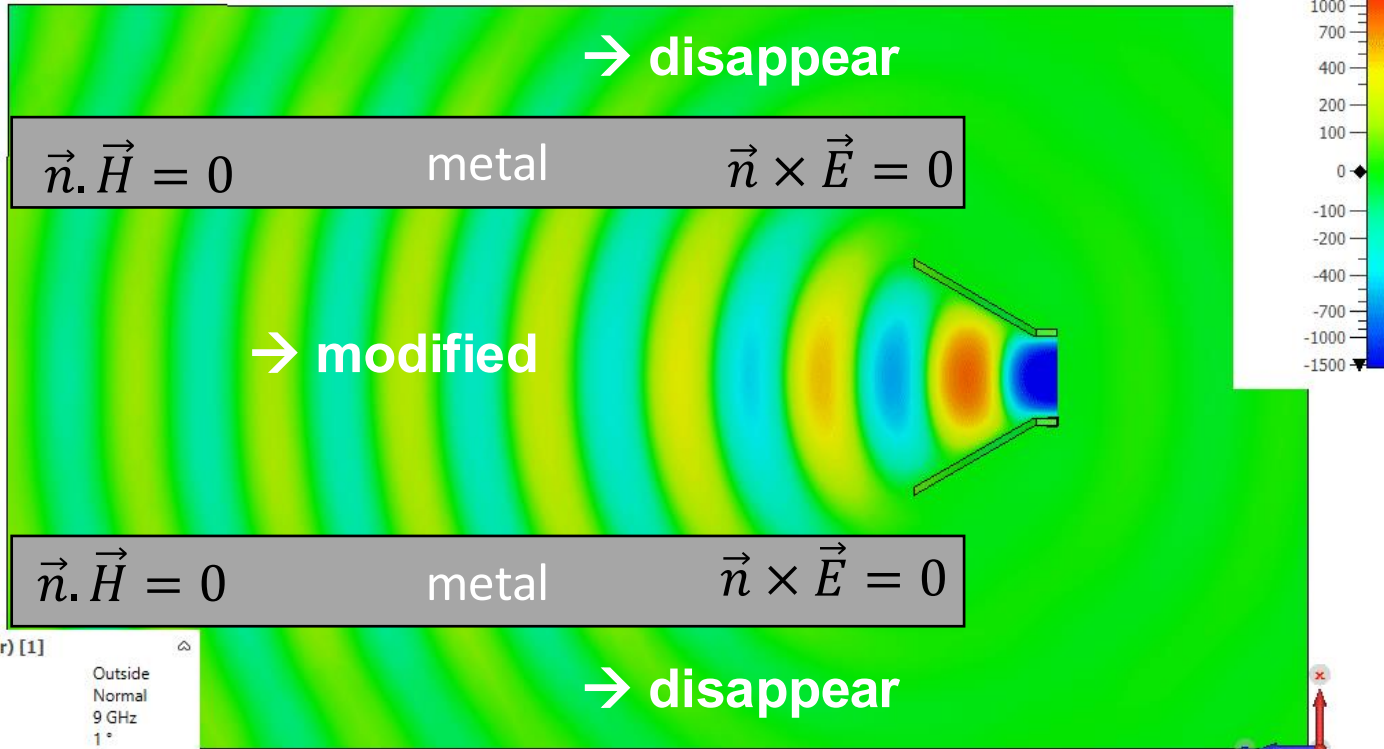
$$\left( \nabla^2 - \mu_0 \epsilon_0 \frac{\partial^2}{\partial t^2} \right) \begin{Bmatrix} \vec{E} \\ \vec{H} \end{Bmatrix} = 0 \rightarrow \vec{E} = \vec{E}_0(x, y, z) \exp(i\omega t - ikz)$$



→ We need to confine fields for accelerator applications

# A solution in free space

$$\left( \nabla^2 - \mu_0 \epsilon_0 \frac{\partial^2}{\partial t^2} \right) \begin{Bmatrix} \vec{E} \\ \vec{H} \end{Bmatrix} = 0 \rightarrow \vec{E} = \vec{E}_0(x, y, z) \exp(i\omega t - ikz)$$



e-field (f=fctr) [1]

Orientation	Outside
Component	Normal
Frequency	9 GHz
Phase	1 °
Cross section	A
Cutplane at Y	0.000 mm
Maximum on Plane (Plot)	2473.61 V/m
Maximum (Plot)	3811.18 V/m

**→ Recalculate Maxwell equations**



# Propagation mode in a waveguide

Difference from free space: propagation constant  $\beta$

$$\vec{E}(\vec{x}, t) = \vec{E}(\rho)e^{i\omega t - i\beta z}$$

$$\vec{H}(\vec{x}, t) = \vec{H}(\rho)e^{i\omega t - i\beta z}$$

$$\left( \nabla_t^2 + \frac{\omega^2}{c^2} - \beta^2 \right) \begin{Bmatrix} \vec{E} \\ \vec{H} \end{Bmatrix} = 0$$

Cut-off wave number

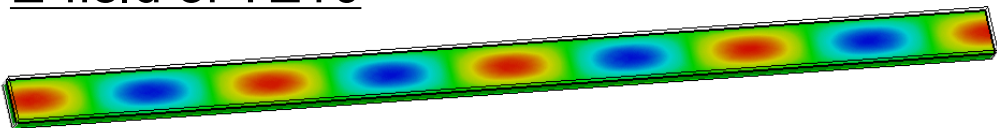
$$k_c^2 = \frac{\omega^2}{c^2} - \beta^2 \geq 0$$

Relation in transverse fields

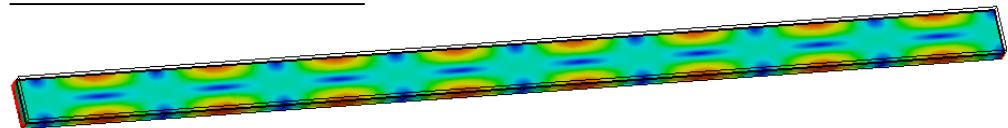
$$\vec{H}_t = \frac{\vec{z} \times \vec{E}_t}{Z}$$

Wave impedance  $Z$

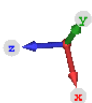
E-field of TE10



H-field of TE10



e-field (f=7) [1]  
 Orientation Outside  
 Component Normal  
 Frequency 7 GHz  
 Phase 1°  
 Cross section A  
 Cutplane at Y 6.096 mm  
 Maximum on Plane (Plot) 3138.43 V/m  
 Maximum (Plot) 3153.92 V/m



h-field (f=7) [1]  
 Orientation Outside  
 Component Abs  
 Frequency 7 GHz  
 Phase 1°  
 Cross section A  
 Cutplane at Y 6.096 mm  
 Maximum on Plane (Plot) 8.22528 A/m  
 Maximum (Plot) 8.25014 A/m



2 sets of modes

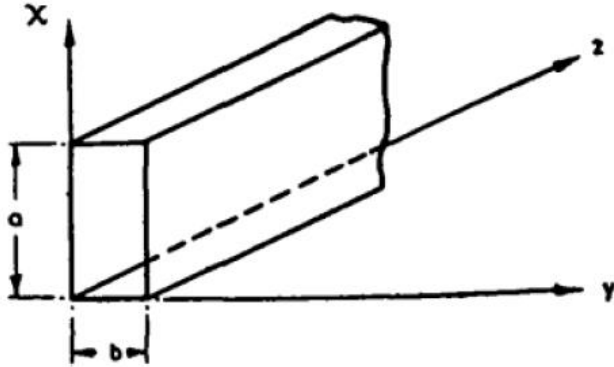
- *transverse magnetic (TM) modes*
- *transverse electric (TE) modes*

$$Z_{TM} = \frac{\beta}{\epsilon\omega}$$

$$Z_{TE} = \frac{\mu\omega}{\beta}$$



# Analytical solutions of rectangular waveguides



- Boundaries conditions

$$TE: \begin{cases} e_x(x, y) = 0 & y = 0, b \\ e_y(x, y) = 0 & x = 0, a \end{cases}$$

$$TM: \begin{cases} e_z(x, y) = 0 & y = 0, b \\ e_z(x, y) = 0 & x = 0, a \end{cases}$$

- Cut-off wave number :  $k_c^2 = k_x^2 + k_y^2$

- Solution of the form ( $e^{-i\beta z}$  disregarded)

$$TE: H_z = A_{mn} \cos k_x x \sin k_y y \left\{ \begin{array}{l} E_x = \frac{i\omega\mu n\pi}{k_c^2 b} A_{mn} \cos k_x x \sin k_y y \\ E_y = \frac{-i\omega\mu m\pi}{k_c^2 a} A_{mn} \sin k_x x \cos k_y y \end{array} \right.$$

$$TM: E_z = B_{mn} \cos k_x x \sin k_y y \left\{ \begin{array}{l} H_x = \frac{i\beta m\pi}{k_c^2 a} B_{mn} \sin k_x x \cos k_y y \\ H_y = \frac{i\beta n\pi}{k_c^2 b} B_{mn} \cos k_x x \sin k_y y \end{array} \right.$$

$$\left. \begin{array}{l} H_x = \frac{i\omega\varepsilon n\pi}{k_c^2 b} B_{mn} \sin k_x x \cos k_y y \\ H_y = \frac{-i\omega\varepsilon m\pi}{k_c^2 a} B_{mn} \cos k_x x \sin k_y y \\ E_x = \frac{-i\beta m\pi}{k_c^2 a} B_{mn} \cos k_x x \sin k_y y \\ E_y = \frac{-i\beta n\pi}{k_c^2 b} B_{mn} \sin k_x x \cos k_y y \end{array} \right\}$$

- The propagating constant is

$$\beta = \sqrt{k^2 - k_c^2} = \sqrt{k^2 - \left(\frac{m\pi}{a}\right)^2 - \left(\frac{n\pi}{b}\right)^2}$$

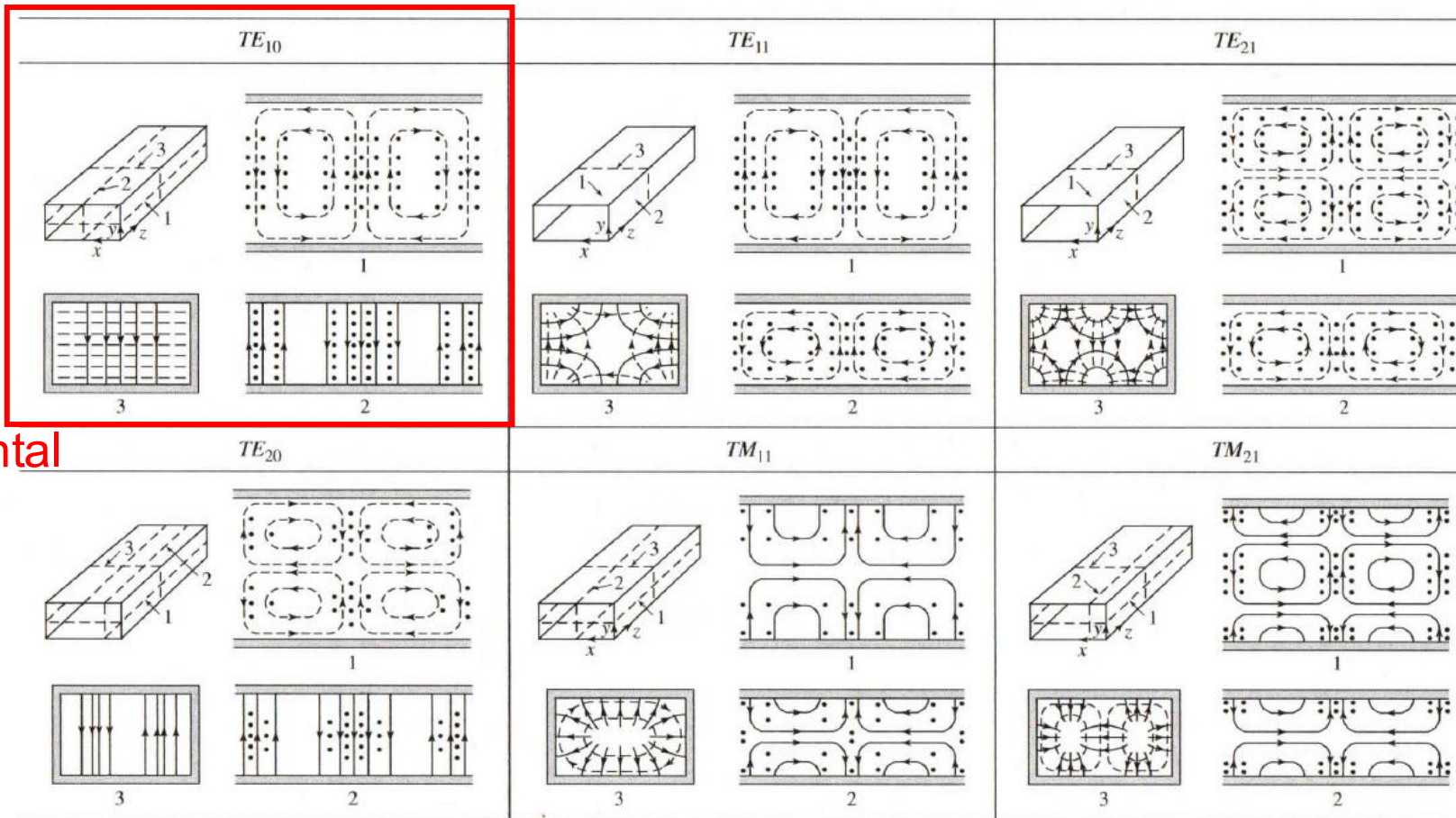
- Each mode has a cutoff frequency

$$f_{c_{m,n}} = \frac{k_c}{2\pi\sqrt{\mu\varepsilon}} = \frac{1}{2\pi\sqrt{\mu\varepsilon}} \sqrt{\left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2}$$

with  $k_x = \frac{m\pi}{a}$  ;  $k_y = \frac{n\pi}{b}$

No  $TE_{00}$ ,  $TM_{00}$ ,  $TM_{01}$  and  $TM_{10}$   
The lowest modes are  $TE_{10}$   $TM_{11}$

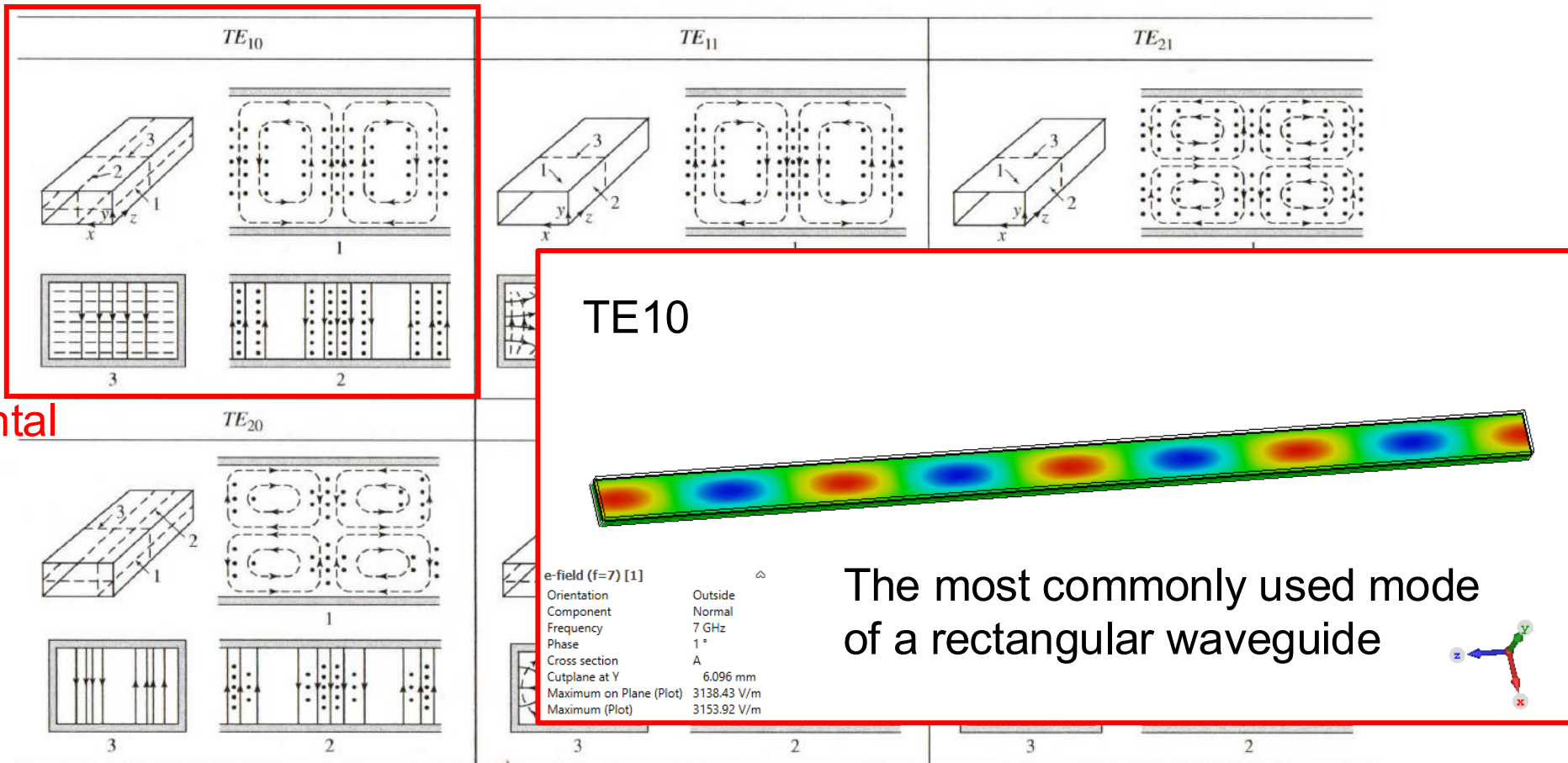
# Visualized modes



Fundamental mode

Field lines for some of the lower order modes of a rectangular waveguide (from D.M. Pozar)

# Visualized modes

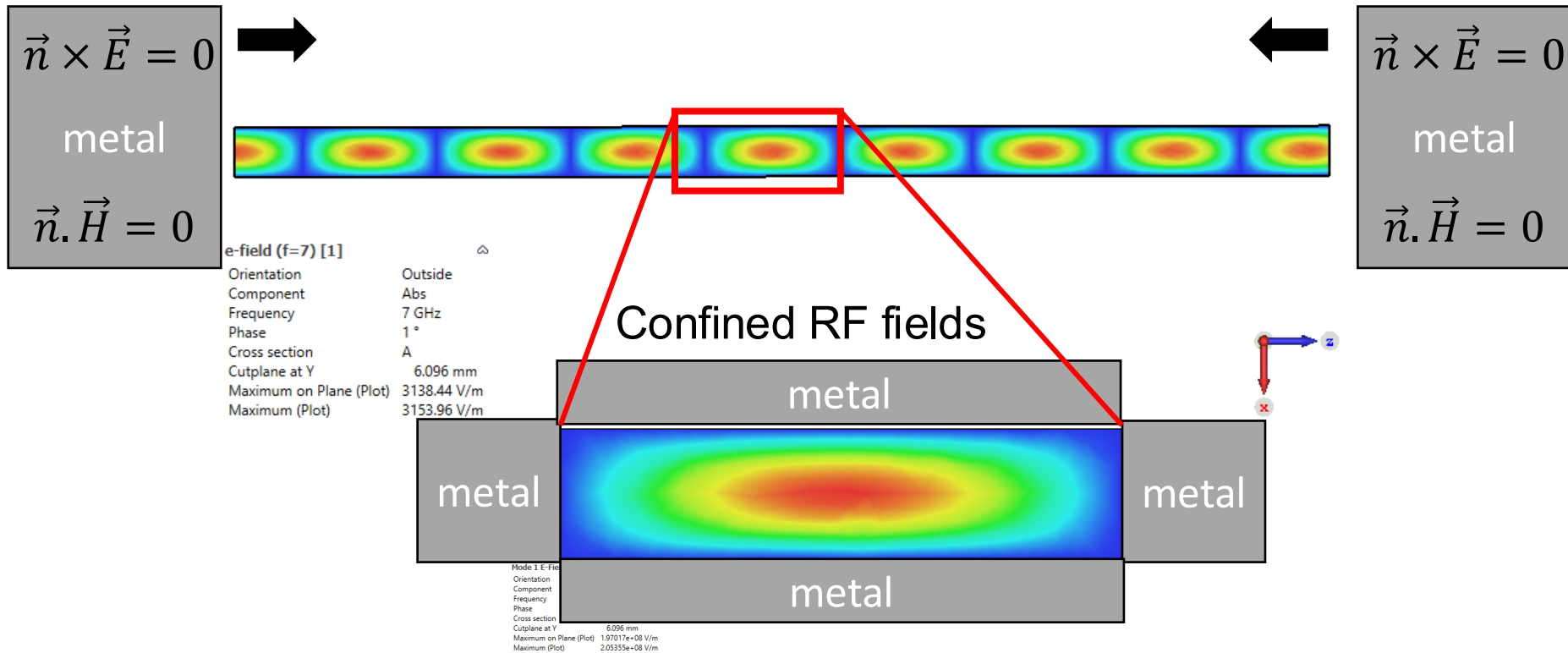


Fundamental mode

Field lines for some of the lower order modes of a rectangular waveguide (from D.M. Pozar)



# From a waveguide to a resonant cavity



However, TE<sub>10</sub> in rectangular cavity cannot accelerate charged particles  
 → One need a strong electric field at the center of the resonator

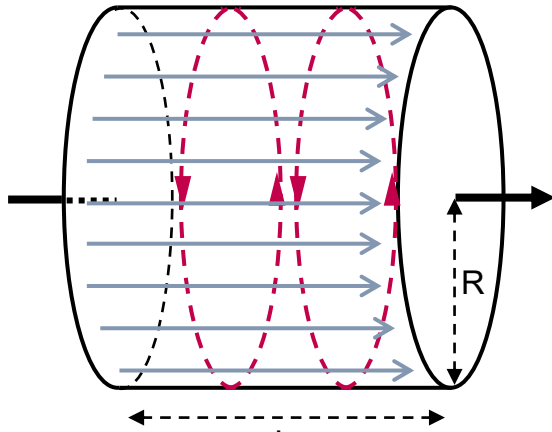


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## Pill-box cavity TM010

The simplest cavity is cylindrical geometry with radius  $R$  and length  $L$



« Pill-box » cavity : TM 010 mode     $\rightarrow E_z$      $-\ - \rightarrow H_\theta$

Transverse magnetic modes with longitudinal electric field are used for acceleration ( $TM_{0,n,p}$ )

Boundaries conditions:

- On cavity wall  $\Rightarrow \vec{n} \cdot \vec{H} = 0$
- Optionally at  $z = 0$  and  $z = L \Rightarrow \vec{n} \cdot \vec{H} = 0$  and  $H = 0$

Applying Maxwell's equation and boundaries conditions yield to Helmholtz equation:

$$(\nabla^2 + \omega^2 \mu \epsilon) H = 0$$

- There is infinity of  $TM_{0XX}$  solutions (modes)
- All modes are defined by frequency  $\omega_n$  and the EM fields:

$$H_n(r, z) = [0, H_{\theta,n}(r, z), 0]$$

$$E_n(r, z) = [E_{r,n}(r, z), 0, E_{z,n}(r, z)]$$



# Performance of cavities 1/2

Good cavity: higher accelerating voltage  $V_{acc}$  with lower power loss  $P_c$  on the cavity wall  
 → Shunt impedance  $R_{sh}$  to be maximized

$$R_{sh} \equiv \frac{V_{acc}^2}{P_c}$$

The field level is related to stored energy of the useful mode (TM010) inside the cavity

$$U \equiv 2\mu \int_V \frac{H^2}{4} dV = 2\varepsilon \int_V \frac{E^2}{4} dV (= \kappa V_{acc}^2) \quad \kappa \text{ (geometrical factor)}$$

The loss is given by surface integral of RF magnetic field on the cavity wall with surface resistance  $R_s$

$$P_c = \frac{R_s}{2} \int H^2 dS$$

→ Unloaded quality factor is defined

$$Q_0 \equiv \frac{\omega U}{P_c} = \frac{1}{R_s} \boxed{\omega\mu \frac{\int_V H^2 dV}{\int H^2 dS}} \equiv G \text{ (geometrical factor)}$$



The shunt impedance can be written

$$R_{sh} \equiv \frac{V_{acc}^2}{P_c} = \frac{U}{\kappa P_c} = \frac{Q_0}{\kappa \omega} = \frac{1}{\omega} \frac{G}{\kappa} \frac{1}{R_s} \rightarrow \text{Surface resistance given by material}$$

$(R_{sh}/Q \text{ is also geometrical})$ 

 $\rightarrow$  geometry

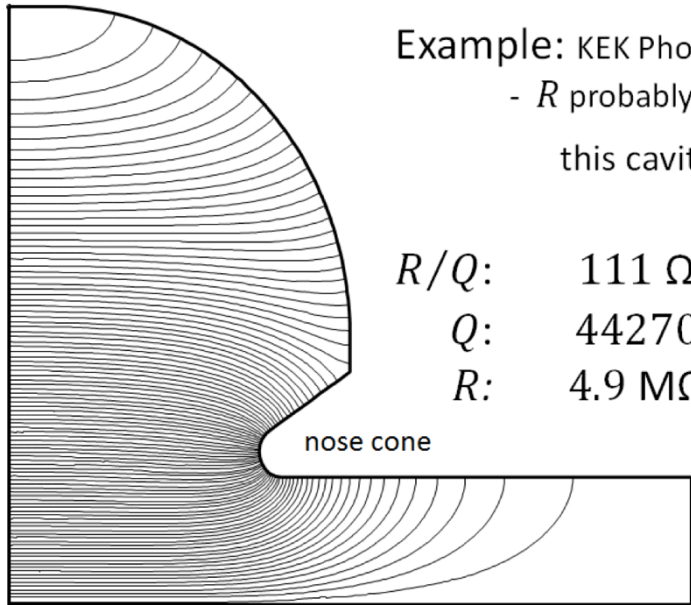
The cavities can be optimized by better geometry and material (normal conducting vs superconducting)

Other figures of merit (geometrical):

$\frac{E_{pk}}{E_{acc}}$  : peak electric field is on the cavity wall NOT the accelerating field  $\rightarrow$  breakdown

$\frac{B_{pk}}{E_{acc}}$  : peak magnetic field is also crucial in superconducting cavities  $\rightarrow$  quench

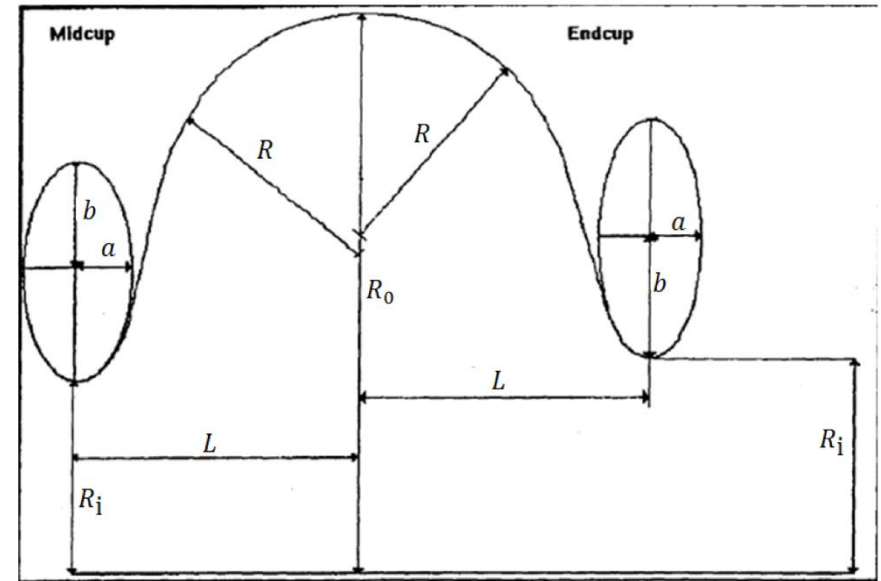
## Maximize $R_{sh}/Q$



Example: KEK Photon Factory 500 MHz  
 -  $R$  probably as good as it gets -

	this cavity	optimized pillbox
$R/Q$ :	111 $\Omega$	107.5 $\Omega$
$Q$ :	44270	41630
$R$ :	4.9 M $\Omega$	4.47 M $\Omega$

## So so $R_{sh}/Q$ but reduce $B_{pk}/E_{acc}$

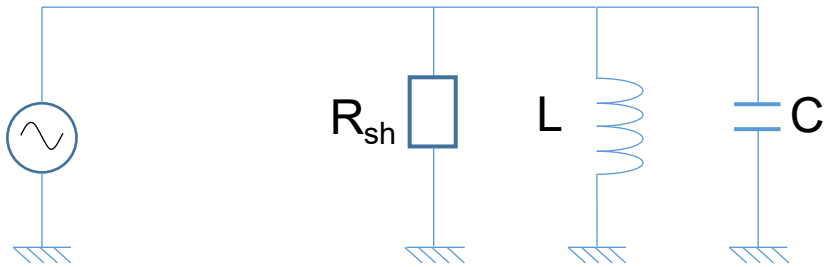
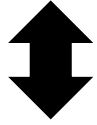
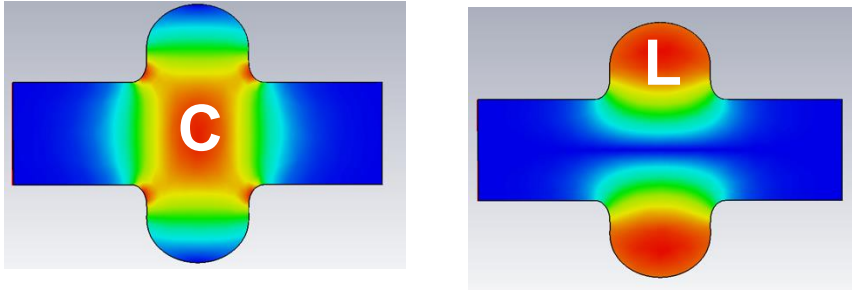


D. Proch, <http://accelconf.web.cern.ch/accelconf/SRF93/papers/srf93g01.pdf>

- Depending on the project demand, frequency, priority, etc, the best structure is different
- A lot of phenomena (ultimate performance, risk of discharge, quench etc)  $\rightarrow$  compromise
- Lessons learned: over-optimization in one figure of merit may overlook a showstopper!



# Equivalent circuit approach



A resonating cavity can be modeled by a lumped capacitance  $C$ , resistance  $R$  and inductance  $L$

The input impedance is: 
$$Z_{in} = \left( \frac{1}{R_{sh}} + \frac{1}{j\omega L} + j\omega C \right)^{-1}$$

Assuming  $\omega = \omega_0 + \Delta\omega$  ( $\Delta\omega \ll \omega_0$ ) and  $\omega_0 = 1/\sqrt{LC}$

$$Z_{in} = \frac{R_{sh}}{1 + 2Q \frac{\Delta\omega}{\omega_0}} \text{ with } Q = \frac{\omega_0}{2\Delta\omega} = \omega_0 R_{sh} C = \frac{R_{sh}}{\omega_0 L}$$

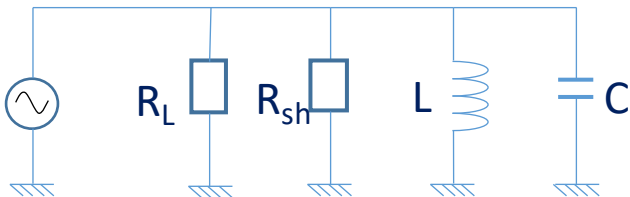
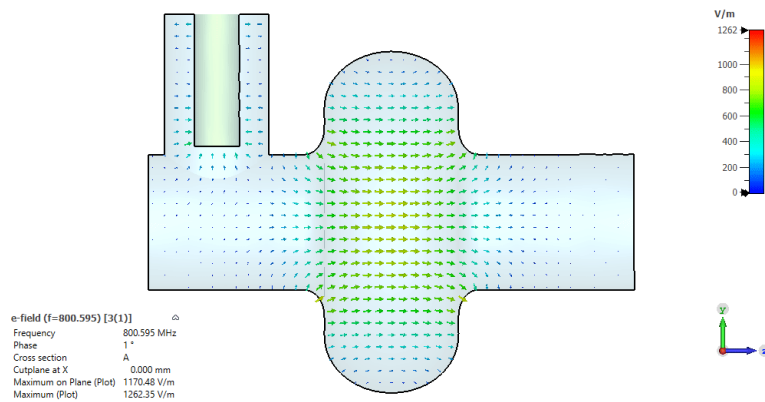
Remark 1:  $R_{sh} \neq R_s$

Remark 2:  $R_{sh}$  conventionally used in general circuit theory differs by factor 2

From the knowledge of the  $\omega_0$ ,  $Q$  and  $R/Q$  of the RF structure, one get the equivalent resonant circuit

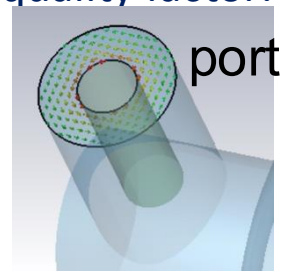


# Benefit of equivalent circuit mode → coupler analysis



Resonant cavity is fed by coupling port in order to provide EM wave. As intrinsic quality factor, one can define the external quality factor:

$$Q_{ext} = \frac{\omega_0 U}{P_e} = \frac{\omega_0 U}{\frac{1}{2} \int_{S_{port}} \vec{E} \times \vec{H} dS}$$



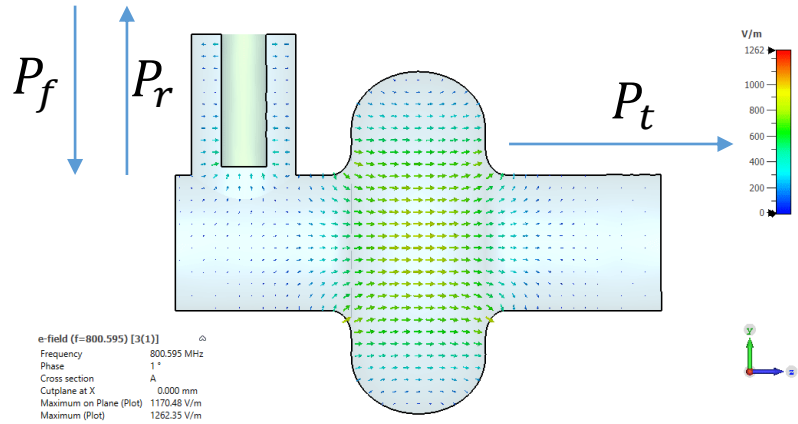
From RLC equivalent circuit, the external coupling yields at additional losses to an external load  $R_L$  in parallel

$$Q_L = \frac{R_{tot}}{\omega_0 L} \quad \text{with} \quad R_{tot} = \frac{R_{sh} R_L}{R_{sh} + R_L}$$

Then, external coupling is:  $Q_{ext} = \frac{R_L}{\omega_0 L} \Rightarrow \frac{1}{Q_L} = \frac{1}{Q_0} + \frac{1}{Q_{ext}}$

Generalization of this concept leads at:  $\frac{1}{Q_L} = \frac{1}{Q_0} + \sum_i \frac{1}{Q_i}$

# Coupling factor and pulse response

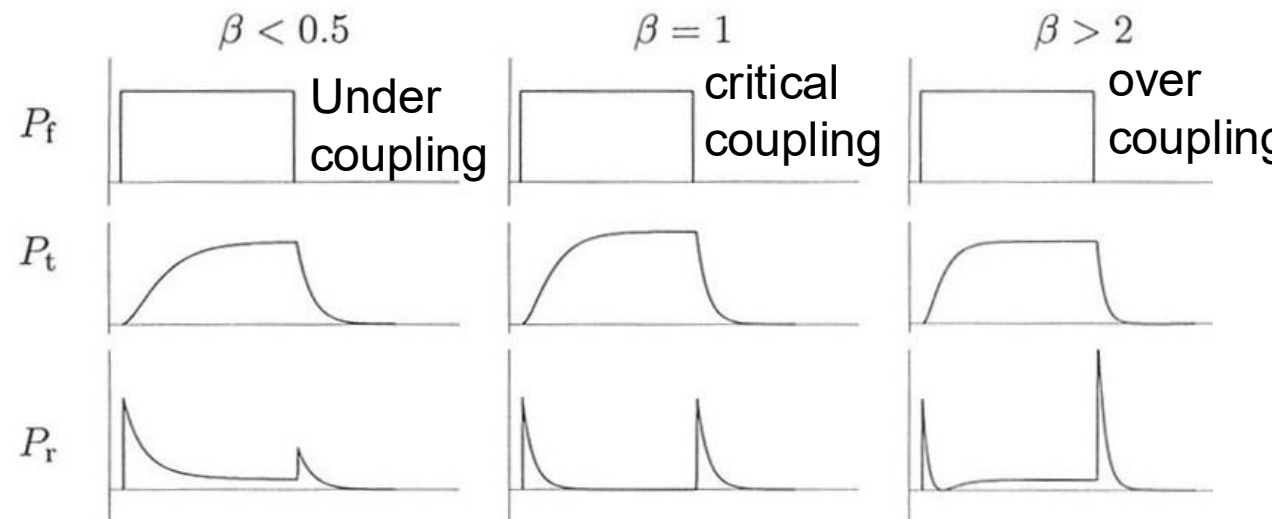
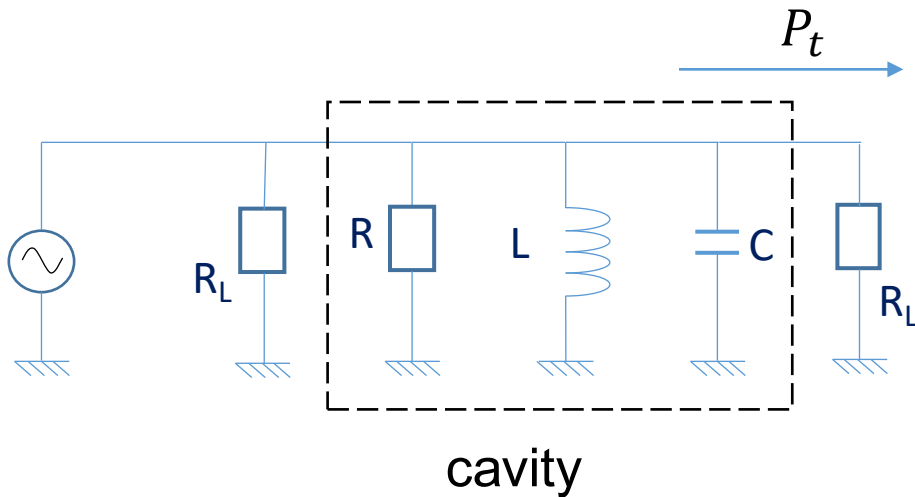


Without beam, the intrinsic quality factor is

$$Q_0 = Q_L(1 + \beta_i + \beta_t) \text{ with } \beta_i = \frac{Q_0}{Q_i} \text{ and } \beta_t = \frac{Q_0}{Q_t}$$

When the RF generator is turned off, the EM field is solution of the equation:

$$E(t) + \tau \cdot \frac{dE(t)}{dt} + \frac{1}{\omega_0^2} \cdot \frac{d^2E(t)}{dt^2} = 0 \text{ with } \tau = \frac{Q_L}{\omega_0} = \frac{1}{\Delta\omega}$$



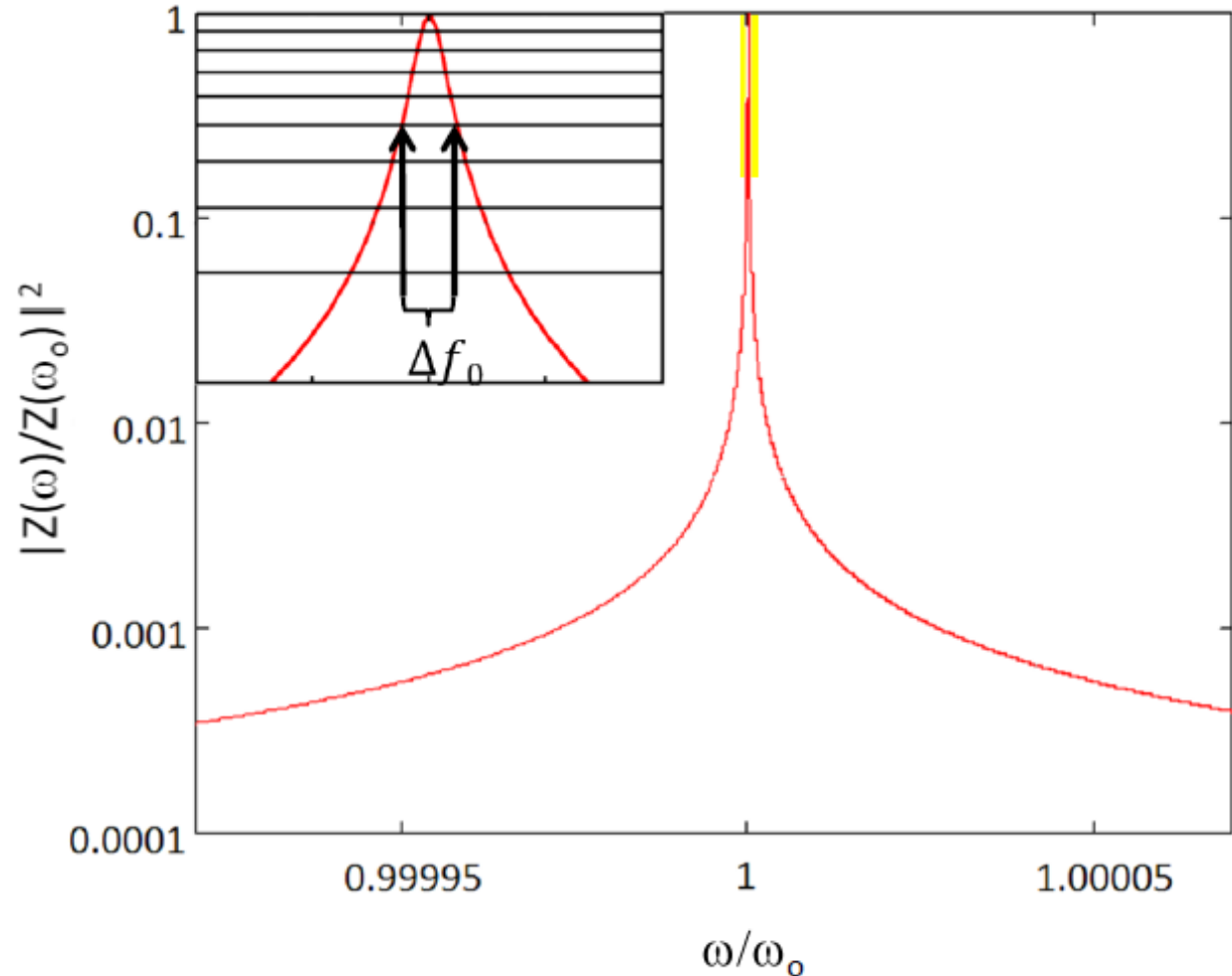


maximum of  $Z(\omega)$

$$\omega_0 \equiv 1/\sqrt{LC}$$

Sharpness of resonance

$$Q_L = \frac{f}{\Delta f} = \frac{U}{\Delta U}$$





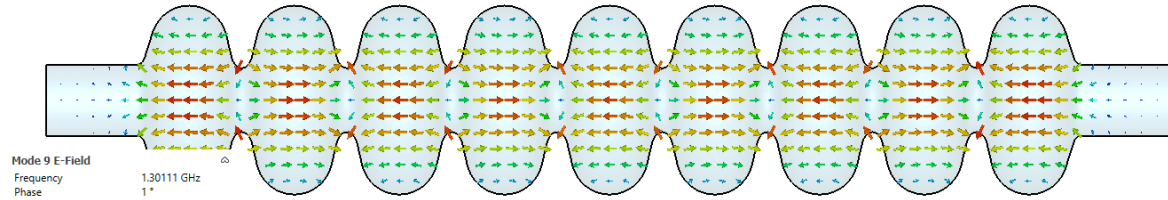
- Introduction: from DC to RF accelerator (15 min)
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- **Break (10 min)**
- RF around cavities (10 min)
- Wake field (10 min)
- Various shapes of RF cavities (10 min)
- Conclusion



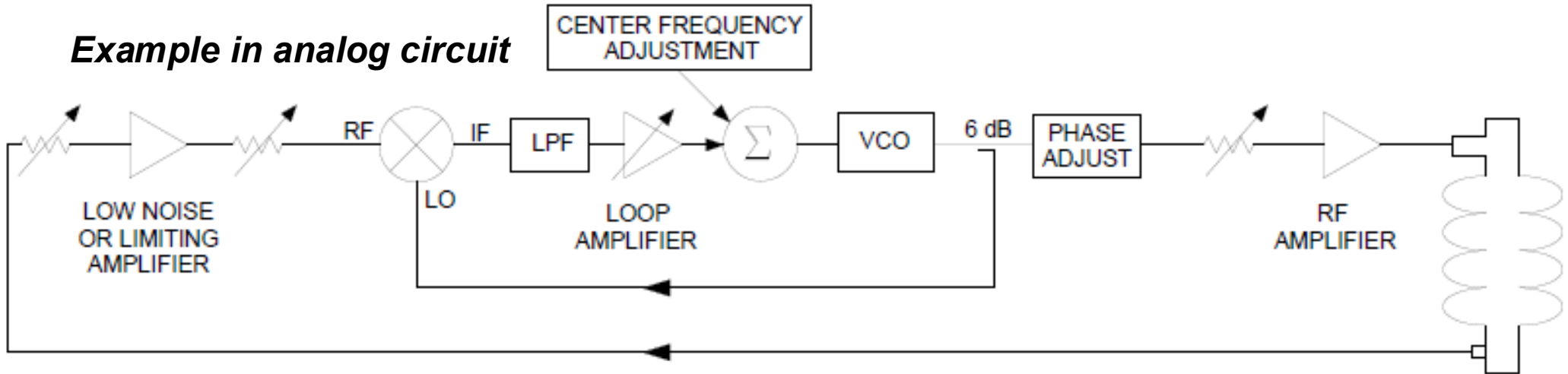
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# A lonely empty cavity is useless

We need RF inside

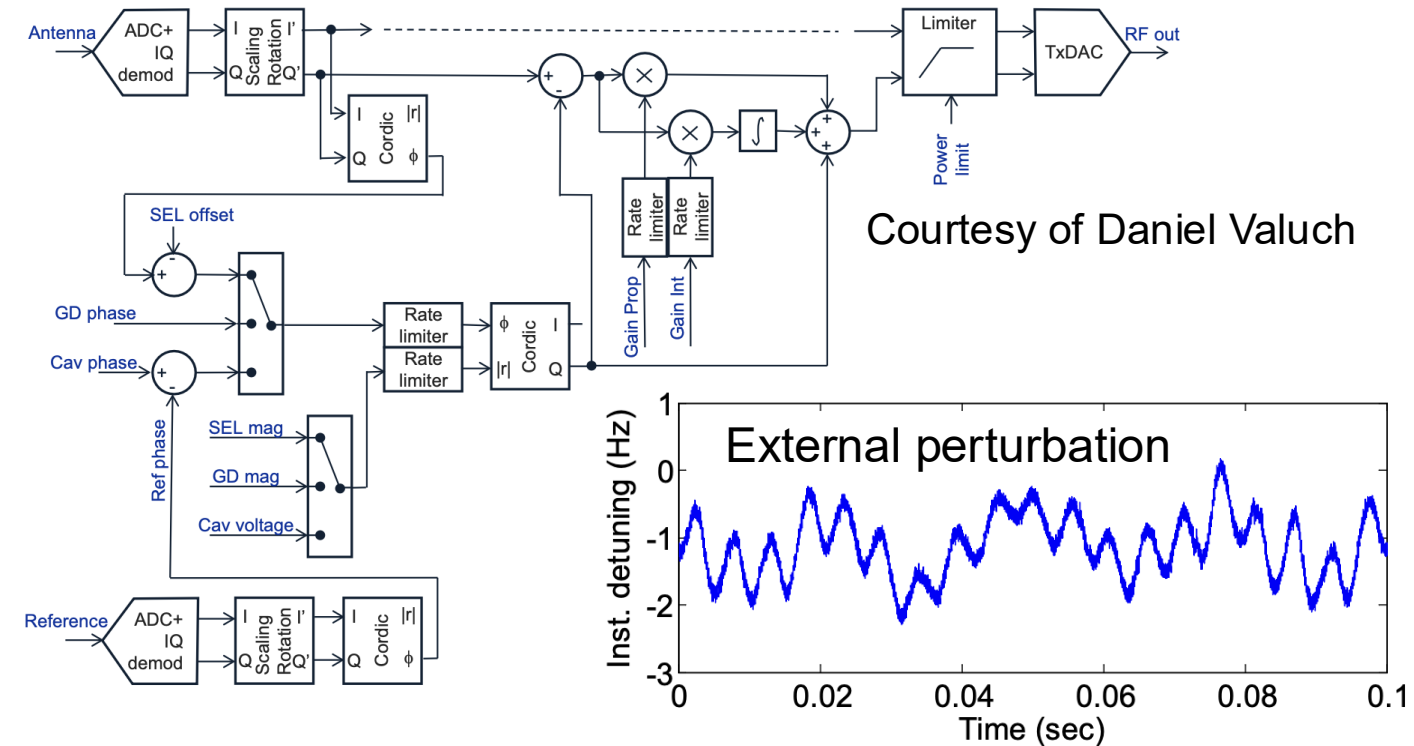


*Example in analog circuit*

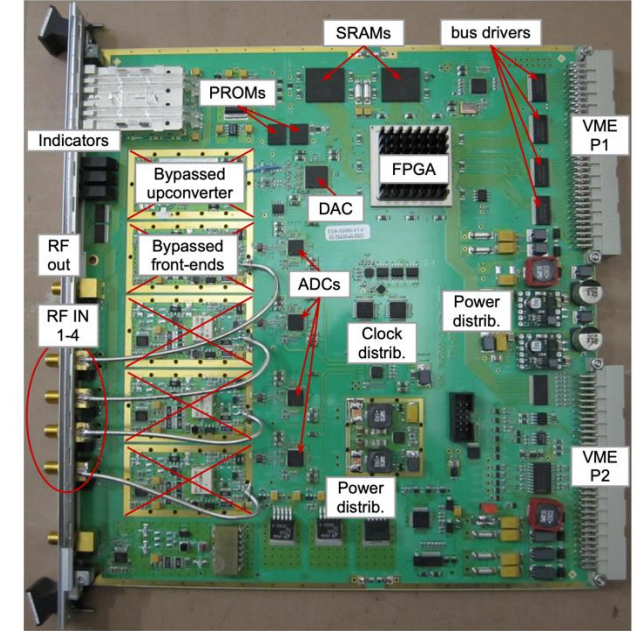


- A low-power RF circuit locks frequency, phase, and amplitude of the superconducting cavity
- An RF amplifier generates useful power level
- A power coupler feeds RF to the cavity
- Tuner controls resonant frequency of the cavity

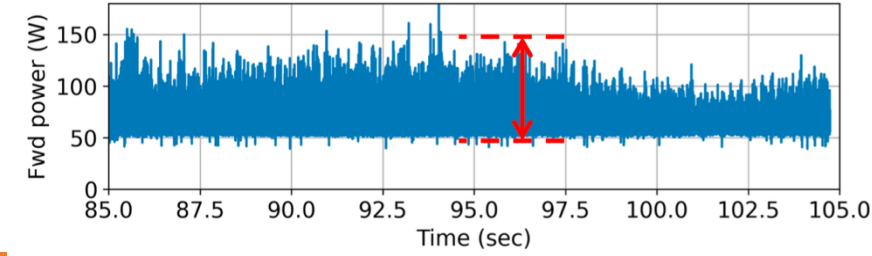
## M. Elias master thesis



Courtesy of Daniel Valuch



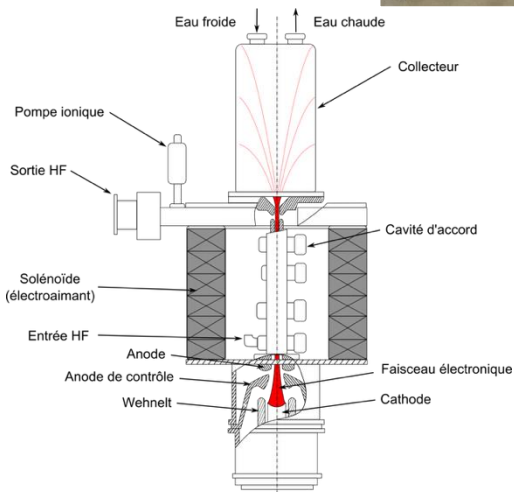
FB to keep cavity field constant



- Design analog and digital circuit to cope with various phenomena to keep cavity field stable
- Control theory and implementation in FPGA
- Directly handled power: 1 mW → needs amplifier

## Vacuum tubes / klystrons

Amplification via the RF & DC beam interaction

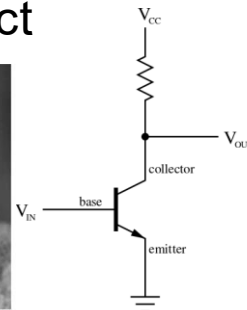


## Transistor-based solid-state amplifiers

Amplification via the tunneling effect



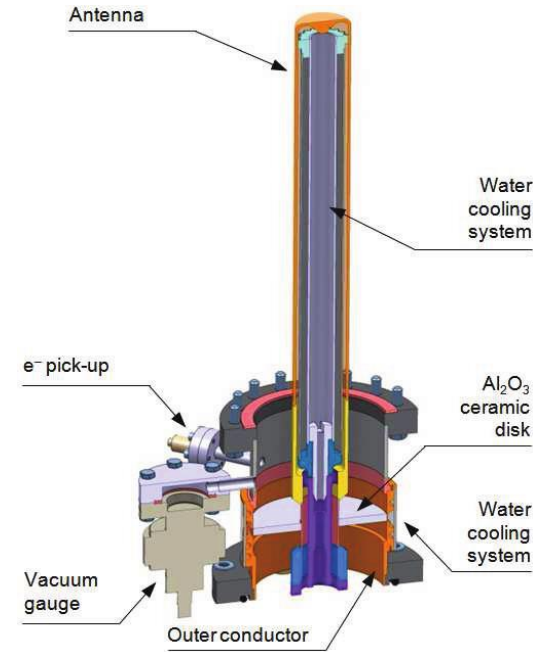
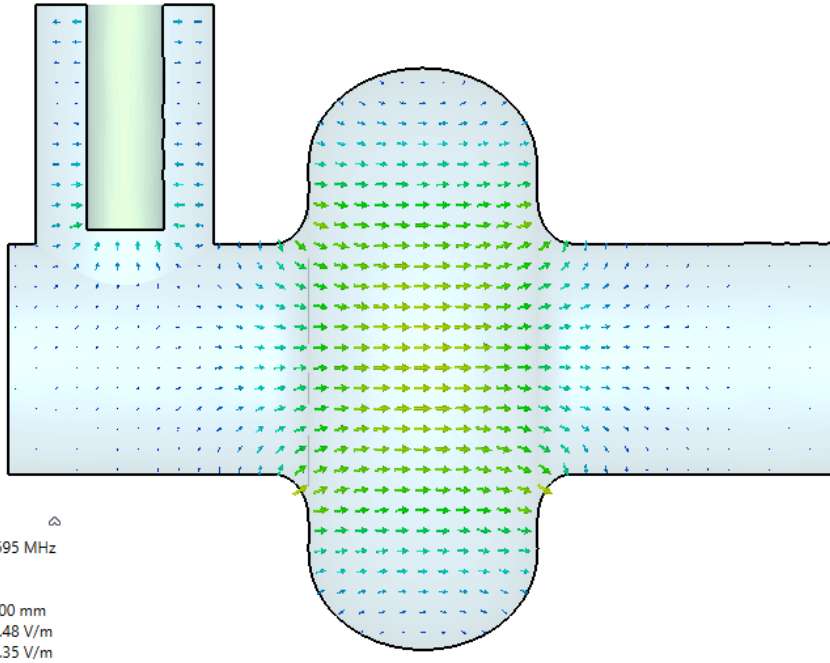
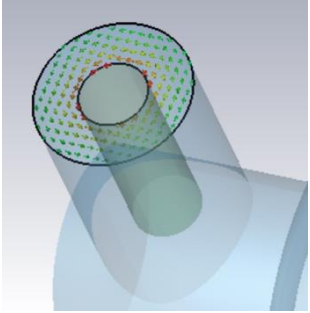
Shockley Bardeen Brattain



Courtesy: Eric Montesinos

# RF power coupler to feed RF

port



Power flow (Poynting vector) through the port gives coupler Q

$$Q_{ext} = \frac{\omega_0 U}{P_e} = \frac{\omega_0 U}{\frac{1}{2} \int_{S_{port}} \vec{E} \times \vec{H} dS}$$

Total Q of the cavity is thus shifted from unloaded  $Q_0$

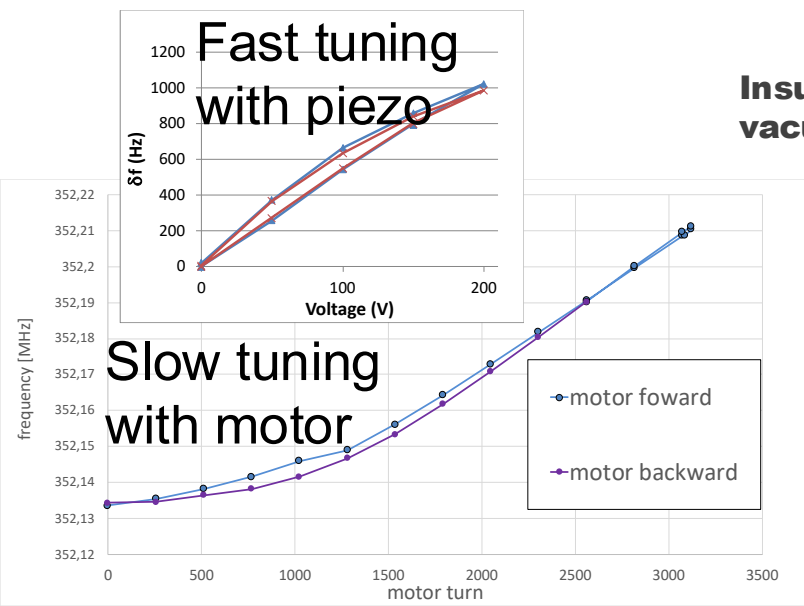
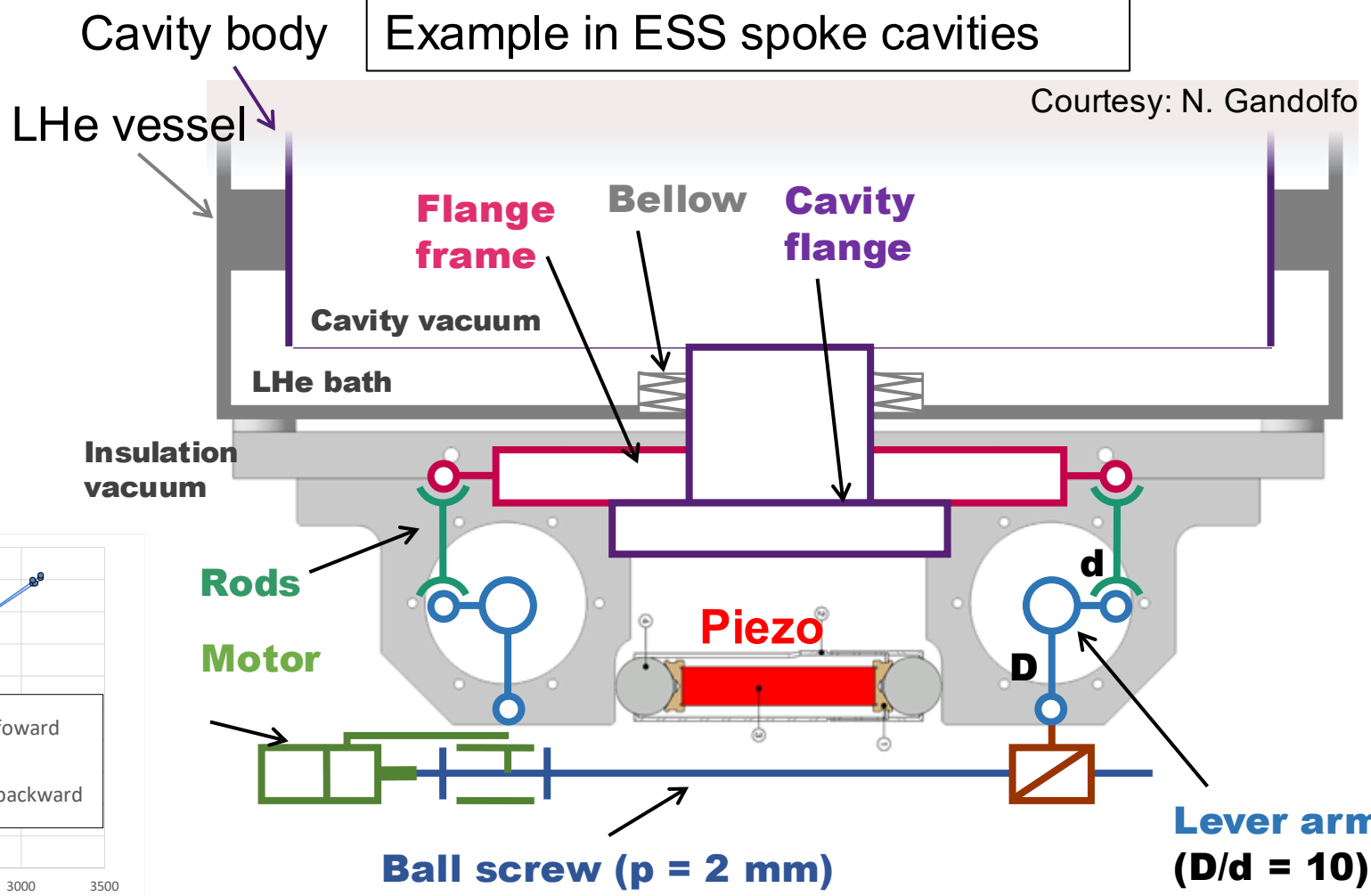
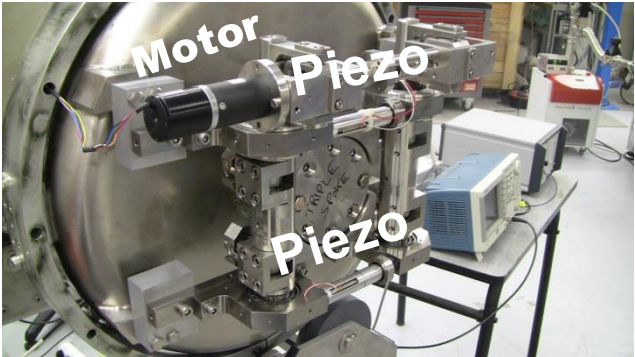
$$\frac{1}{Q_L} = \frac{1}{Q_0} + \frac{1}{Q_{ext}}$$

ESS coupler

# Cavity tuner

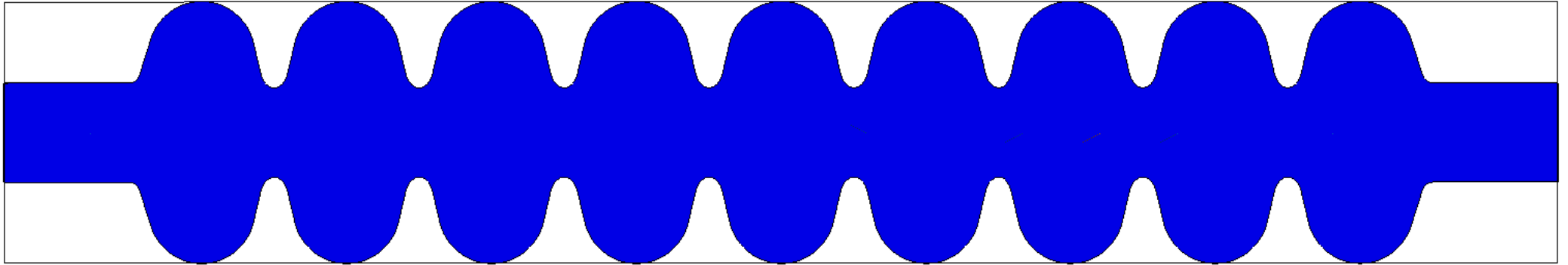
Example in ESS spoke cavities

Courtesy: N. Gandolfo





- Introduction: from DC to RF accelerator (15 min)
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- **Wake field (10 min)**
- Various shapes of RF cavities (10 min)
- Conclusion

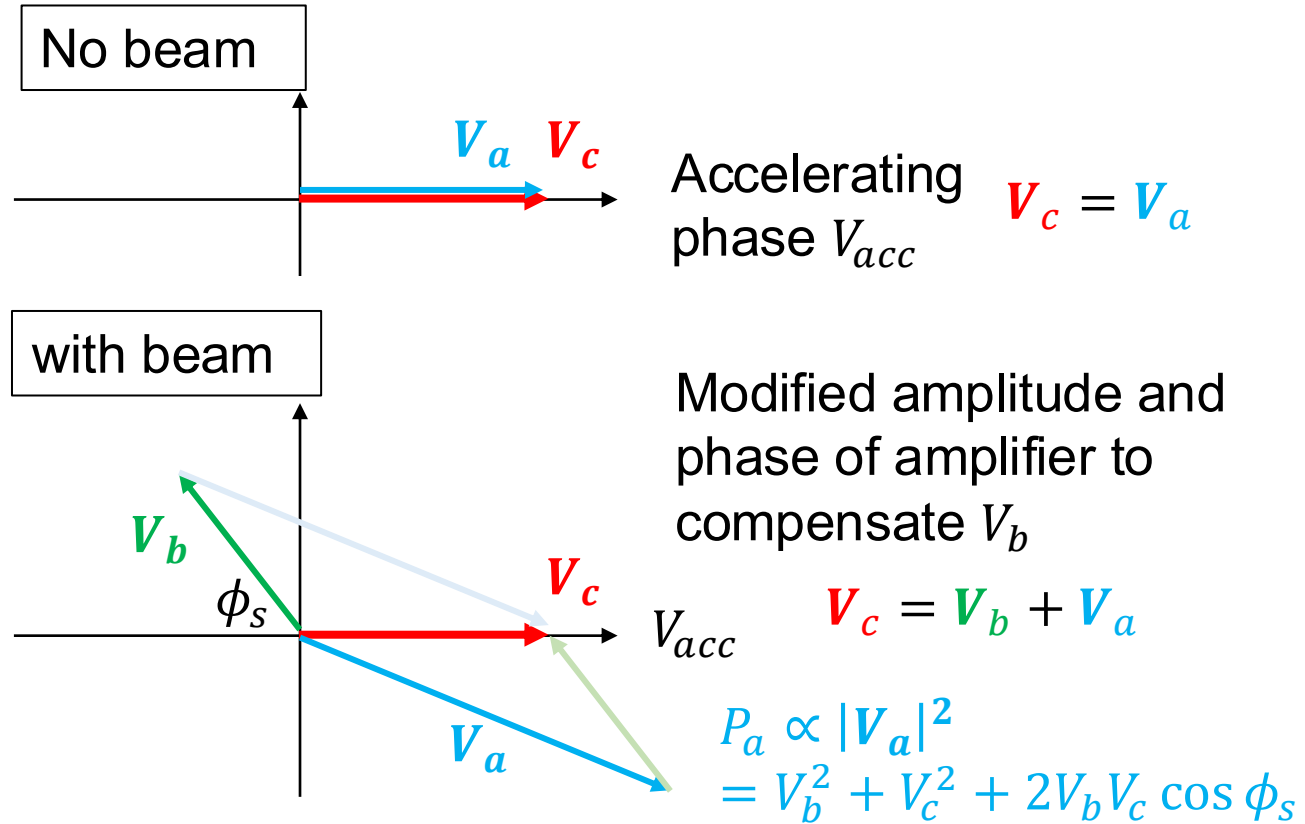
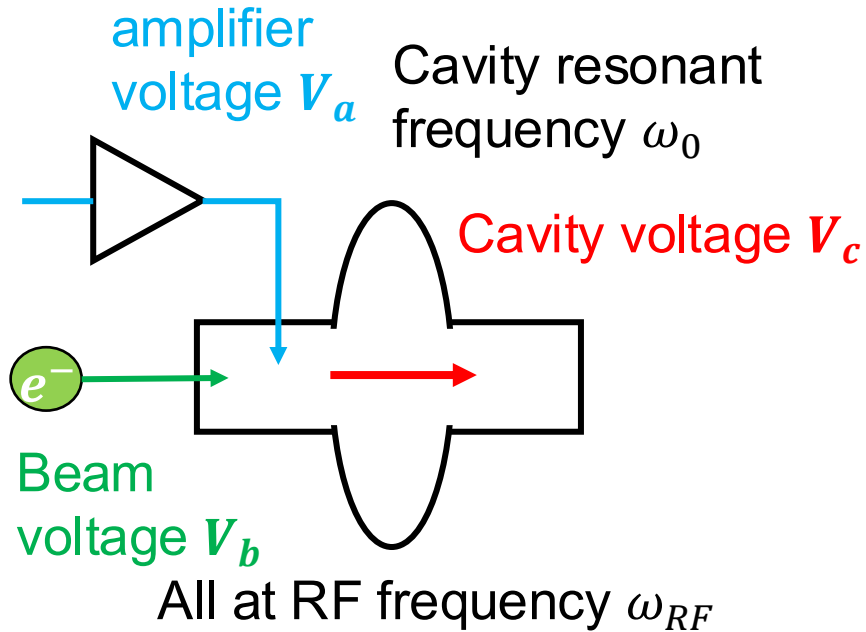


$$\left\{ \begin{array}{l} \nabla \cdot \mathbf{E} = \rho(t, \mathbf{r}) \\ \nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t} \\ \nabla \cdot \mathbf{B} = 0 \\ \nabla \times \mathbf{B} = \mu_0 \mathbf{J}(t, \mathbf{r}) + \frac{1}{c^2} \frac{\partial \mathbf{E}}{\partial t} \end{array} \right.$$

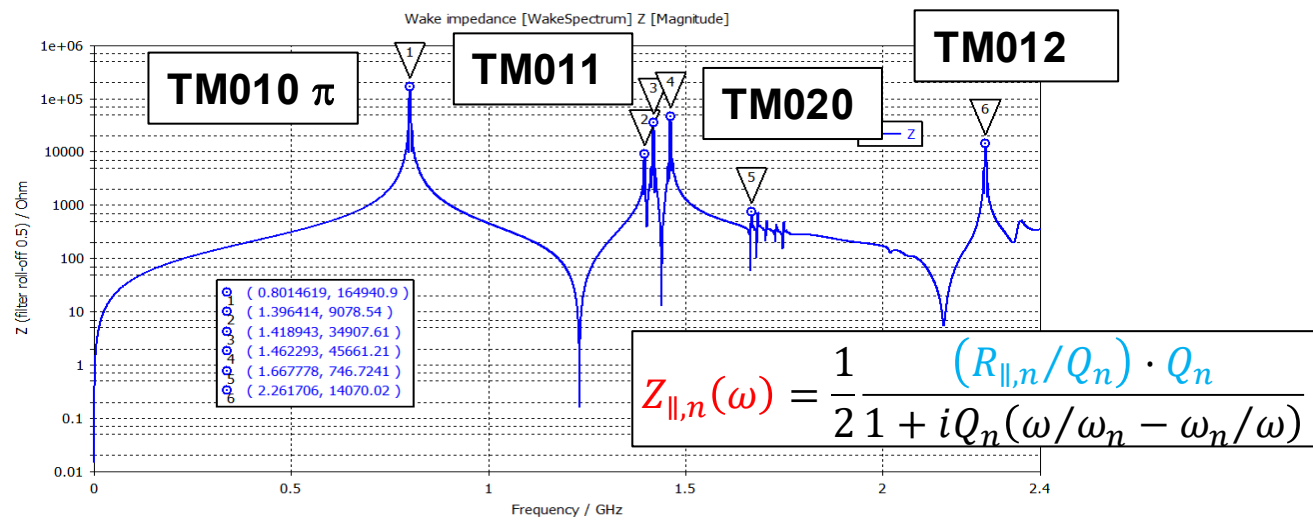
Trajectory of charged particles  $\rightarrow$  Induce RF fields

- Influence to accelerating mode (beam loading)
  - $\rightarrow$  Compensation with amplifier
- Influence to other modes
  - $\rightarrow$  kick following bunches
  - $\rightarrow$  Needs to be damped (Higher Order Mode damper)

# Beam loading

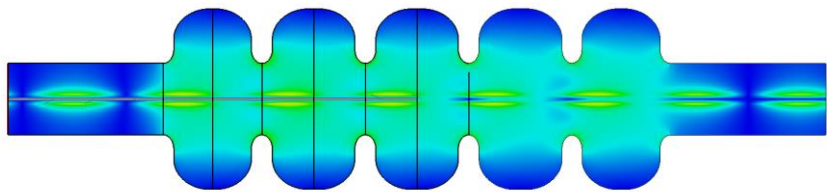


- One needs power higher than without beam to compensate the beam effect
- Further optimization: cavity detuning to save power (beyond the level of this lecture)



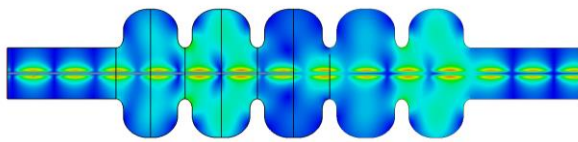
$$Z_{\parallel,n}(\omega) = \frac{1}{2} \frac{(R_{\parallel,n}/Q_n) \cdot Q_n}{1 + iQ_n(\omega/\omega_n - \omega_n/\omega)}$$

**TM010**

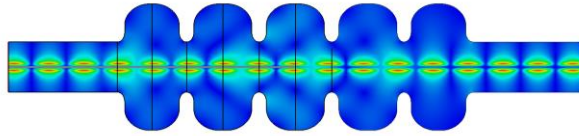


Accelerating mode in another phase → beam loading

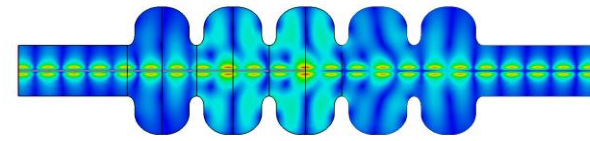
**TM011**



**TM020**



**TM012**



- Beam charge and current generate additional RF
- Some modes disturb beam → Beam instability

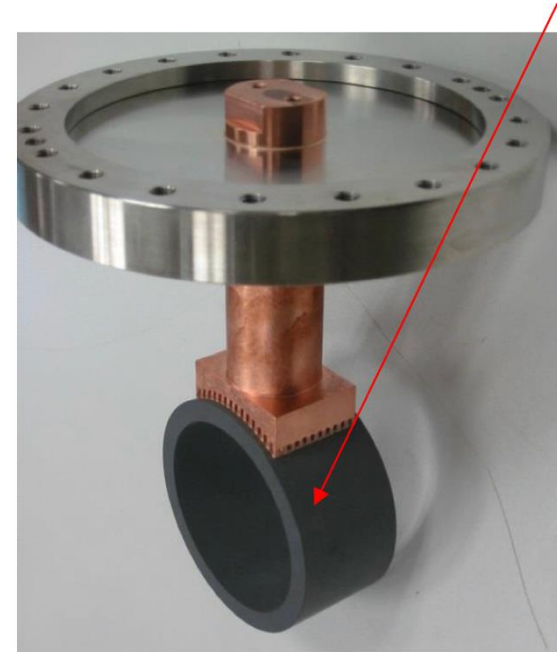
## HOM couplers



Extract HOMs outside the cavities

**Key technology in high-current accelerators**  
(LHC, FCC, SuperKEKB, PERLE, EIC, etc)

## HOM absorbers



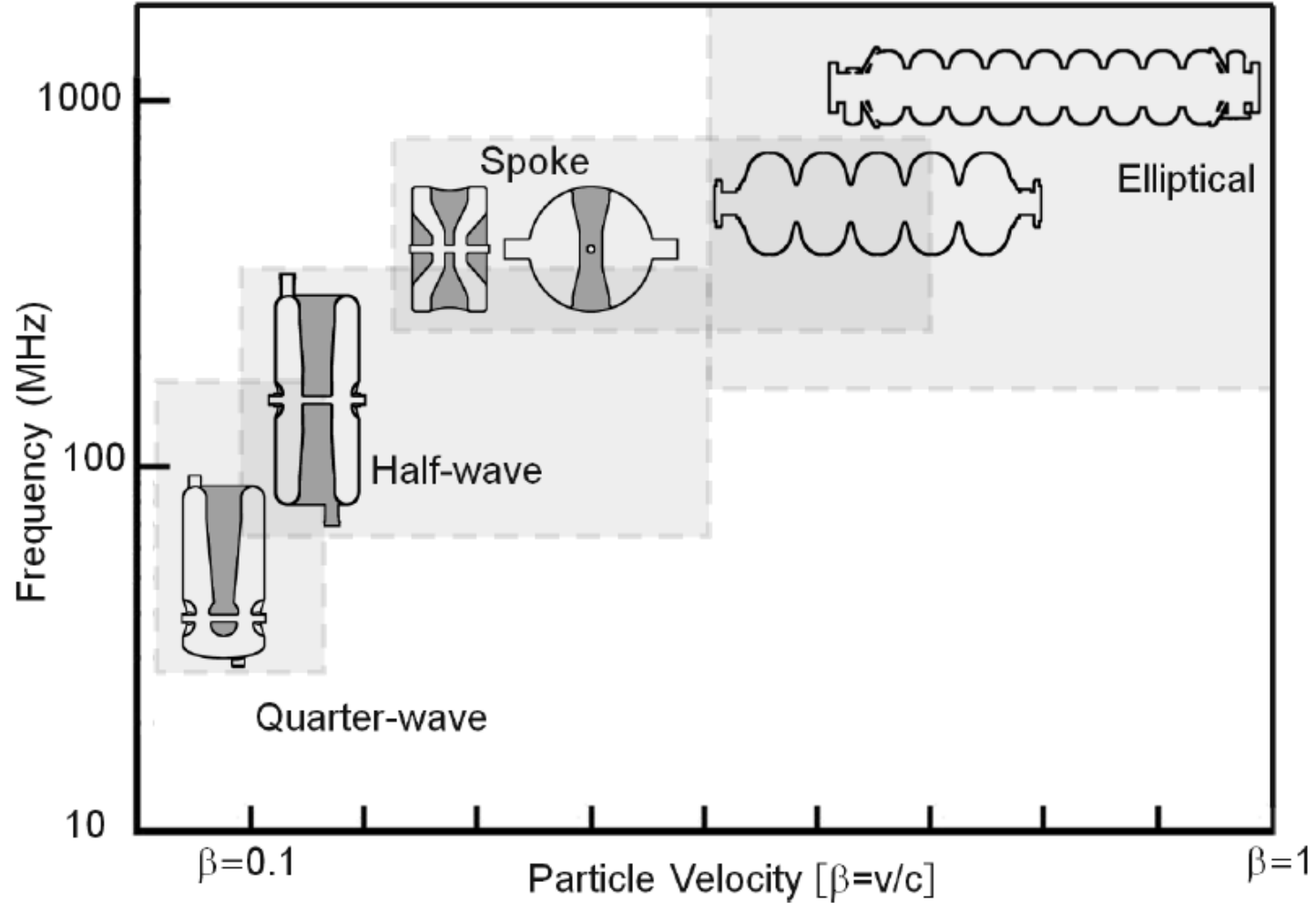
Absorbs HOMs in the beam pipe

[https://indico.fnal.gov/event/10102/contributions/813/attachments/436/508/Solyak\\_HOM\\_Absorber.pdf](https://indico.fnal.gov/event/10102/contributions/813/attachments/436/508/Solyak_HOM_Absorber.pdf)



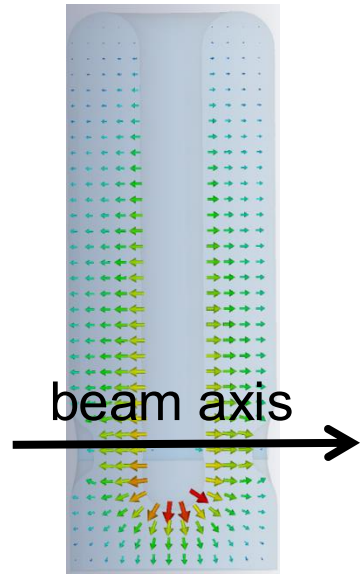
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- Conclusion

# Various shapes for acceleration

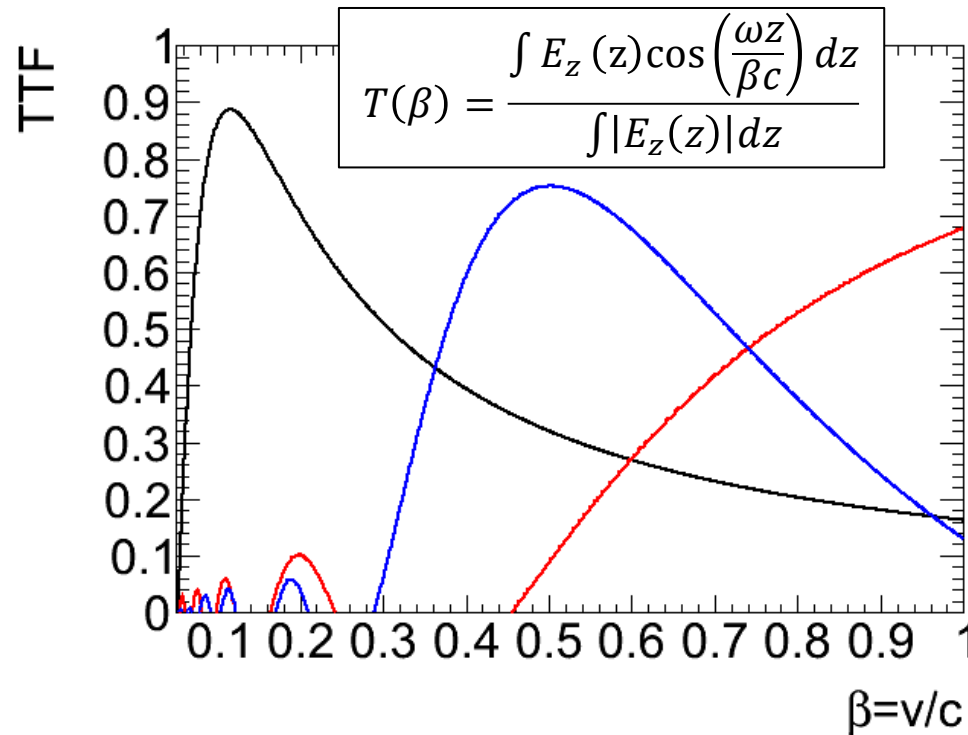


# Why different shapes? Example in cavities

TEM<sub>00</sub> modes in a quarter-wave or half-wave cavity

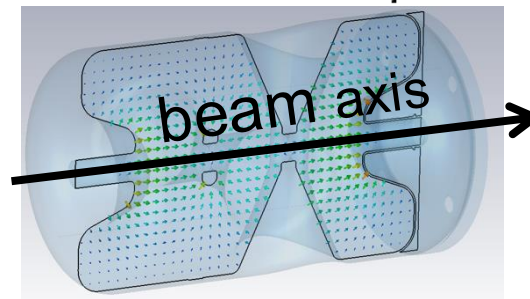


- p+ upstream (<1GeV)
- Heavy ion

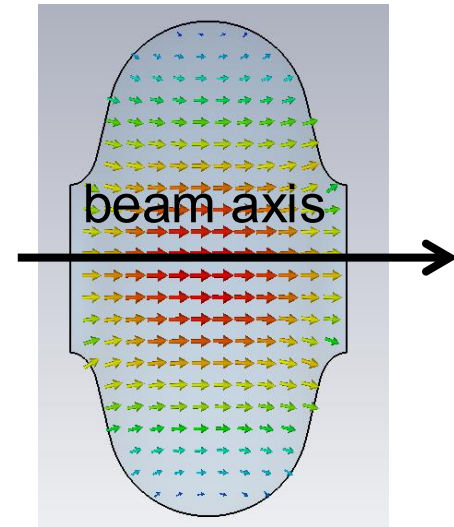


TEM modes in a spoke cavity

- p+ (<1GeV)



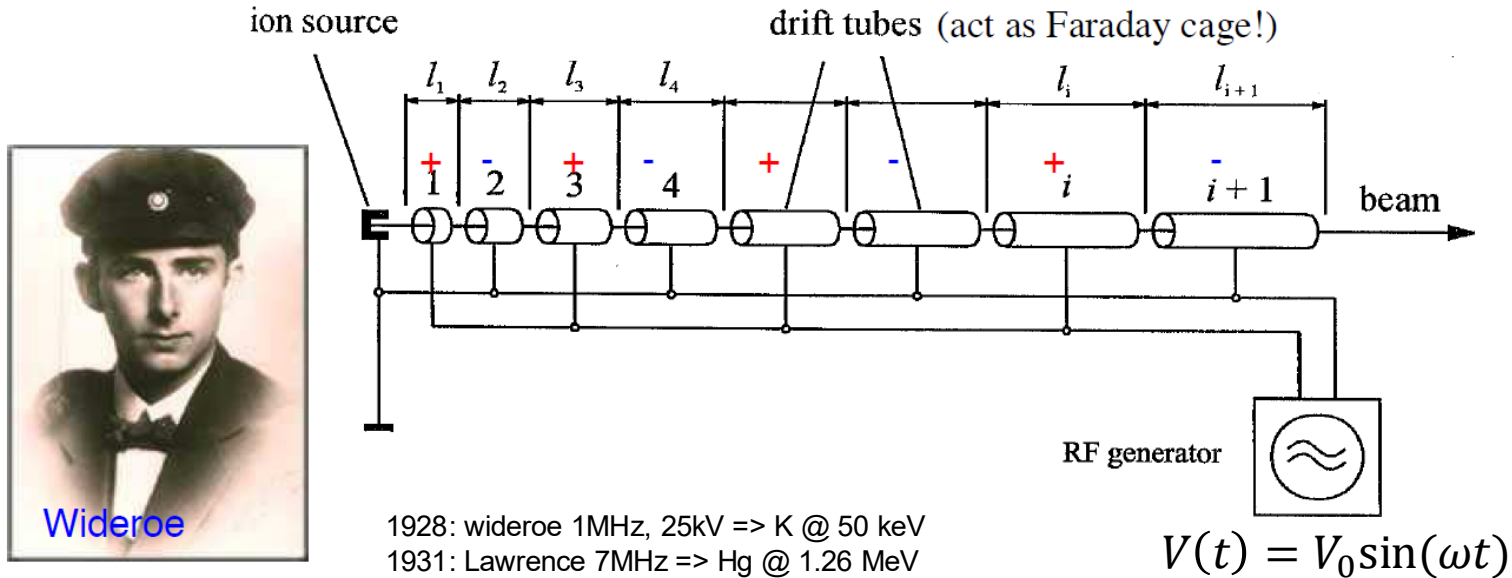
TM<sub>010</sub> modes in an elliptical cavity



- p+ downstream (>1GeV)
- e-, e+ (>0.5MeV)

# Drift tube in a space

## Wideroe structure:



For non-relativistic particles =>  $K_n = nqV_0 \sin(\varphi) = \frac{1}{2} m v_n^2$

For constant  $\varphi$  in all gaps, the distance between each at the  $n^{\text{th}}$  drift tube length:

$$l_n = v_n \frac{T}{2} = \frac{k}{2} \beta_n \lambda = \frac{\sqrt{n}}{f} \sqrt{\frac{qV_0 \sin(\varphi)}{2m}} \quad \text{Not efficient } (\pi \text{ mode})$$

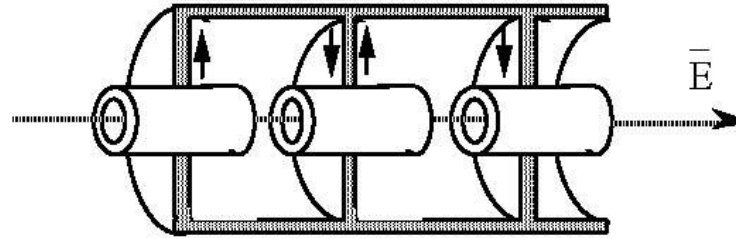
# Drift tube inside a cavity

## Alvarez structure:

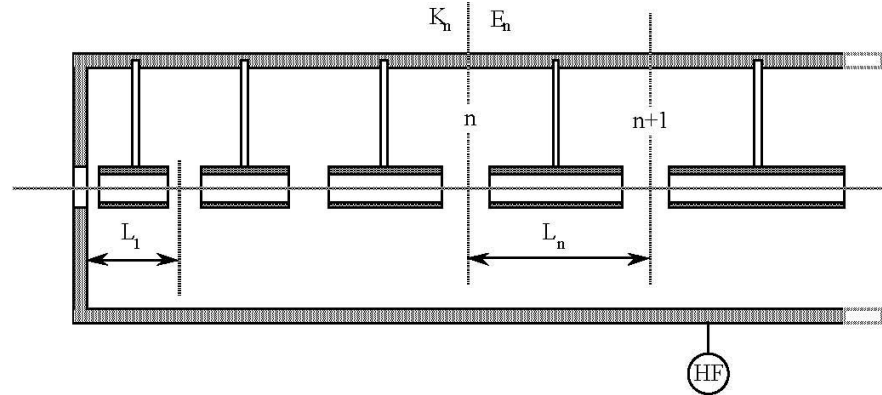
Working on  $2\pi$  mode,  $\beta = 0.1 - 0.35$ ,  $f = 100 - 500\text{MHz}$



Fermilab DTL, 425 MHz

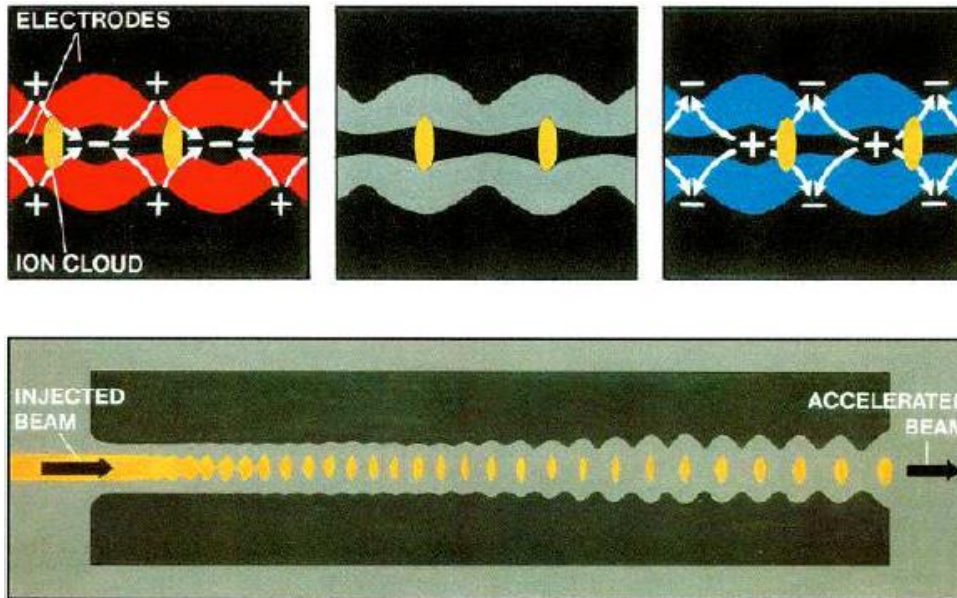


*Surface current allows removing cavity wall*



# RFQ

Efficient for very low beta particles and light ions acceleration.  
Best for  $\beta = 0.005 - 0.03$ ,  $f = 10 \sim 400$  MHz

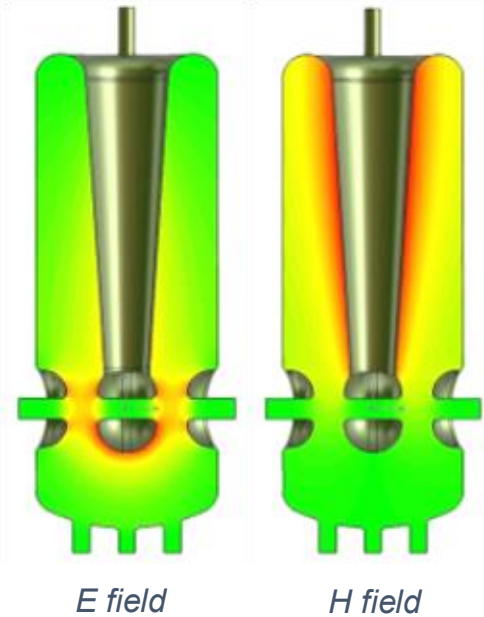


Spiral2 RFQ section, 88 MHz, 240kW  
20 keV/u  $\Rightarrow$  0.75 MeV/u, 5 mA

2 types: 4-rod (low f), 4-vane (high f)  
High acceptance, low operational cost

## QWR structures:

Low frequency, large accelerating gaps, suitable for heavy ions  $v < 0.15c$



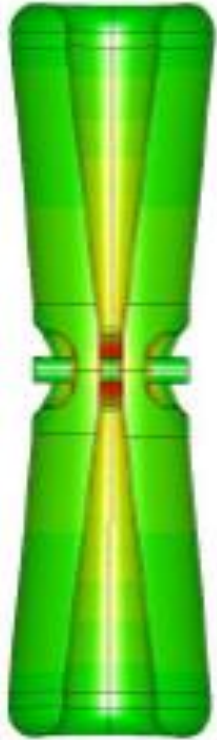
Why not high beta QWR?

- Physically large
- Strong magnetic steering on beam axis

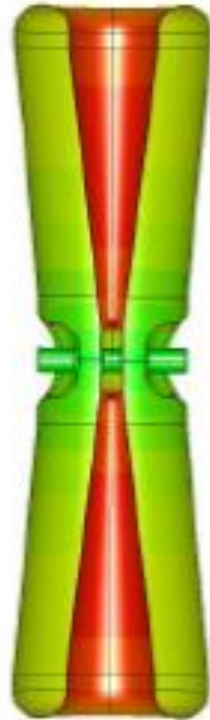


# Half-wave resonators

Low frequency, large accelerating gaps, suitable for heavy ions  $v < 0.5c$



*E field*

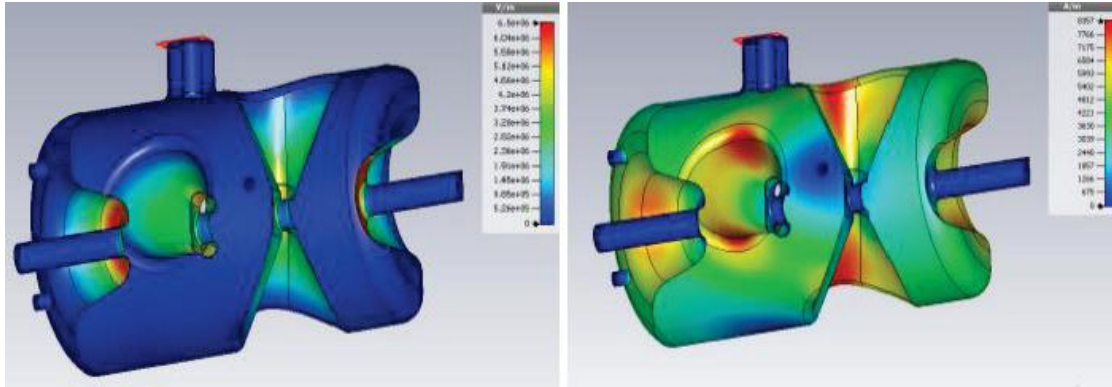


*H field*

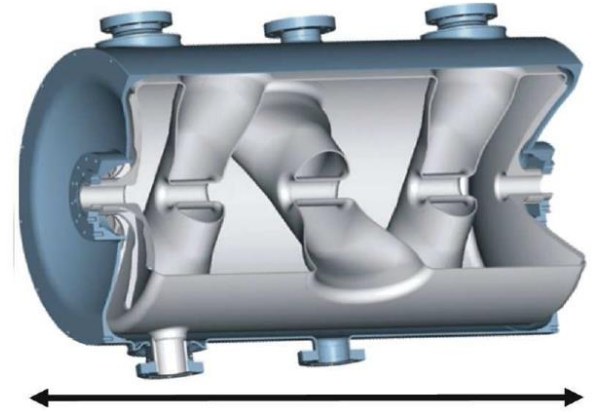


# Spoke cavities (IJCLab's speciality)

Suitable of proton with  $0.15c < v < 0.7c$



ESS 2-spoke cavity,  $\beta=0.5$ ,  $f=352$  MHz



1 m

RIA 3-spoke cavity,  $\beta=0.63$ ,  $f=340$  MHz



1<sup>st</sup> SC spoke 1991

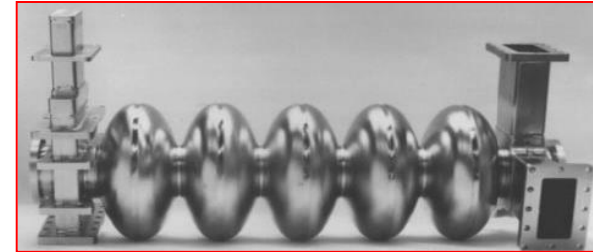


# Elliptical cavities

For relativistic particles ( $f > 1\text{GHz}$  for electrons,  $f \approx 700\text{ MHz}$  for proton).



*XFEL 9-cell cavity,  $f=1.3\text{ GHz}$*



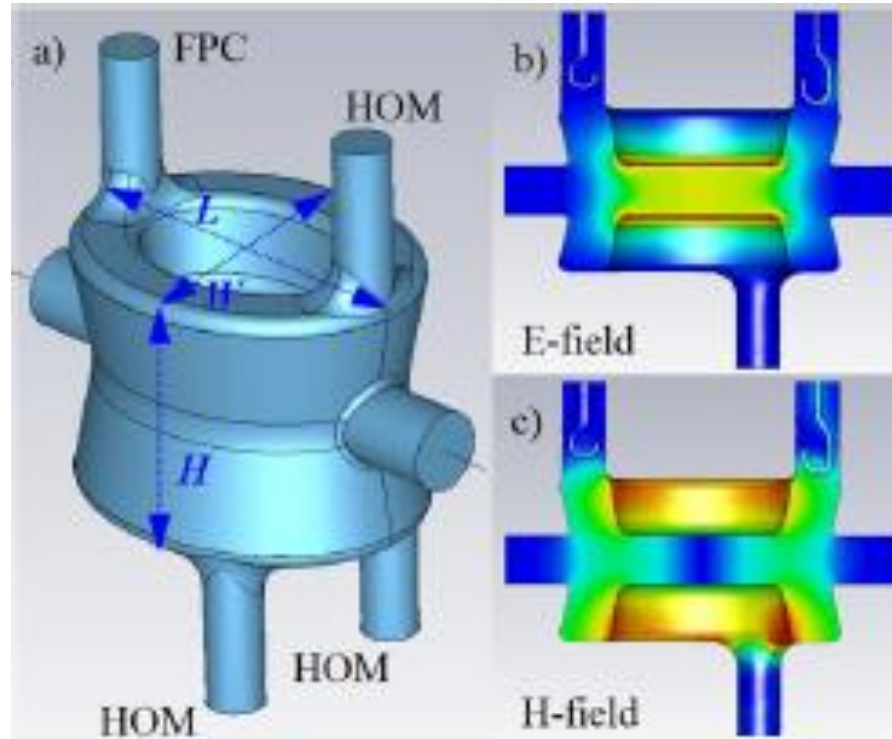
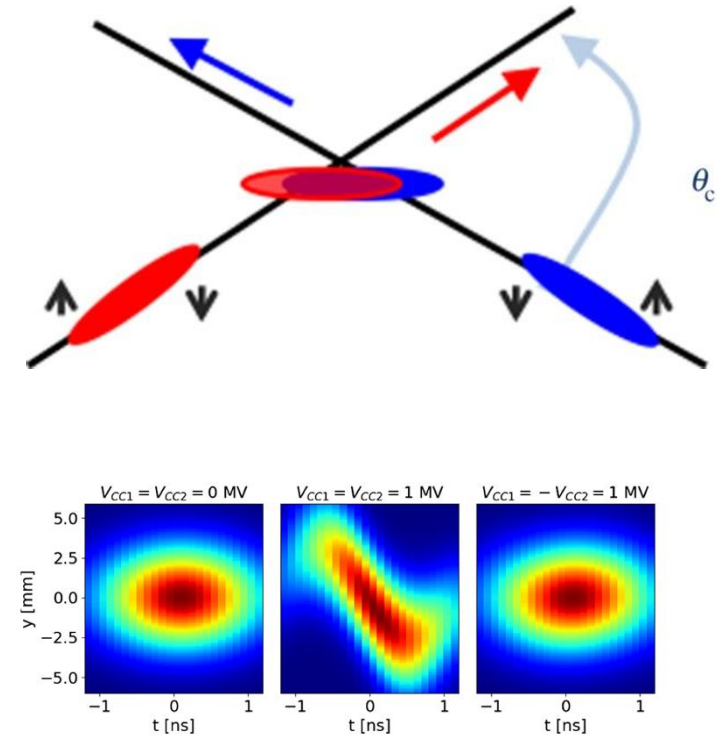
*CEBAF 5-cell cavity,  $f=1.5\text{ GHz}$*



*ILC Ichiro shape 9-cell cavity,  $f=1.3\text{ GHz}$*



*ESS 5-cell cavity,  $\beta=0.86$ ,  $f=704\text{ MHz}$*



Phys. Rev. Accel. Beams 24, 062001 2021

## For better luminosity



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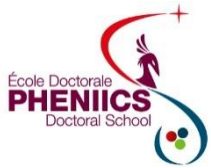


## Conclusion: *Radiofrequency Technologies for Particle Accelerators*

- DC accelerator is excellent for low energy heavy ions but with limited energy level
  - RF is a way to go beyond GeV
- RF is in short just a solution of Maxwell equations but contains rich physics and technical challenges behind it
  - Free space → waveguide → resonant cavities
  - Pill box cavity, optimized cavities, figures of merits
  - equivalent circuit, quality factor
- RF cavities are operated with ancillaries
  - control system, amplifier, coupler, tuner
- RF cavities suffer from back-action of beam: wakefield
  - Beam loading, higher order modes, handed by HOM couplers & absorbers
- Various RF cavity shape for different purpose
  - TEM type: QWR, HWR, spoke for slow particles
  - TM type: elliptical cavities for fast particles (electrons, protons in down stream)
  - Deflecting cavities: crab cavity for crabbing
- Excellent interplay of physics and engineering to enable particle acceleration!

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# *Part 2: Superconductivity and Cryogenics for Particle Accelerators*

Akira Miyazaki

Laboratoire de Physique des 2 infinis Irène Joliot-Curie  
Pôle Physique des Accélérateurs  
[akira.miyazaki@ijclab.in2p3.fr](mailto:akira.miyazaki@ijclab.in2p3.fr)



- Introduction: thermodynamics and benefit of cooling (10 min)
- Basics of cryogenics (15 min)
- BCS superconductivity (15 min)
- Non-BCS superconductivity (5 min)
- Break (10 min)
- Superconducting magnet (10 min)
- Superconducting RF cavities (20 min)
- Conclusion

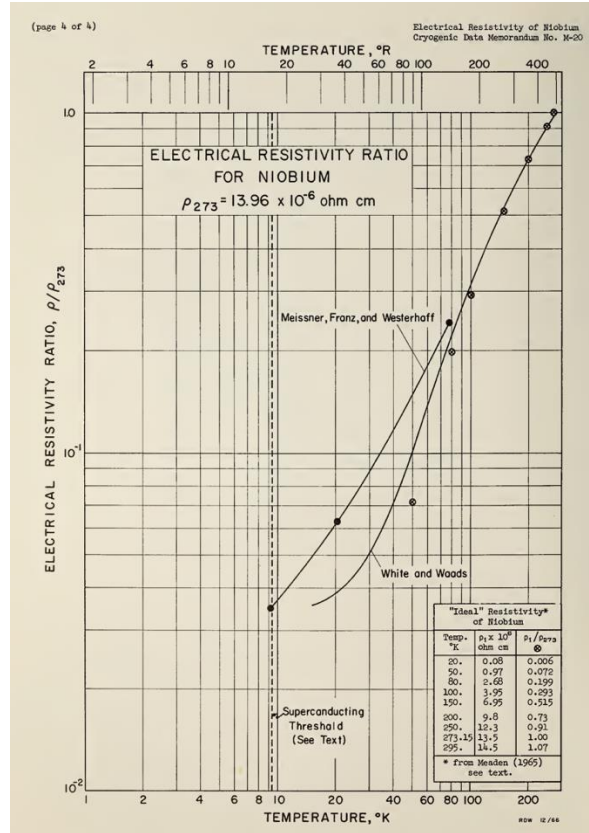
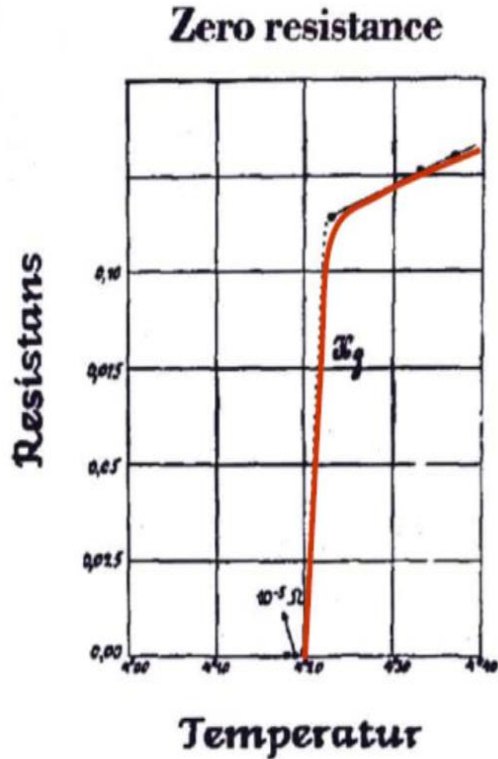


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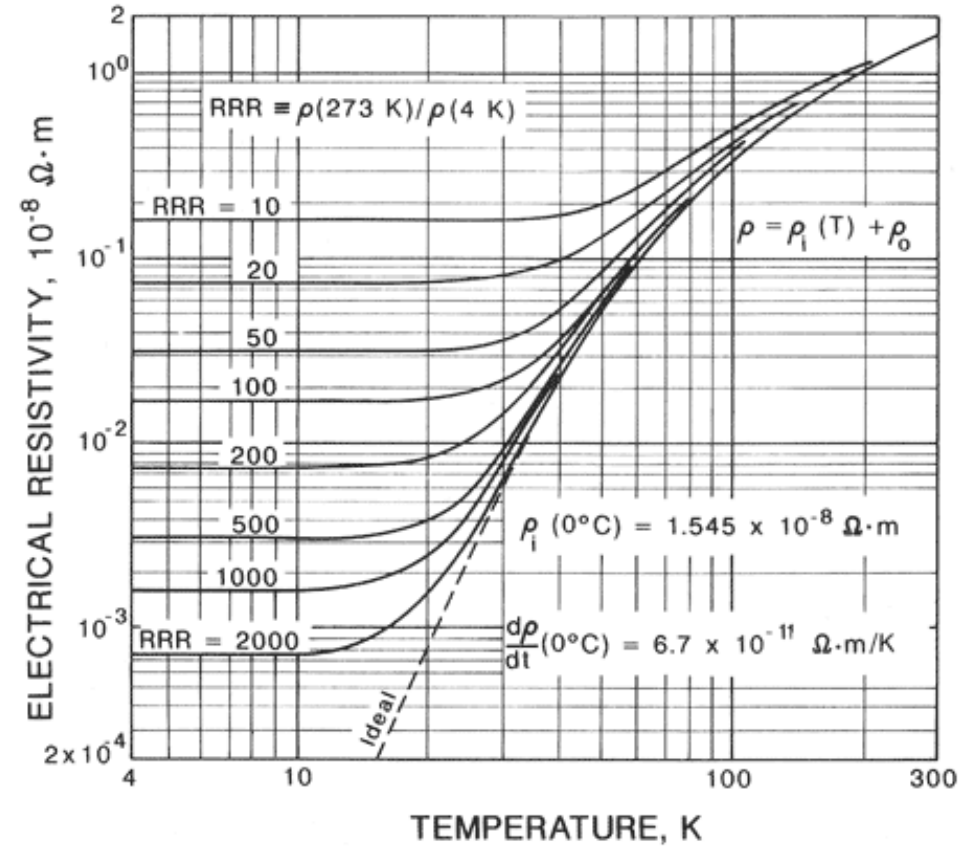
# Cooling down to reduce electric loss

## Superconducting (Hg)



<https://nvlpubs.nist.gov/nistpubs/Legacy/TN/nbstechnicalnote365.pdf>

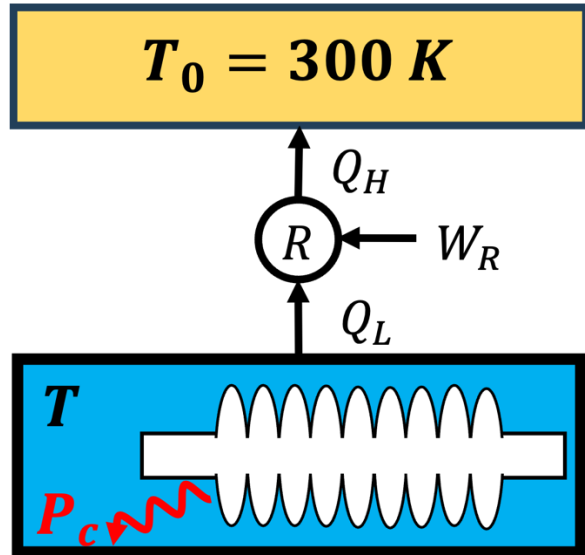
## Copper



<https://www.copper.org/resources/properties/cryogenic/>

# Cost of ideal cryogenics

Cooling power 1 W depends on temperature



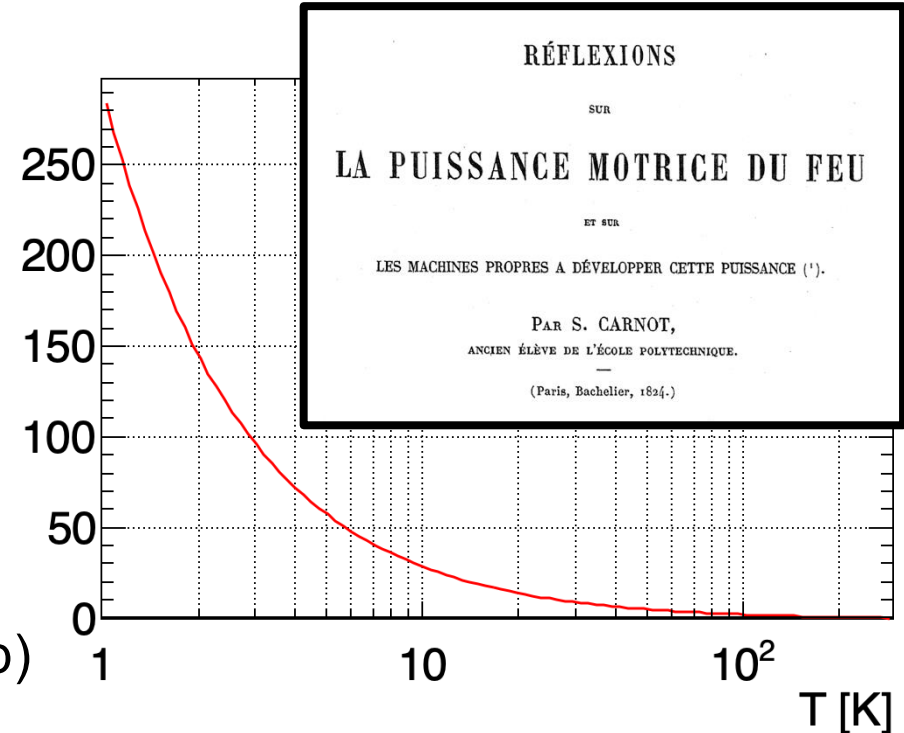
Carnot's theorem  $1/\beta$

$$\beta = \frac{Q_L}{W_R} = \frac{Q_L}{Q_H - Q_L} = \frac{T}{T_0 - T}$$

Required power

$$P_{cryo} > \frac{P_c}{\beta}$$

(be careful about logical jump)

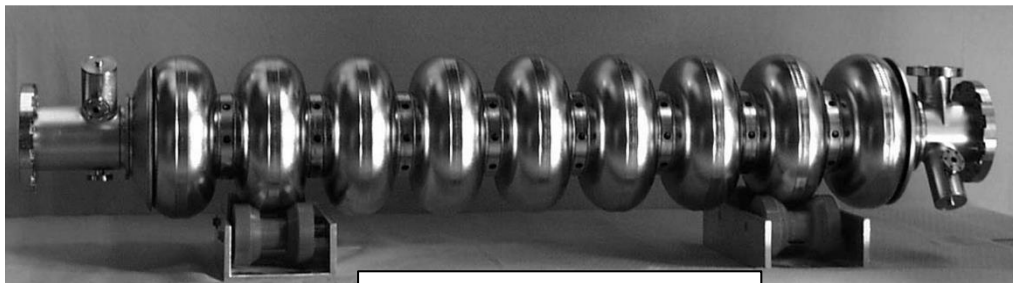


- We may need >150 W to evacuate 1 W from 2 K
- Cryogenics is an option if the resistance is improved better than this factor
  - Or some applications (eg superconductors) are not feasible at warm

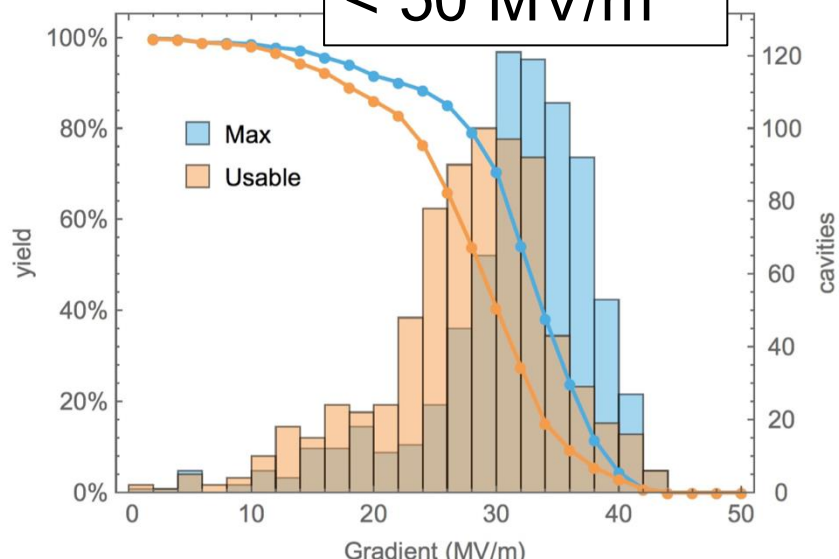


# Case study: superconducting vs normal conducting cavities

## Superconducting niobium cavities (TESLA)

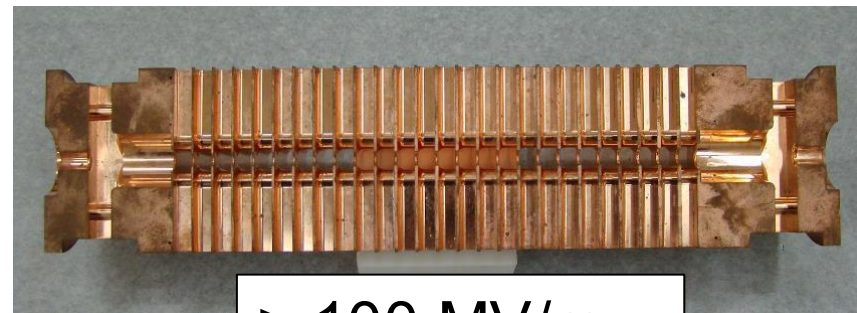


< 50 MV/m

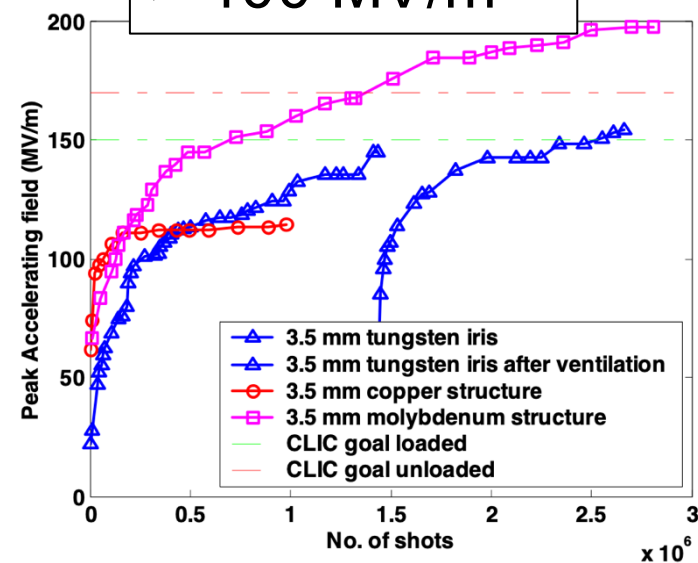


PHY REV ST - ACCEL BEAMS, **3**, 092001 (2000)  
 PHY REV ACCEL BEAMS **20**, 042004 (2017)

## Normal conducting copper cavities



> 100 MV/m



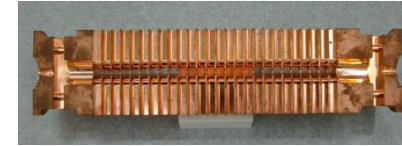
Courtesy: Walter Wuensch

> x 2

## Aperture

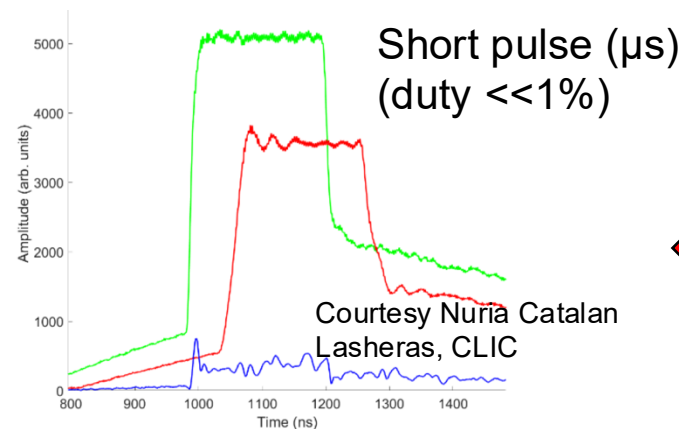
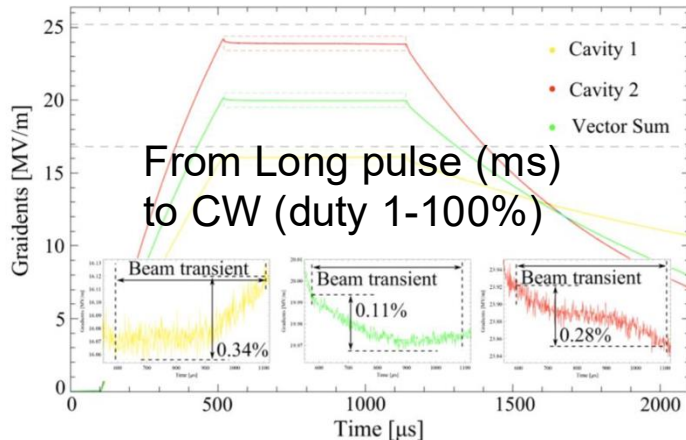


Superconducting cavities have high gradient at low frequency  
 → large aperture (ILC:  $\phi 70$  mm)



Normal conducting cavities are efficient at high frequency  
 → small aperture (CLIC X-band: around  $\phi 3$  mm)

## Pulse length and duty cycle



SC cavities' quality factor

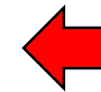
$\times 10^6$

than copper cavities

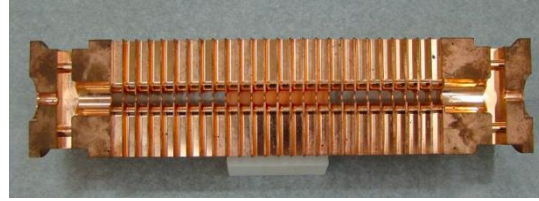
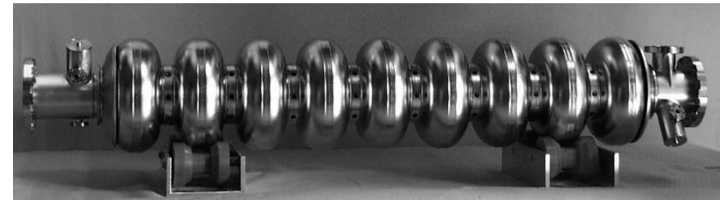
→ power dissipation

$\times 10^{-6}$

but in **cryogenics!**



# SC vs NC cavities and cooling



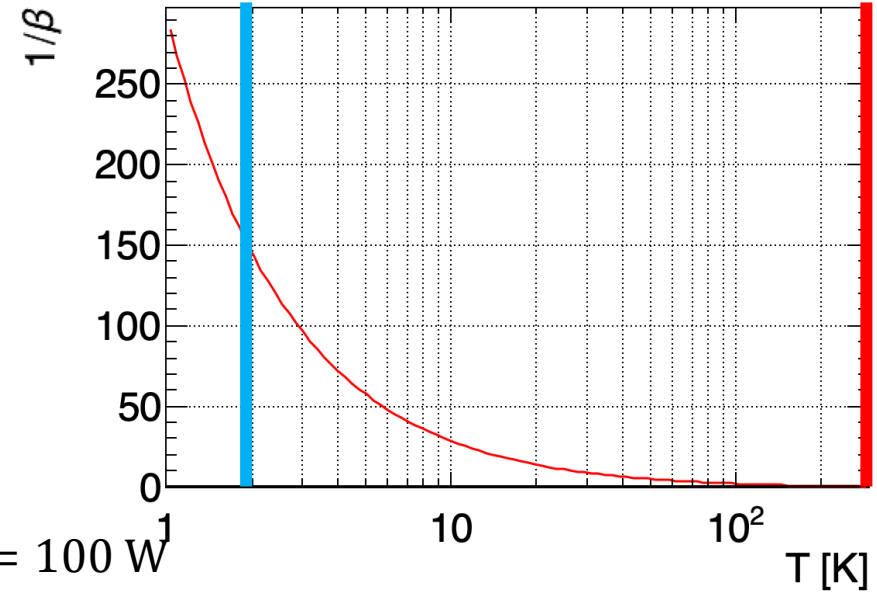
## SC cavities

$P_c = 100 \text{ W (CW)}$   
 Duty cycle  $10^{-2}$   
 $T = 2 \text{ K}$

## NC cavities

$P_c = 10 \text{ MW (CW)}$   
 Duty cycle  $10^{-5}$   
 Water cooling

$$P_{NET} \sim 100 \text{ W} \times 1\% \times 150 = 150 \text{ W} \quad P_{NET} \sim 10 \text{ MW} \times 10^{-5} \times 1 = 100 \text{ W}$$



- Short pulsed NC cavities and long pulsed SC cavities are similar in power consumption
  - If we need very long pulse or CW beam (LEP, FCCee, LCLSII) → SC cavities
  - If we need very short pulse beam (LCLS) → NC cavities
  - If we need CW but with low energy (many storage rings) → NC cavities
- Linear colliders are on the boarder: both SC (ILC) and NC (CLIC) may be OK



# Carnot cycle is unrealistic at all

Thermodynamics does not include characteristic time constant

→ Carnot cycle gives maximum efficiency in quasi-static process ( $\Delta t \rightarrow \infty$ )

→ Power (work per time) is in trade off with the efficiency

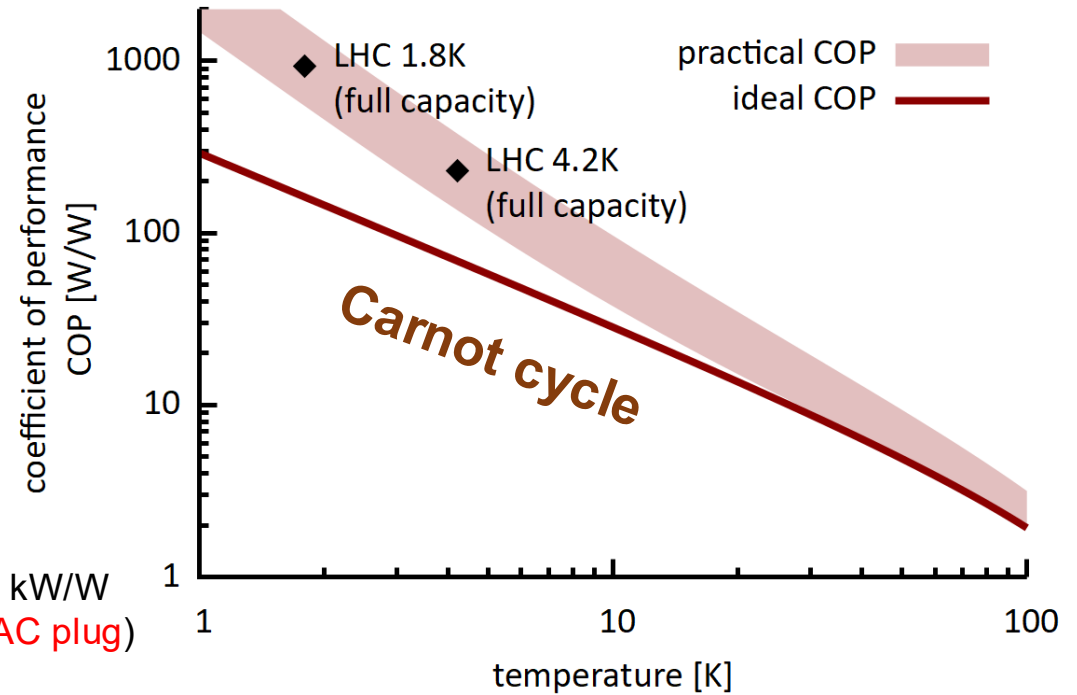
PRL117 190601 (2016)

$$P_c \leq \bar{\Theta} \beta_L \eta (\eta_c - \eta)$$

We lose useful power if efficiency  $\eta$  is too good approaching to Carnot  $\eta_c$

In addition, more practical limitations further degrade the efficiency

→ Around 1 kW is necessary to evacuate 1 W from 2 K (typically 5 kW/W @ 2 K for AC plug)



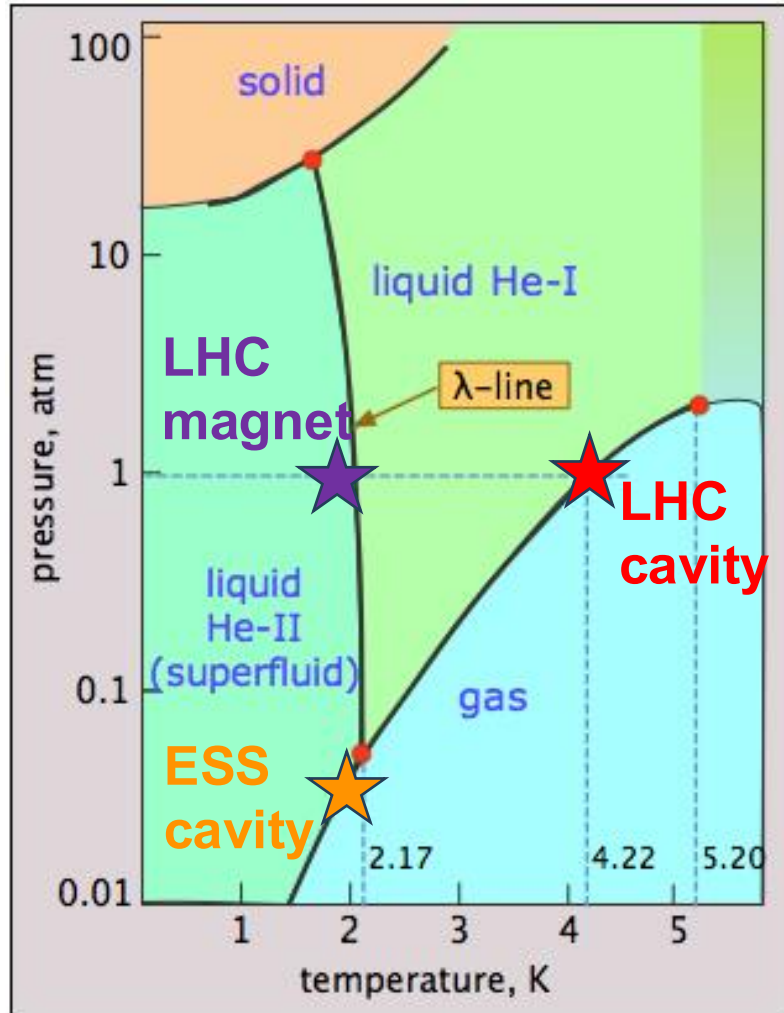
→ If the power loss of the device improves by  $>10^3$  by cooling, 2 K operation is beneficial



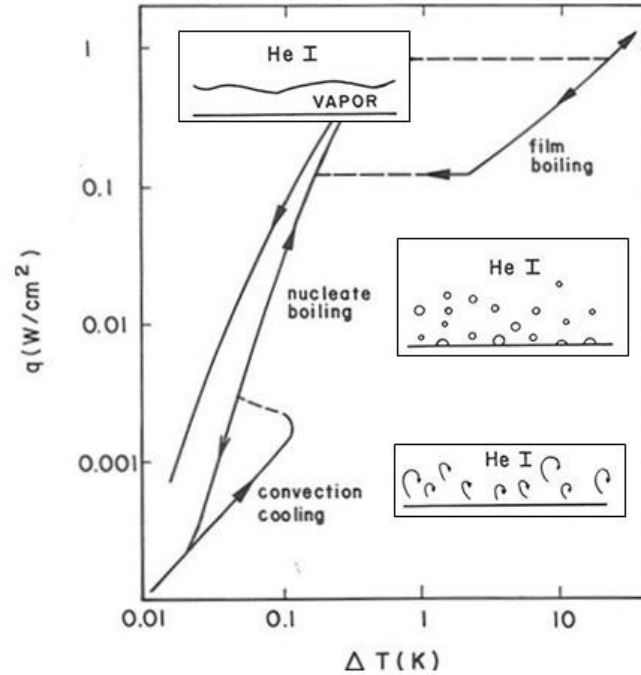
- Introduction: thermodynamics and benefit of cooling (10 min)
- **Basics of cryogenics (15 min)**
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- Non-BCS superconductivity (5 min)
- Break (10 min)
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- Superconducting RF cavities (20 min)
- Conclusion



# Cavities and magnets are in liquid helium

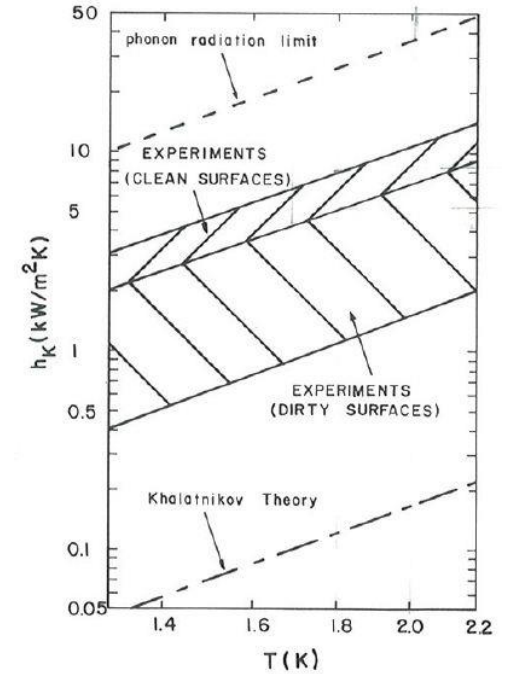


Normal helium (He-I)



**$\sim 100 \text{ W}/\text{m}^2/\text{K}$**

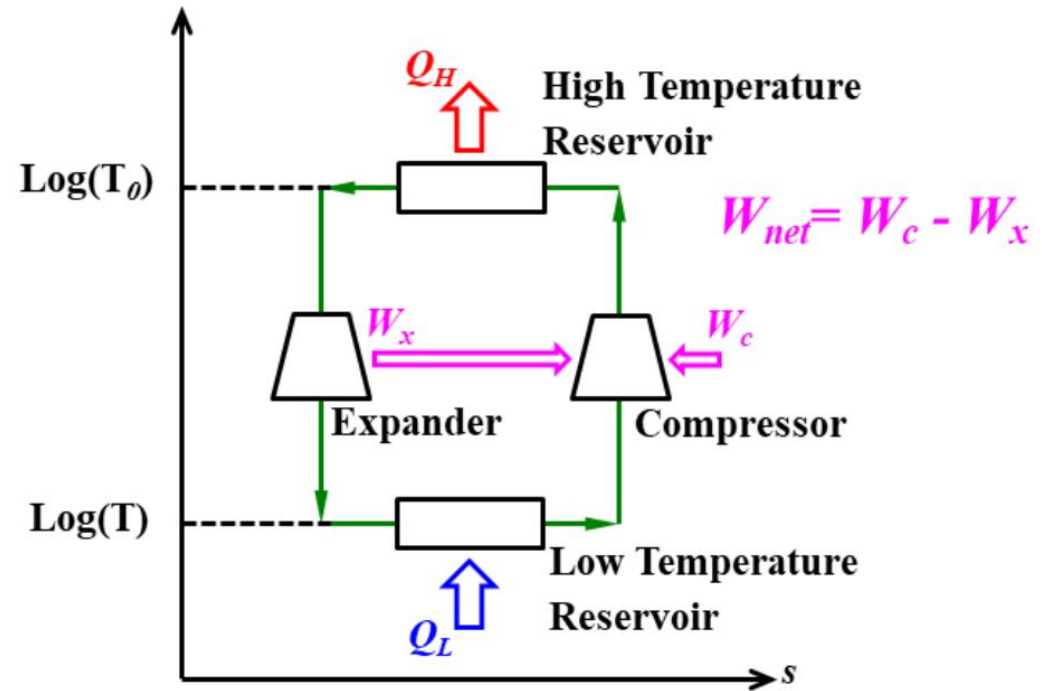
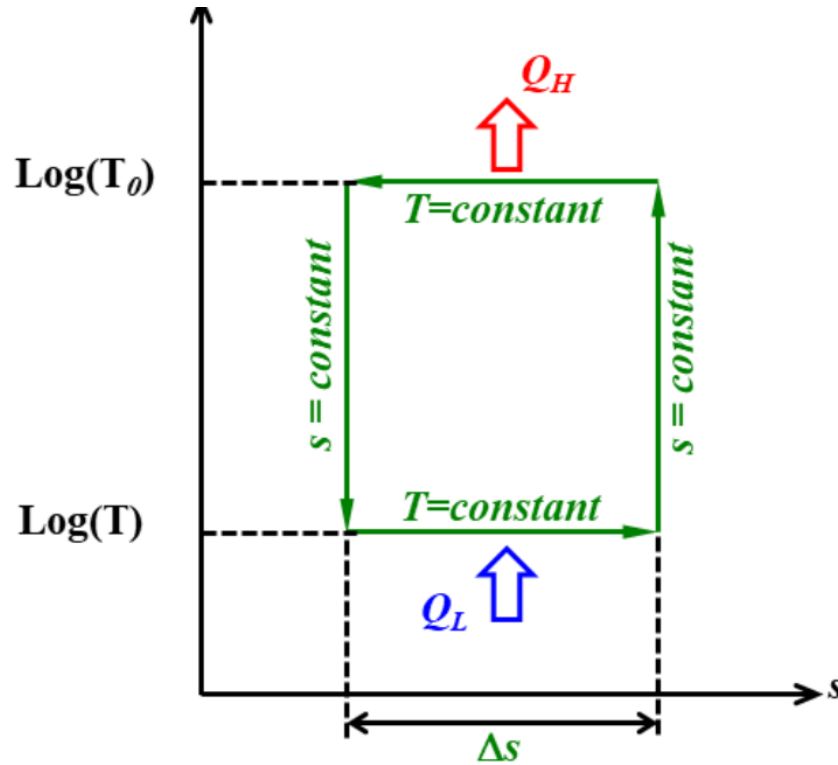
Superfluid helium (He-II)



**$\sim 5000 \text{ W}/\text{m}^2/\text{K}$**

**We need to liquify gas helium!**

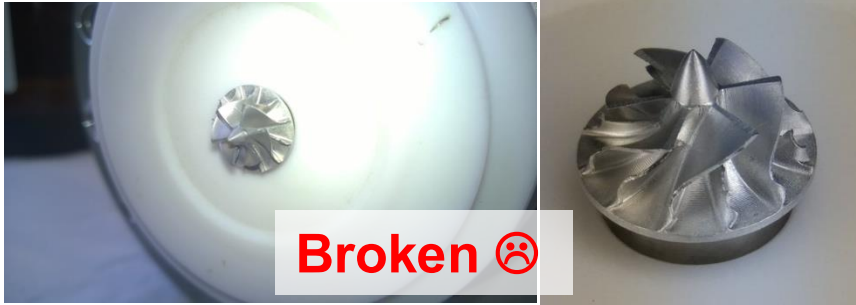
S. W. Van Sciver, "Helium cryogenics", Plenum press, 1986



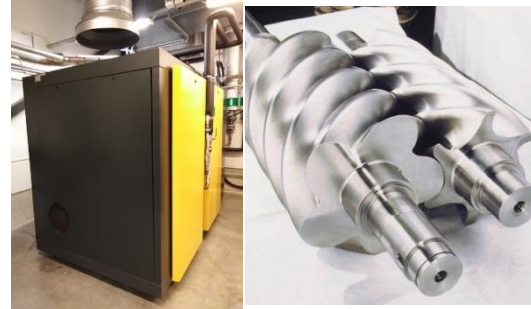
- Combination of isentropic (reversible adiabatic) and isothermal compression & expansions
- Expander & compressor are the key components
- A Carnot cycle could theoretically generate LHe but requires unrealistically high pressure

## Turboexpander (expansion turbine)

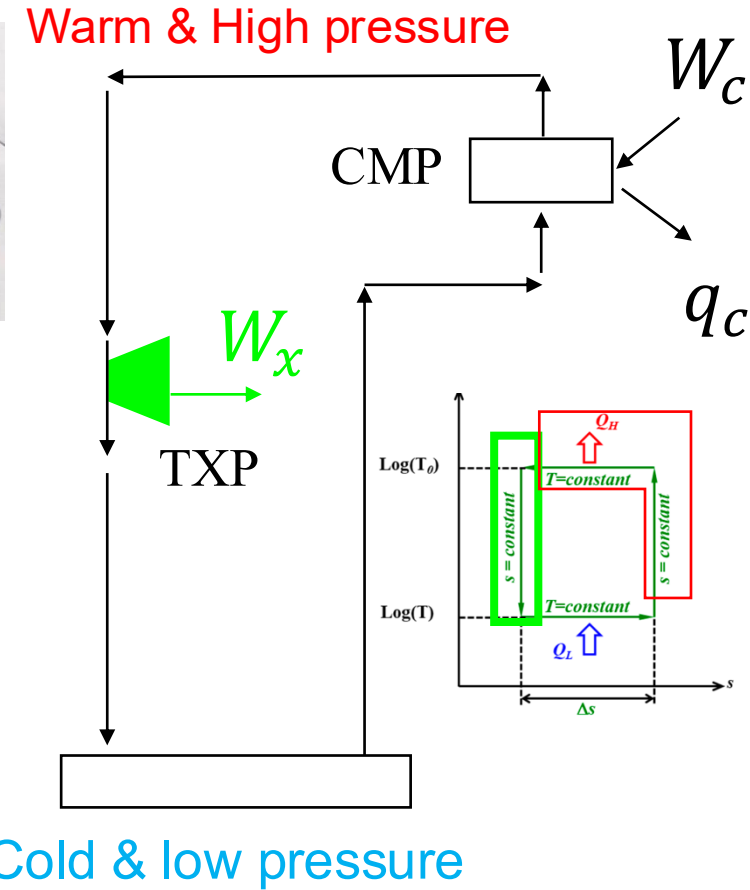
Courtesy: M. Pierens



## Compressor



## Reversed-modified Joule (Brayton) cycle

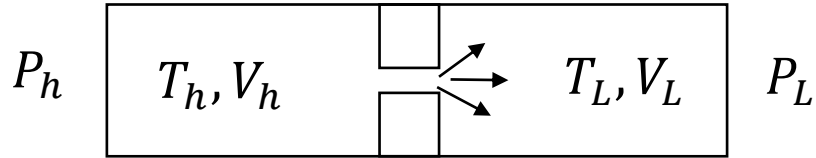


isentropic (=reversible adiabatic) expansion

### Remarks

- Isobar process  $\rightarrow$  Joule cycle  $\neq$  Carnot cycle
  - Weak points (and expensive!) of a cryogenic facility
    - If your accelerator is down, maybe one of them are out of order
  - Not used for liquefaction of helium alone practically
    - Turbine does not like LHe
- $\rightarrow$  Another process needs to be combined

Joule-Thomson (JT) process is isenthalpic (irreversible adiabatic)



$$H = U_h + P_h V_h = U_L + P_L V_L$$

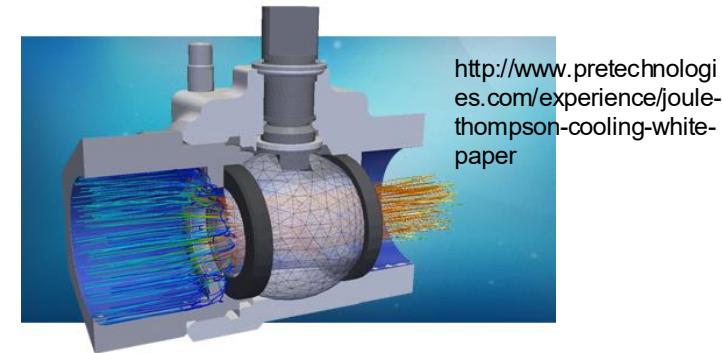
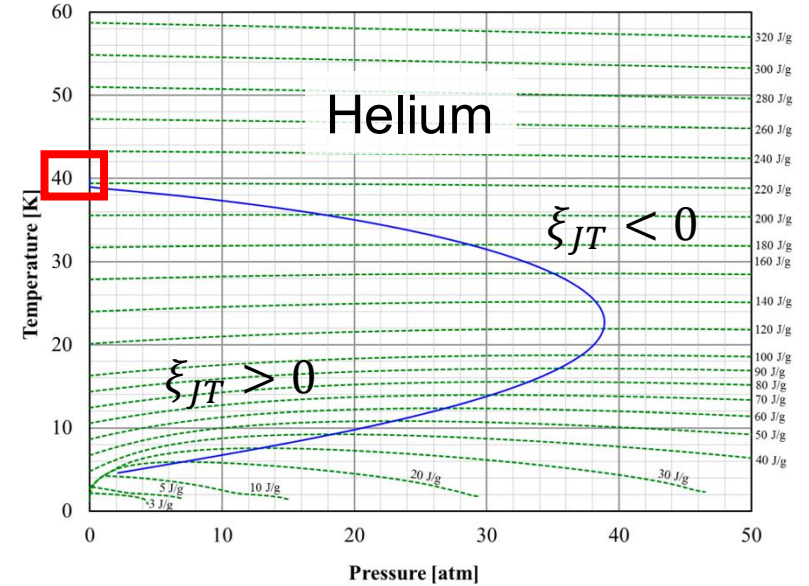
JT coefficient

$$\xi_{JT} = \left( \frac{\partial T}{\partial P} \right)_H$$

$\xi_{JT} < 0$  ( $\rightarrow T_h < T_L$ ): heating  
 $\xi_{JT} > 0$  ( $\rightarrow T_h > T_L$ ): cooling  
 $\xi_{JT} = 0$  at reverse temperature

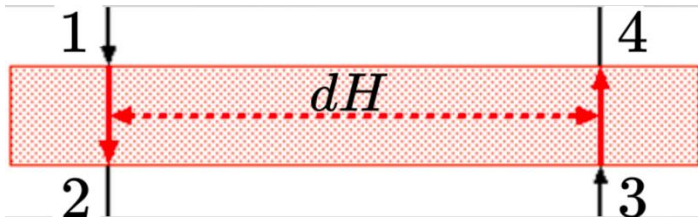
He Liquefier is made of i) compressor ii) turbine iii) JT valve

Adiabatic  $\neq$  isentropy ( $ds \geq d'Q/T$ )



Heat exchanger profits from cold return gas to enhance the liquefaction yield

$$H_4 = H_3 + dH$$



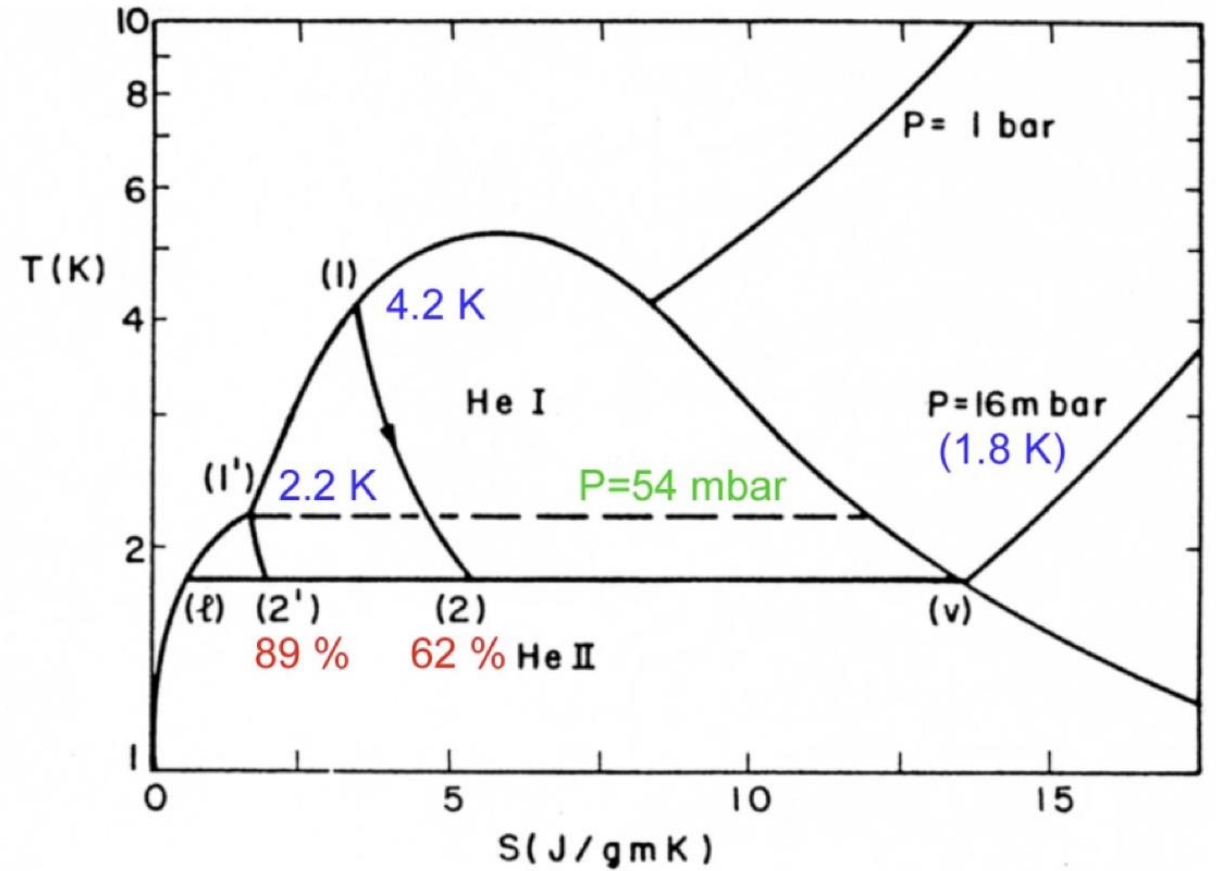
$$H_2 = H_1 - dH$$

If temperature before the JT valves is

- 4.2K → 62%
- 2.2K → 89%

Superfluid is generated by pumping down to 30 mbar

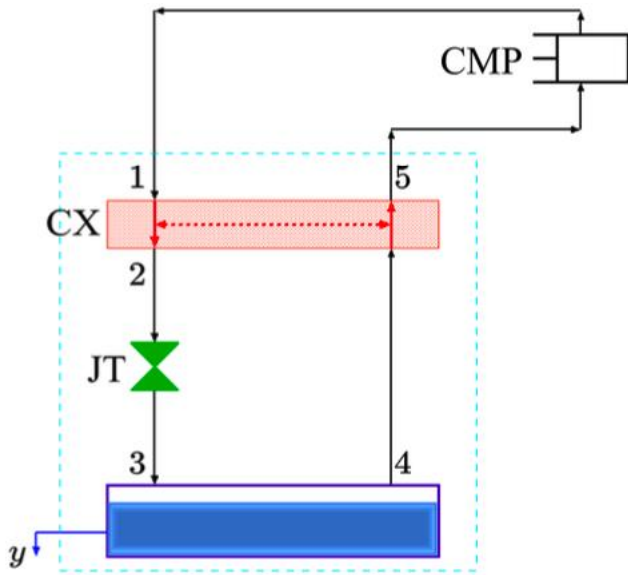
Courtesy: Elias Waagaard



Van Sciver S. W. "Helium Cryogenics", Plenum Press (1986)

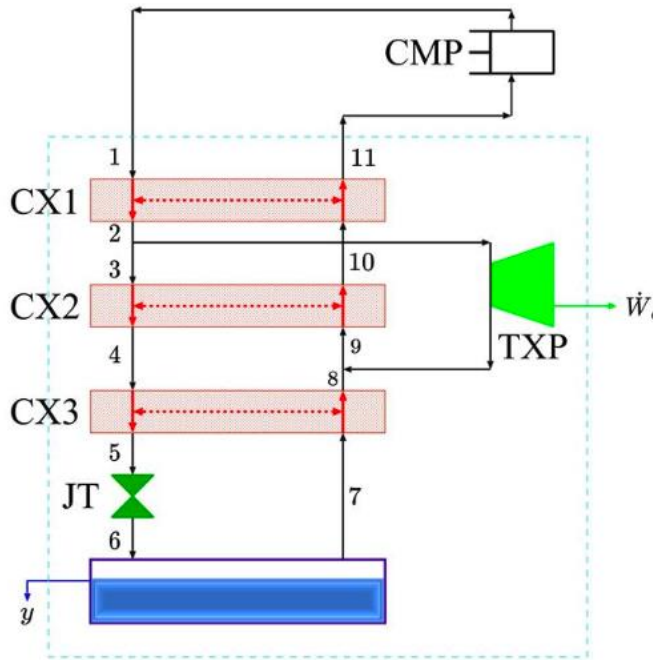


## Linde cycle



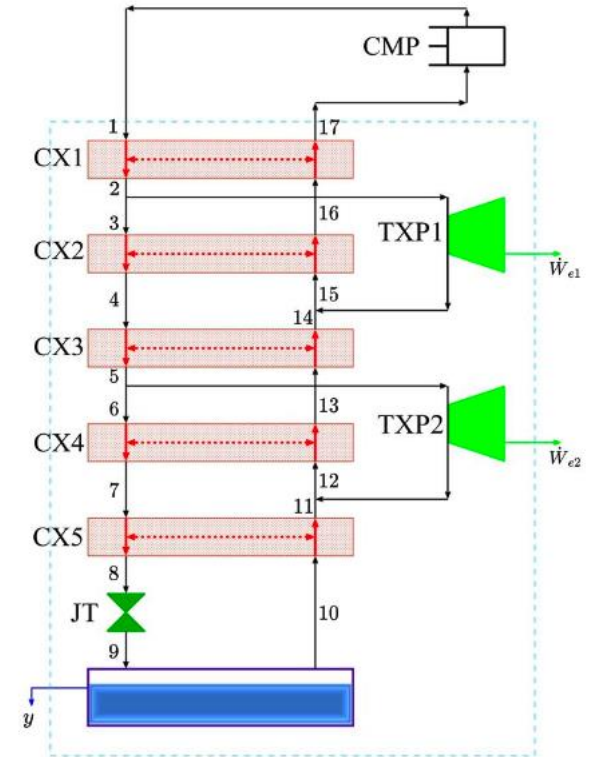
Joule-Thomson liquefaction

## Claude cycle



Joule cycle refrigeration +  
Joule-Thomson liquefaction

## Collins cycle

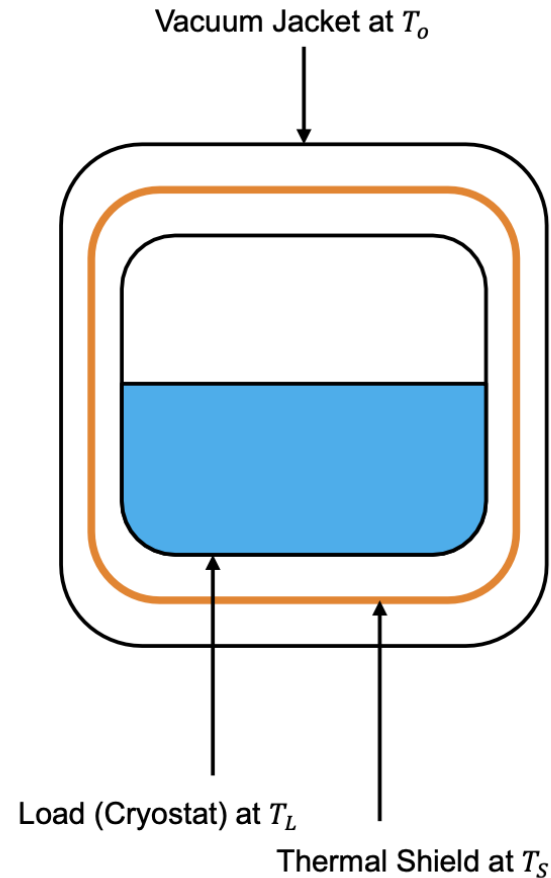
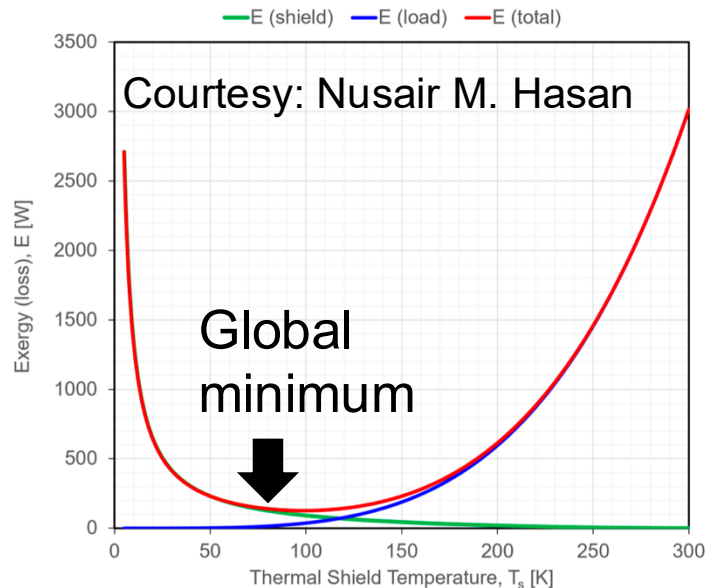


Courtesy: Elias Waagaard

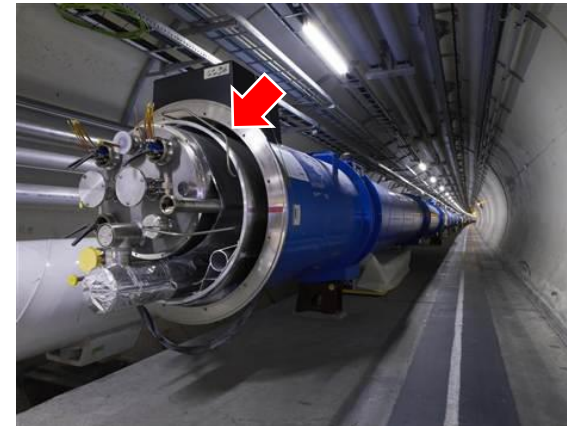


Stephan Boltzmann:  $q = \epsilon A \sigma T^4$

- Intersect the thermal radiation by intermediate temperature
- Easier to evacuate heat at higher temperature



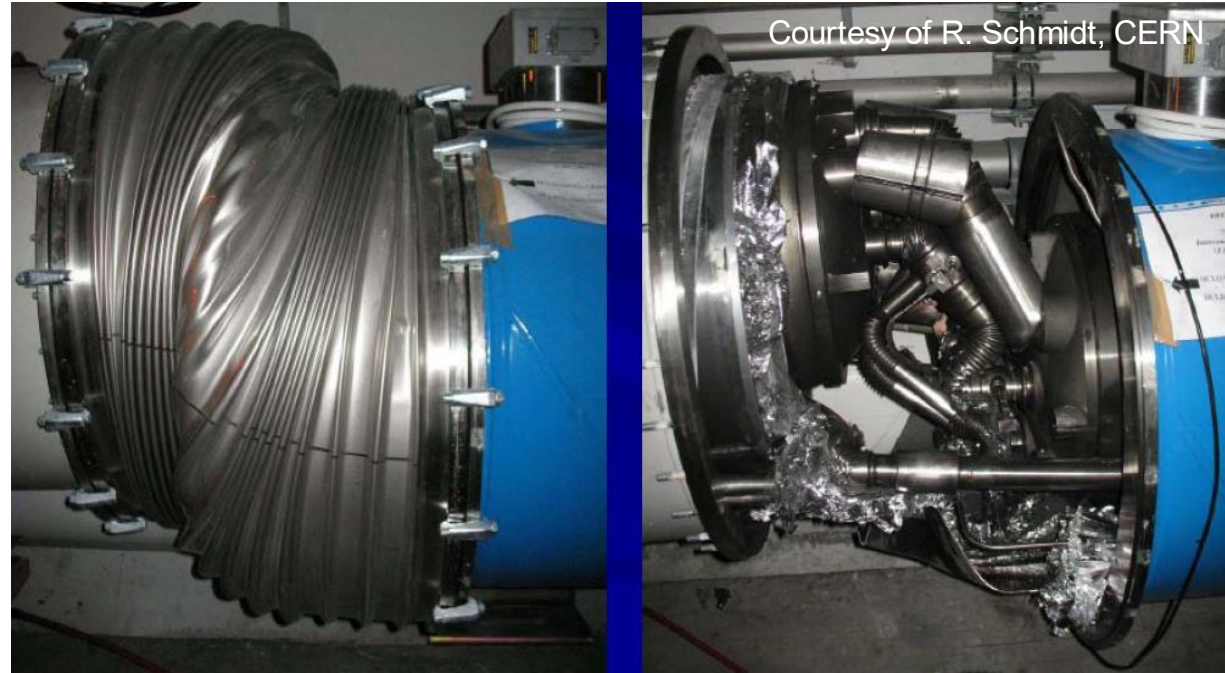
## Multilayer Insulation (MLI)



LHC dipole

## 3 months after I got a staff position

## 3 months after I started PhD in particle physics



High power RF → SC cavity quenched by multipacting → wrong interlock setup → Overpressure in LHe → Rupture disk burst → no mechanical damage

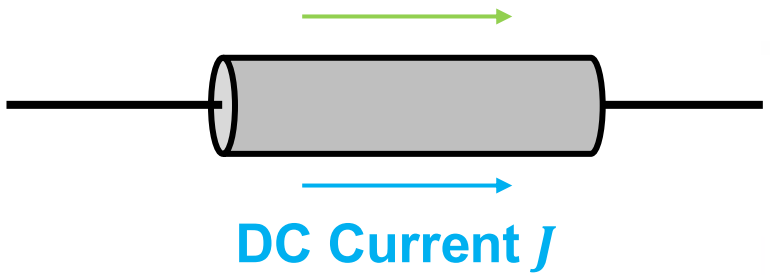
Defect in soldering joint → resistive (magnet quench itself was NOT the trigger) → Electrical arc → He goes into isolation vacuum → helium boiled off → mechanical damage



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## Ohm's law

Applied DC electric field  $E$



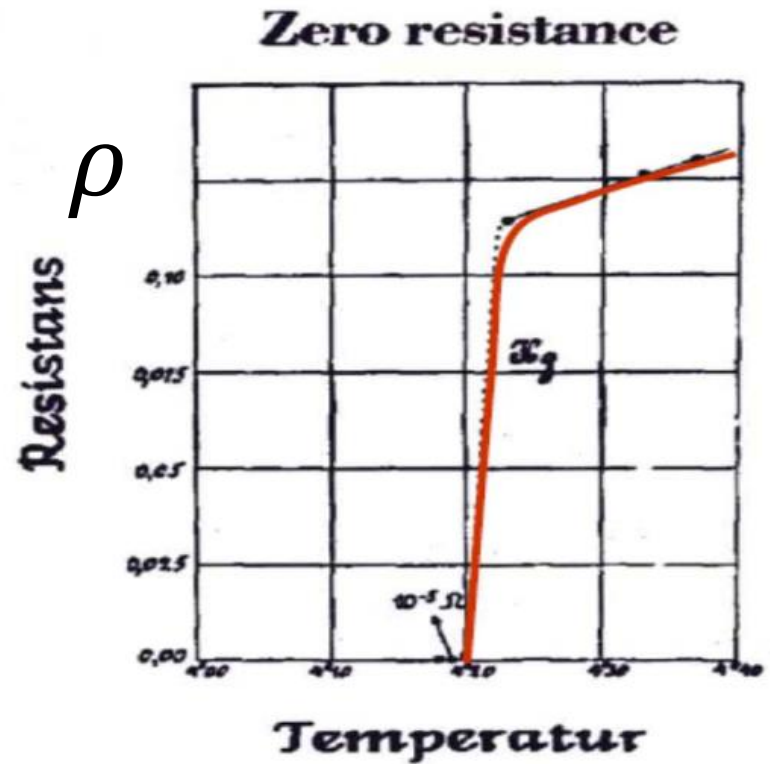
DC resistivity  $\rho$

$$\rho \equiv \frac{E}{J}$$

DC conductivity  $\sigma$

$$\sigma = \frac{1}{\rho} \equiv \frac{J}{E}$$

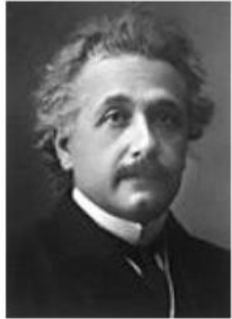
Cool down the resistor...



Heike Kamerlingh Onnes  
Nobel prize in 1913

$\rho = 0$  below transition temperature  $T_c$

J. Schmalian, arxiv:1008.0447



Albert Einstein  
(1879-1955)



Niels Bohr  
(1885-1962)



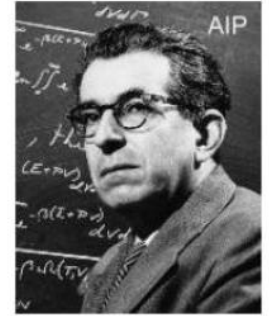
Ralph Kronig  
(1905-1995)



John Bardeen  
(1908-1991)



Werner Heisenberg  
(1901-1976)



Fritz London  
(1900-1954)



Lev D. Landau  
(1908-1968)



Felix Bloch  
(1905-1983)



Léon Brillouin  
(1889 -1969)



Max Born  
(1882-1970)



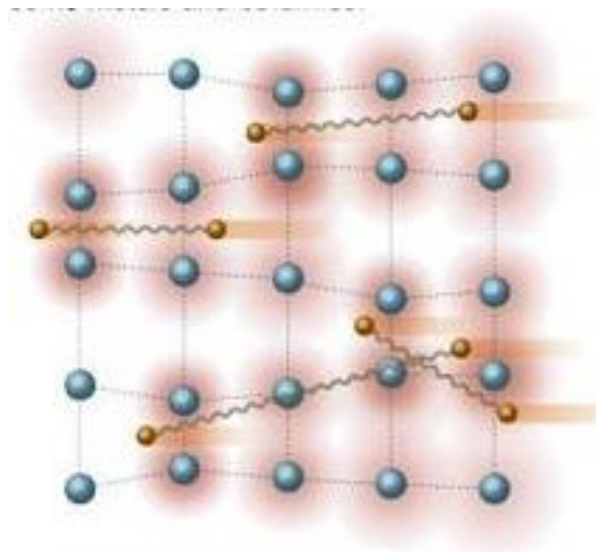
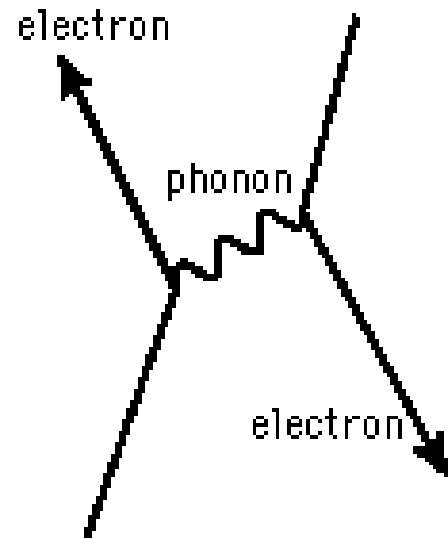
Herbert Fröhlich  
(1905-1991)



Richard Feynman  
(1918-1988)

A lot of models...all failed ☹️

Development of quantum field theory in many body problems was necessary...



John Bardeen



Leon Cooper



John Robert Schrieffer

## Cooper pair: Composite boson

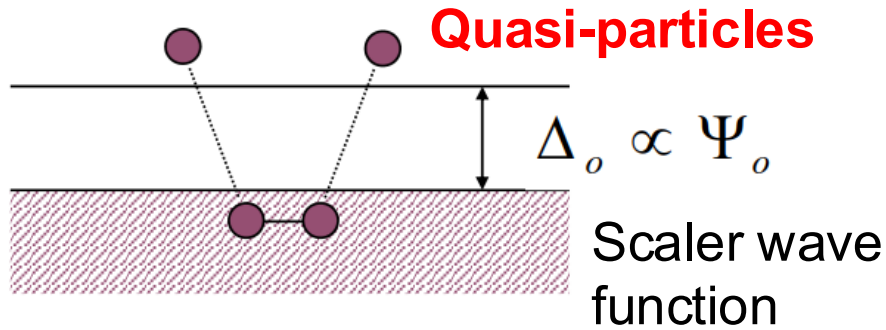
Two electrons are bounded by something (phonon)  $\rightarrow$  effective Hamiltonian  $\mathcal{H}_{BCS}$

Mean field approximation + Variational method (+other approximations...)

$$\mathcal{H}_{BCS}|\Phi_0\rangle = E|\Phi_0\rangle$$



# Solution: superconducting gap



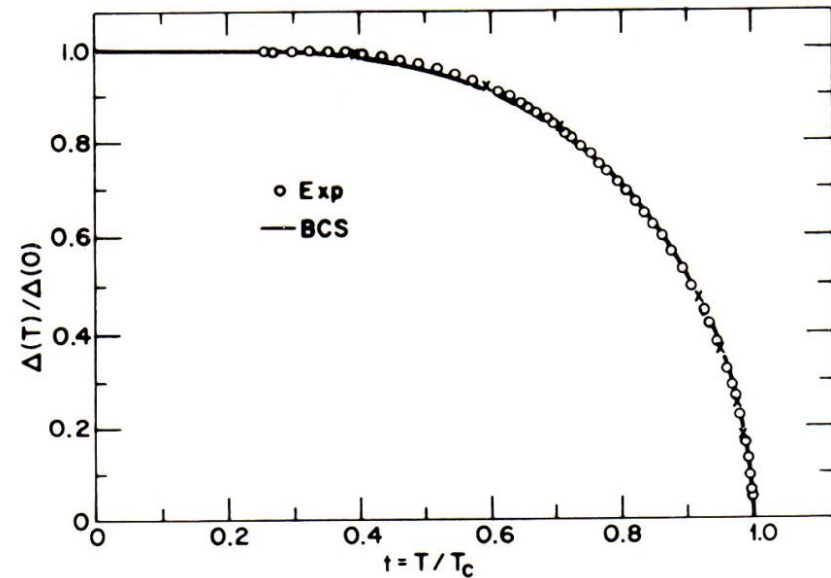
- The Cooper pair needs certain amount of energy to be broken
- The cause of Ohmic loss, stochastic scattering of one single electron by phonon or impurity **cannot break the pair**  
→ No DC loss

The Equilibrium state of conventional superconductor was understood !

→ In this lecture, we try to obtain qualitative insight of the phenomenon

Self-consistent gap equation

$$\Delta = N(E_F)V \int_{\Delta}^{\hbar\omega_D} \frac{\Delta}{\sqrt{\xi^2 + \Delta^2}} \tanh\left(\frac{1}{2} \frac{\sqrt{\xi^2 + \Delta^2}}{k_B T}\right) d\xi$$



# Electrons in a perfect metal are free (independent)

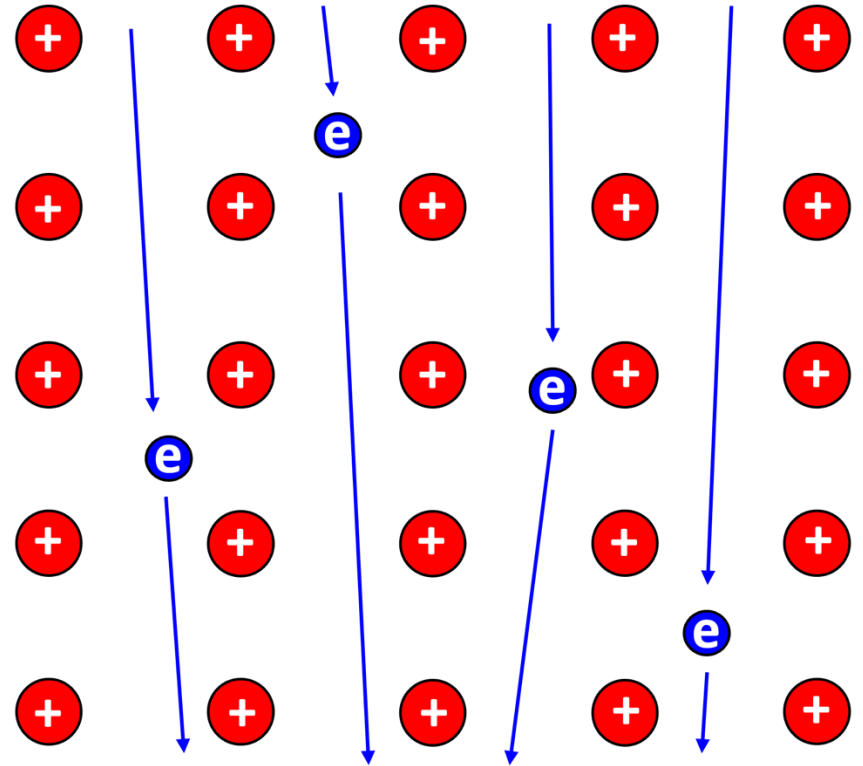
Perfectly periodic potential by ions does **NOT** scatter electrons (Bloch's theorem)

These electrons are **NOT** our favorite elementary particle of

$$m = 511 \text{ keV}$$

These electrons are **dressed** by complicated electromagnetic property of metals to have an effective mass  $m^*$  given by a band structure

→ **Quasi-particles**



In reality, imperfection causes quasi-particle scattering

# Electrons in a real metals show Ohmic loss

Imperfections causes **local** scattering

1. Impurity, defects (scattering time  $\tau_{def}$ )
2. Lattice vibration, phonon ( $\tau_{ph}$ )

Total scattering time

$$\frac{1}{\tau} = \frac{1}{\tau_{def}} + \frac{1}{\tau_{ph}}$$

Macroscopic phenomenology (Drude model)

An electron accelerated by an electric field

$$m^* \frac{dv}{dt} = -eE$$

is scattered by imperfections per  $\tau$ , and its velocity relaxes to a mean velocity

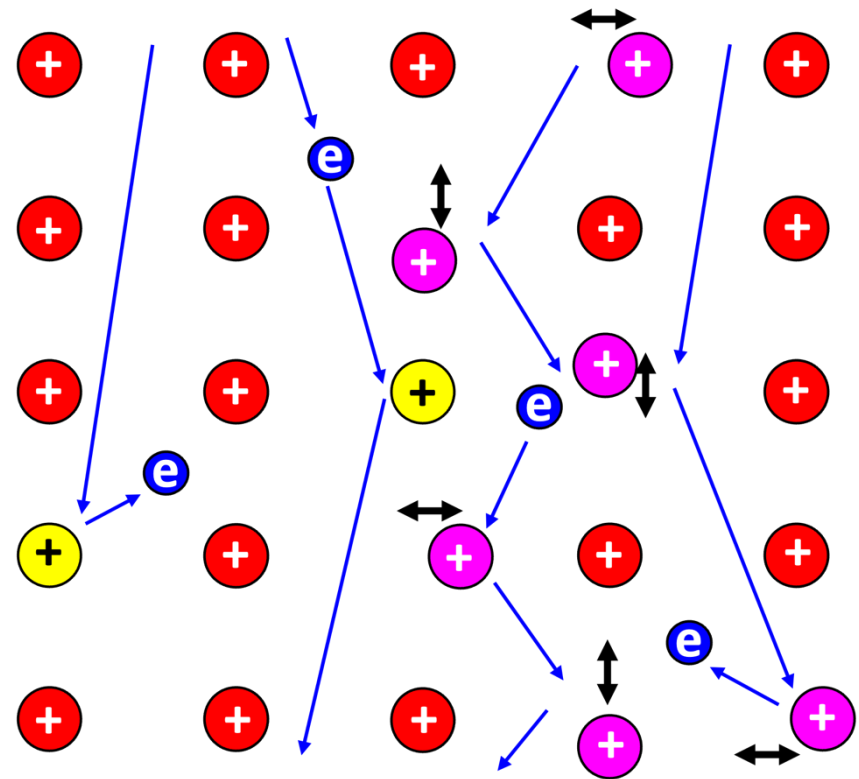
$$\langle v \rangle = -\frac{e}{m^*} E \tau$$

Electric current is a collective flow of  $n$  electrons

$$j = -en\langle v \rangle = \frac{e^2 n \tau}{m^*} E \quad \text{Ohm's law}$$

Electrical conductivity  $\sigma$

$$j = \sigma E$$



If electrons *in a distance* (>39 nm) are bounded, *local* (< 0.5 nm) scattering can be avoided

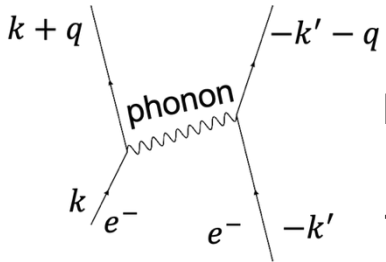
**Any** small attractive interaction  $V$  between electrons can lead to a **Cooper pair** coupled with an energy  $2\Delta$ , below critical temperature  $T_c$

## BCS gap equation (1957)

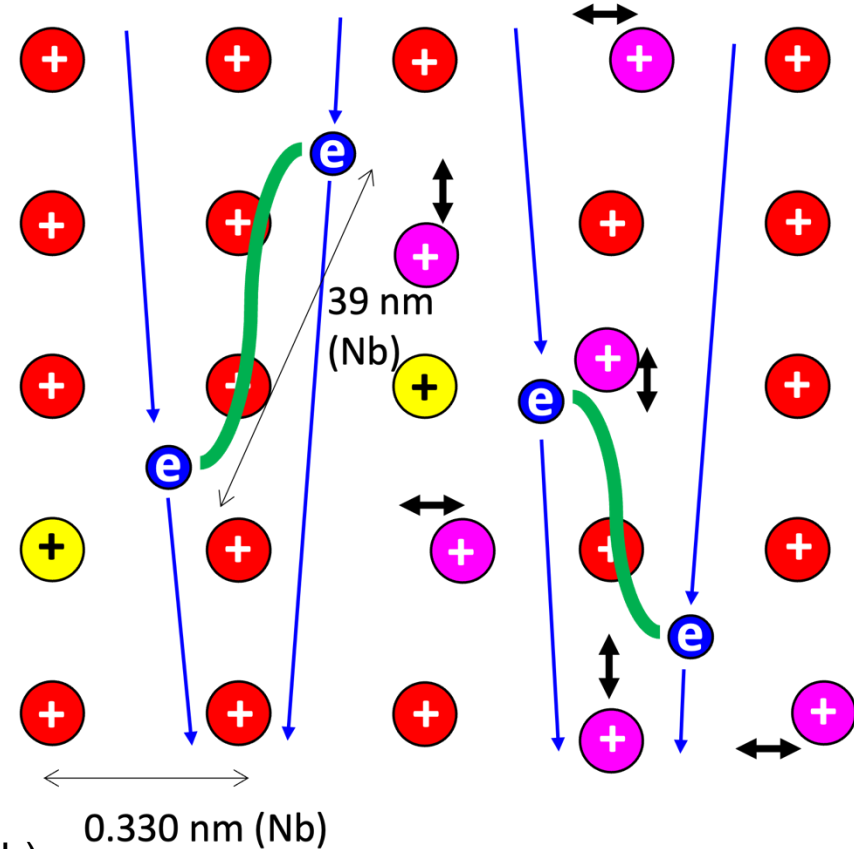
Non-perturbative!

$$\Delta = n(E_F)V \int_{\Delta}^{\hbar\omega_D} \frac{\Delta}{\sqrt{\xi^2 + \Delta^2}} \tanh\left(\frac{1}{2} \frac{\sqrt{\xi^2 + \Delta^2}}{k_B T}\right) d\xi$$

Classical superconductors' attractive potential is from **longitudinal mode of lattice vibration**



If energy transfer  $|\epsilon_{k+q} - \epsilon_k|$  is smaller than phonon energy the interaction is attractive (Flöhlich)  $\rightarrow$  Eliashberg's strong coupling superconductor (1960)



No scattering

$$m^* \frac{\partial \langle v \rangle}{\partial t} = -eE$$

generates super-current

$$j_s = -en_s \langle v \rangle$$

$$\rightarrow \frac{\partial j_s}{\partial t} - \frac{n_s e^2}{m^*} E = 0$$

Apply  $\nabla \times$  from the left

$$\frac{\partial}{\partial t} (\nabla \times j_s) - \frac{n_s e^2}{m^*} \nabla \times E = 0$$

$\sim \nabla \times \mathbf{B} / \mu_0$

leads to

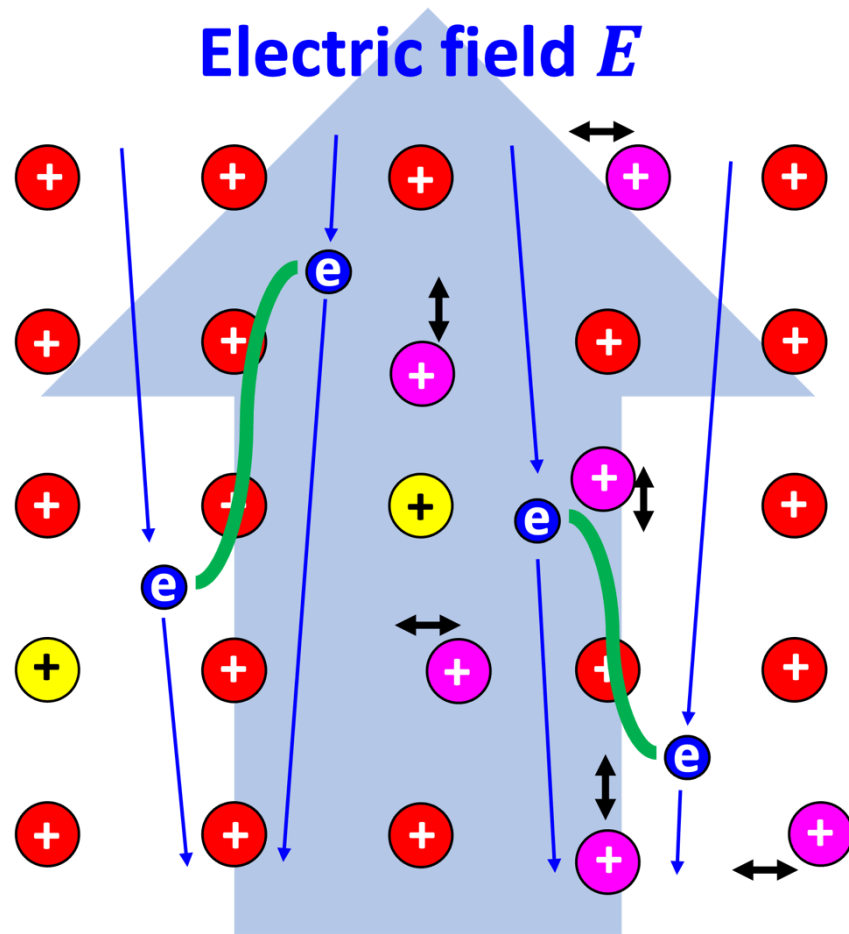
$$\frac{\partial}{\partial t} \left[ \nabla^2 \mathbf{B} - \frac{1}{\lambda_L^2} \mathbf{B} \right] = 0$$

$$\lambda_L^2 \equiv \frac{m^*}{n_s e^2 \mu_0}$$

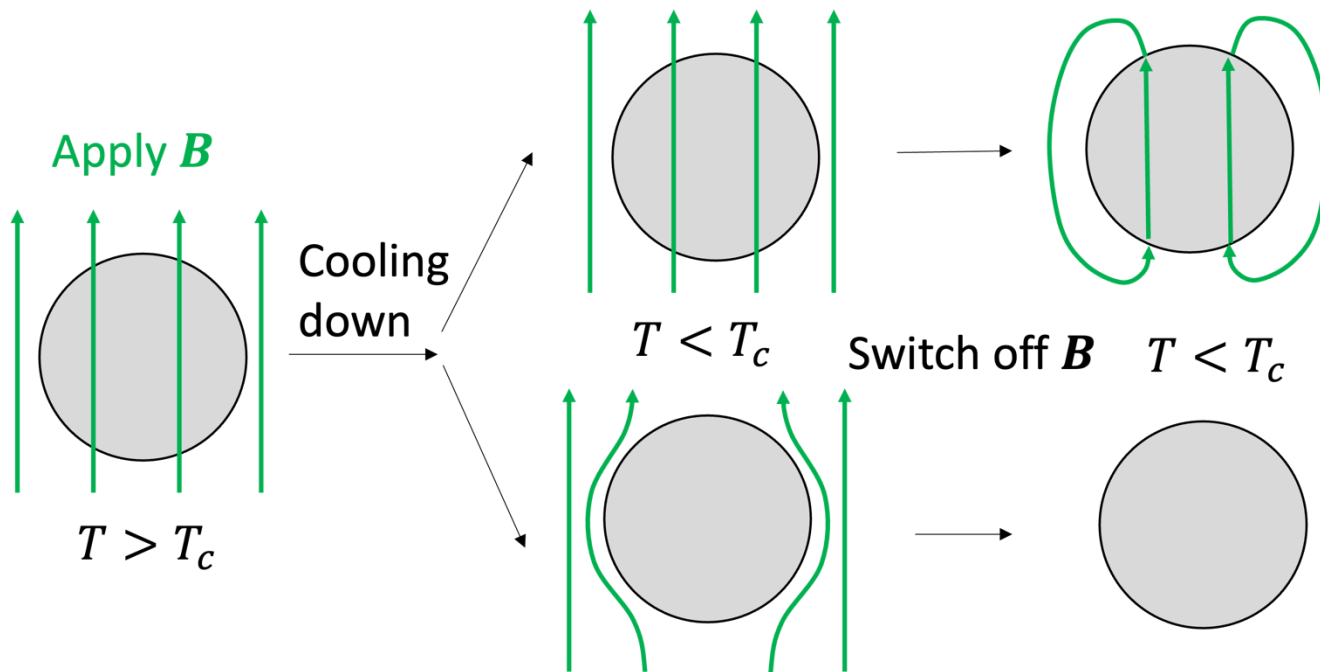
Constant of time

→ Initial condition before phase transition  $T > T_c$  must be preserved

## Electric field $E$



## **Meissner effect** differentiates them



### Perfect Electric Conductor

$$\nabla^2 \left( \frac{\partial \mathbf{B}}{\partial t} \right) - \frac{1}{\lambda_L^2} \left( \frac{\partial \mathbf{B}}{\partial t} \right) = 0$$

Preserve initial condition!

### Superconductor

Zero field!

$$\nabla^2 \mathbf{B} - \frac{1}{\lambda_L^2} \mathbf{B} = 0$$

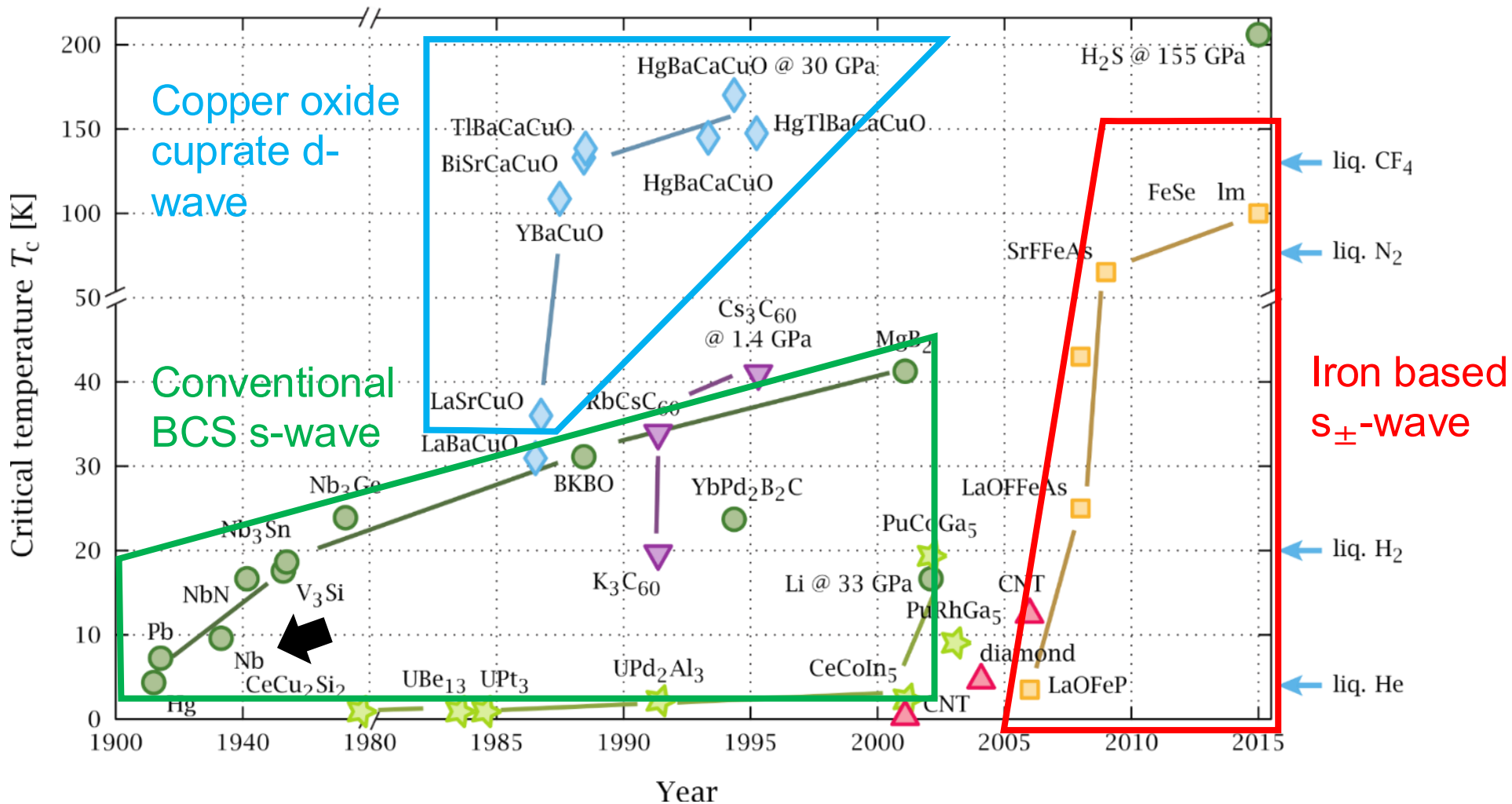
London **Additional constraint**  
equation **(broken Gauge symmetry)**

Superconductivity is a thermodynamical state which expels magnetic fields and cannot be explained by classical electrodynamics  $\rightarrow$  **beyond the scope of this lecture** 😞



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# BCS and non BCS superconductors





- **BCS superconductors (1911)**
  - Example: Hg, Al, Sn, Pb, Nb, NbN, NbTi, Nb<sub>3</sub>Sn, ..., MgB<sub>2</sub> (?)
  - Phonon mediated Cooper pairs
  - Application: superconducting magnet, cavities, detectors, qubit
- **Cooper oxide superconductors (discovered in 1986)**
  - Example: YBCO, ...
  - Fundamental theory unknown (Coulomb repulsive force generates correlation ?)
  - Application: magnet, current lead, beam screen, dark matter detector, etc
- **Iron based superconductors (discovered in 2008)**
  - Example: Ba-122, FeSeTe, ...
  - Fundamental theory unknown (Spin interaction generates correlation ?)
  - Application: magnet, current lead, dark matter detector, cavities (?), etc
- **More fancy superconductors...**



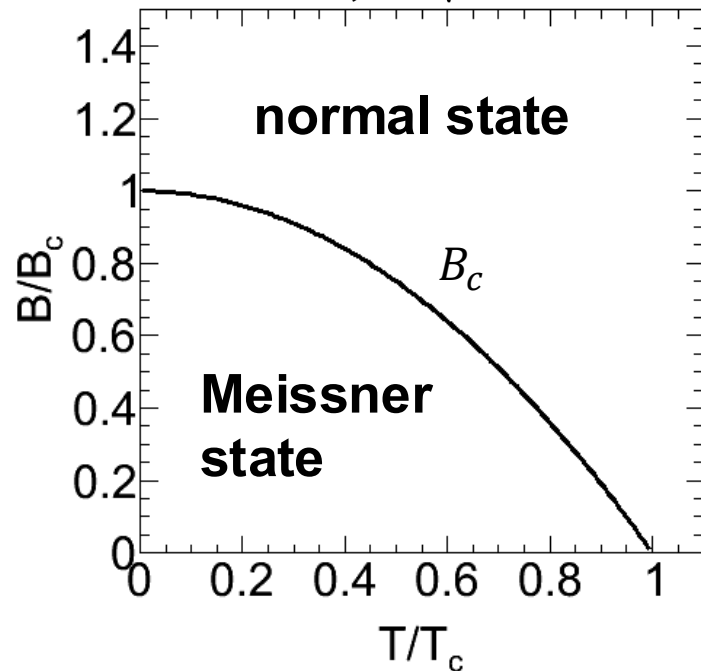
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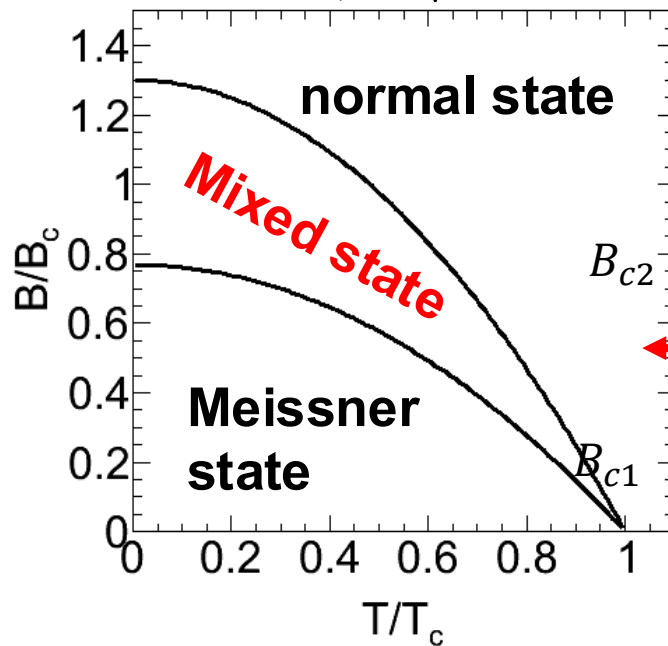
# Strong but *static* magnetic field: Type-I vs Type-II

Type-I  $\kappa = \frac{\lambda}{\xi} < \frac{1}{\sqrt{2}} = 0.71$



$$\kappa_{Pb} \sim \frac{28 \text{ nm}}{71 \text{ nm}} \sim 0.40$$

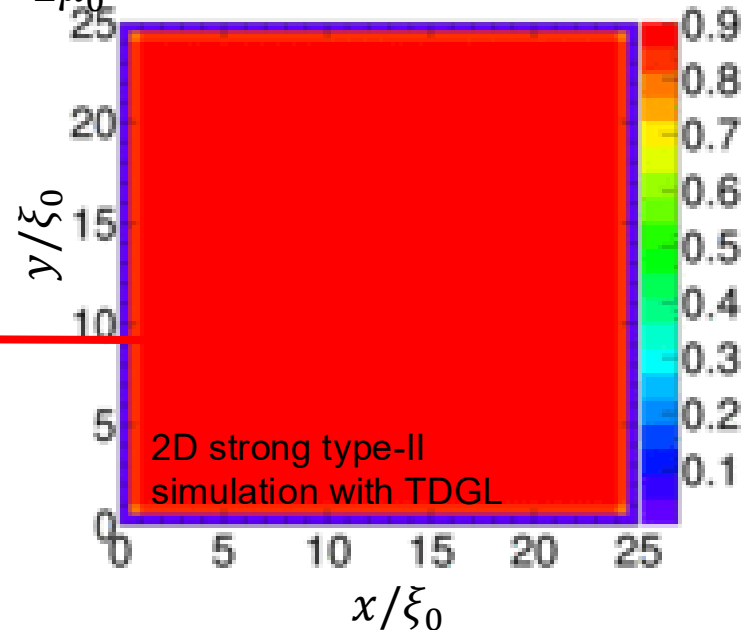
Type-2  $\kappa = \frac{\lambda}{\xi} > \frac{1}{\sqrt{2}} = 0.71$



$$\kappa_{Nb} \sim \frac{36 \text{ nm}}{39 \text{ nm}} \sim 0.92$$

Stabilized by NC/SC boundary energy

$$\frac{1}{2\mu_0} (\xi_0 B_c^2 - \lambda_L B^2) < 0 \text{ for } B > B_{c1}$$



Without pinning centers, type-II **traps** magnetic flux if  $B > B_{c1}$

Quantized flux  $\Phi_0 = \frac{h}{2e} = 2.07 \times 10^{-15} \text{ Wb}$

**DC Magnetic fields** in magnets to bend the trajectory (**Mixed state**)



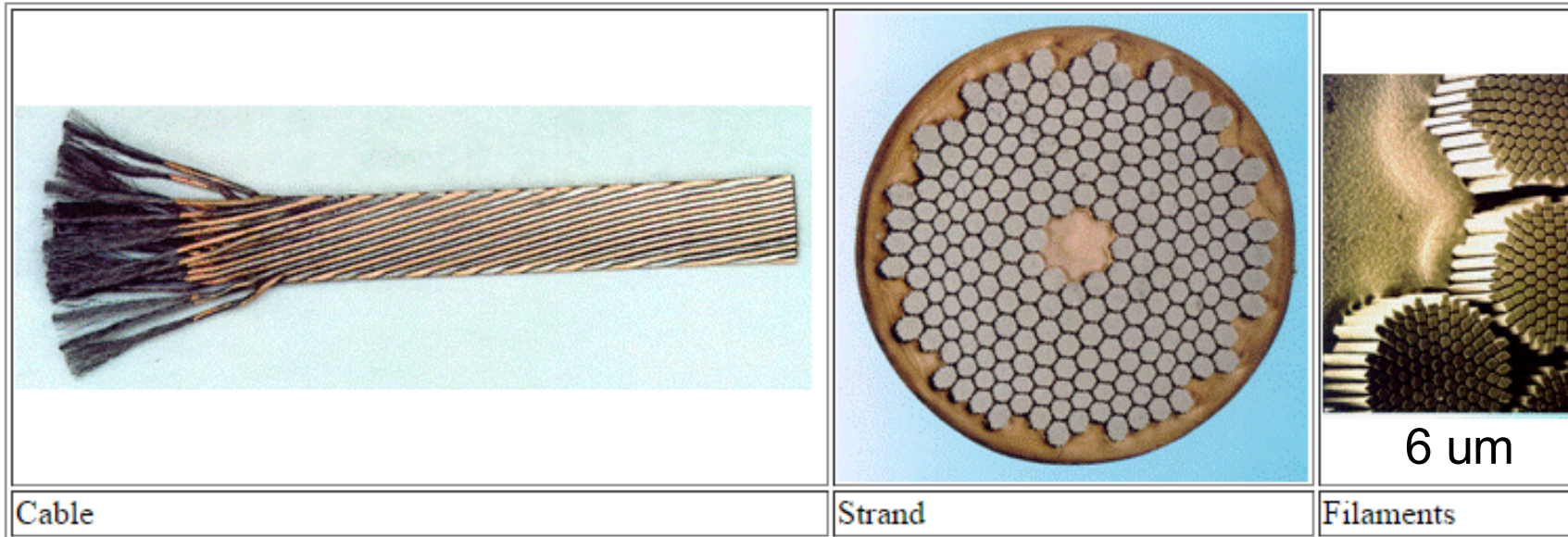
**RF Electric fields** in cavities to accelerate the beam (**Meissner state**)



DC vs RF is qualitatively different in superconducting devices

## Rutherford cable

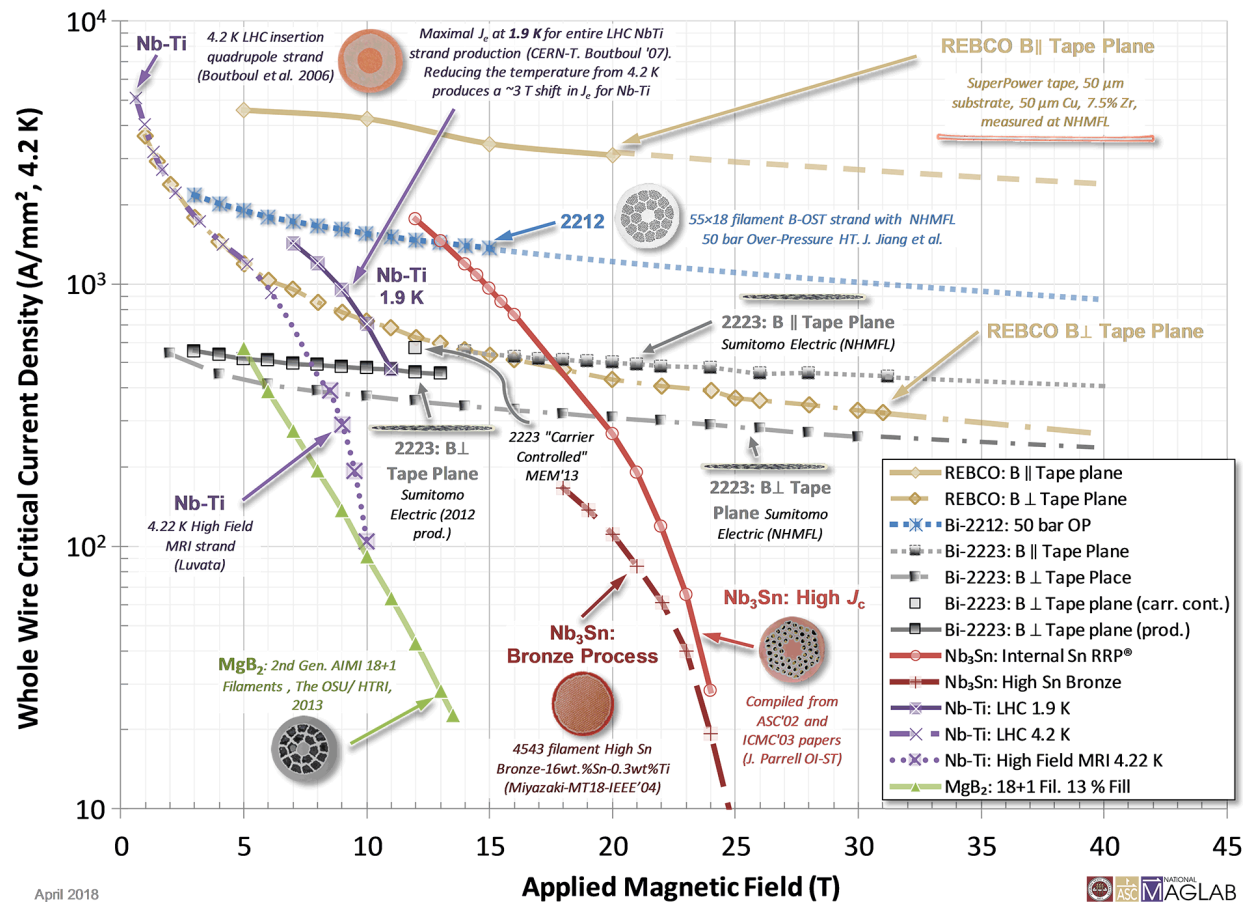
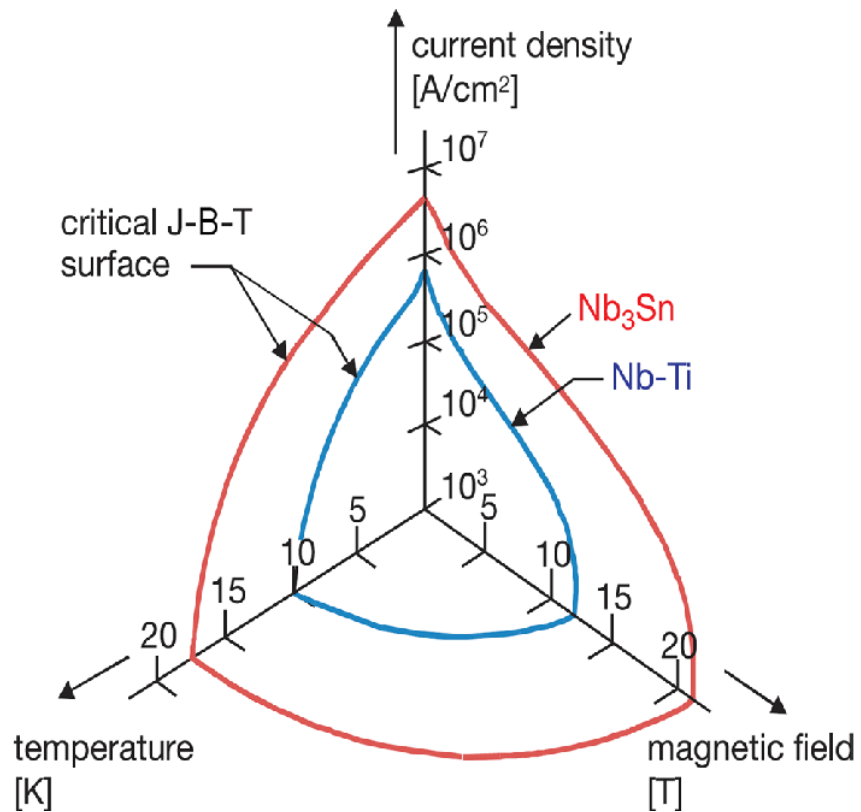
NbTi filaments embedded in copper matrix for heat and current → LHC magnets



In LHC :  
 1200 magnets  
 7600 km of cable  
 36 strands per cable  
 6400 filaments per strands  
 → Total length of filaments  
 10 times the distance  
 between earth and sun !!!

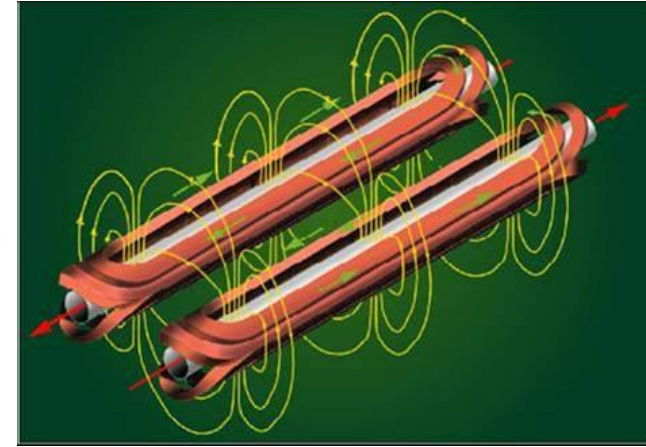
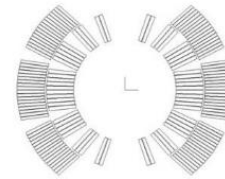
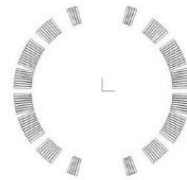
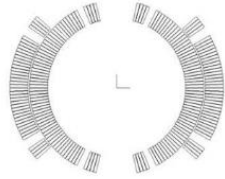
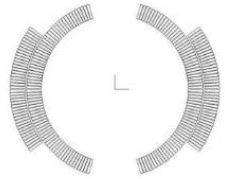
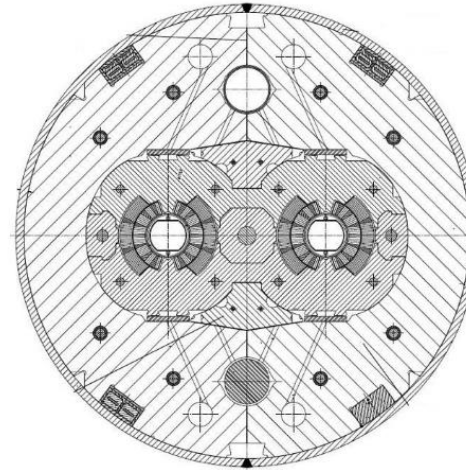
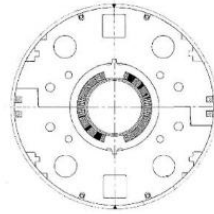
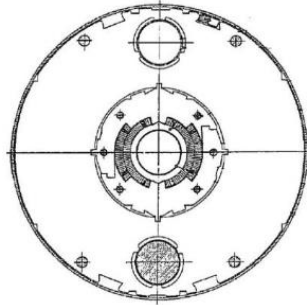
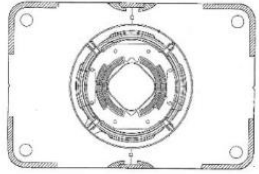
The NbTi materials is exposed to 8.3 T  $\gg$   $H_{c1}$  at 1.9 K → Mixed state

# Critical current density

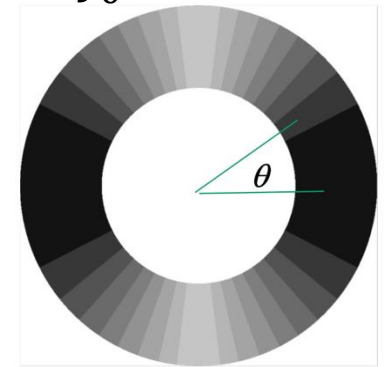


April 2018

# SC dipole: history of NbTi



$$J = J_0 \cos \theta$$



$\cos \theta$  current distribution gives pure dipole field

Tevatron

HERA

RHIC

LHC

76 mm bore

$B = 4.4 \text{ T}$

$T = 4.2 \text{ K}$

first beam 1983

75 mm bore

$B = 5.0 \text{ T}$

$T = 4.5 \text{ K}$

first beam 1991

80 mm bore

$B = 3.5 \text{ T}$

$T = 4.3\text{-}4.6 \text{ K}$

first beam 2000

56 mm bore

$B = 8.34 \text{ T}$

$T = 1.9 \text{ K}$

first beam 2008

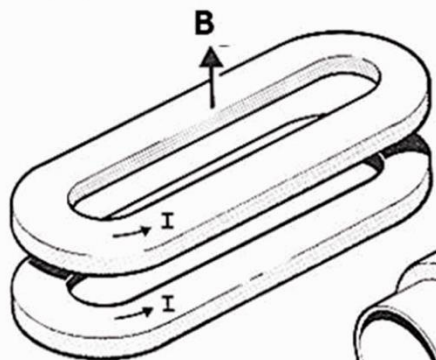
Courtesy G. d. Rijk and P. Ferracin, CERN



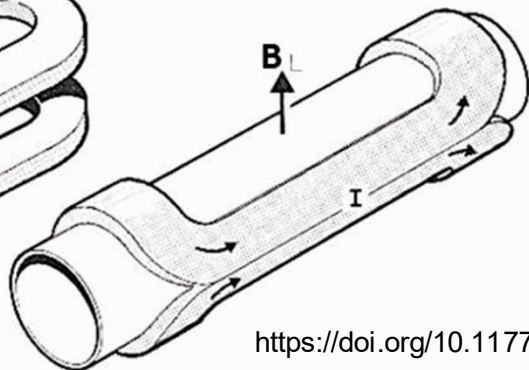
# Different dipoles

Baseline:  $\cos \theta$  (racetrack or saddle)

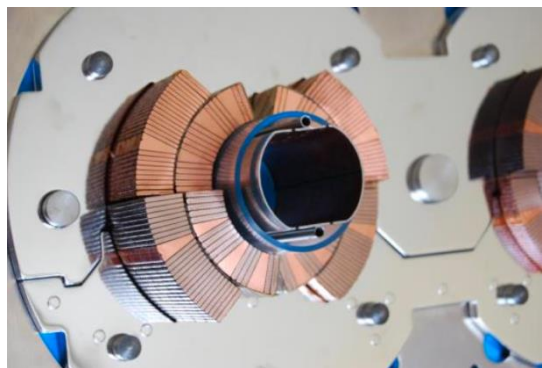
(b)



(c)



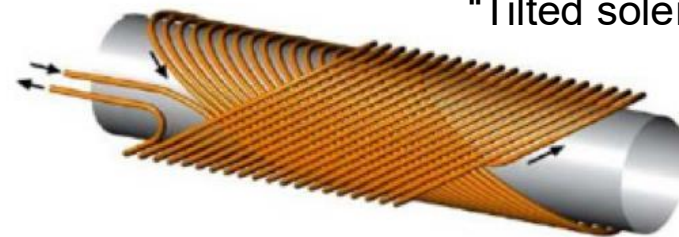
<https://doi.org/10.1177/15280837166612>



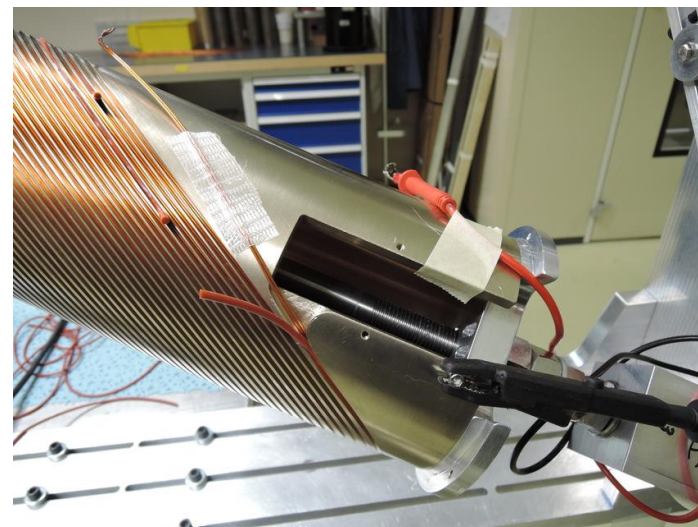
Courtesy G. d. Rij, M. Wilson,

Canted  $\cos \theta$  (CCT)

“Tilted solenoid”



Proposed in 1960s realized recently

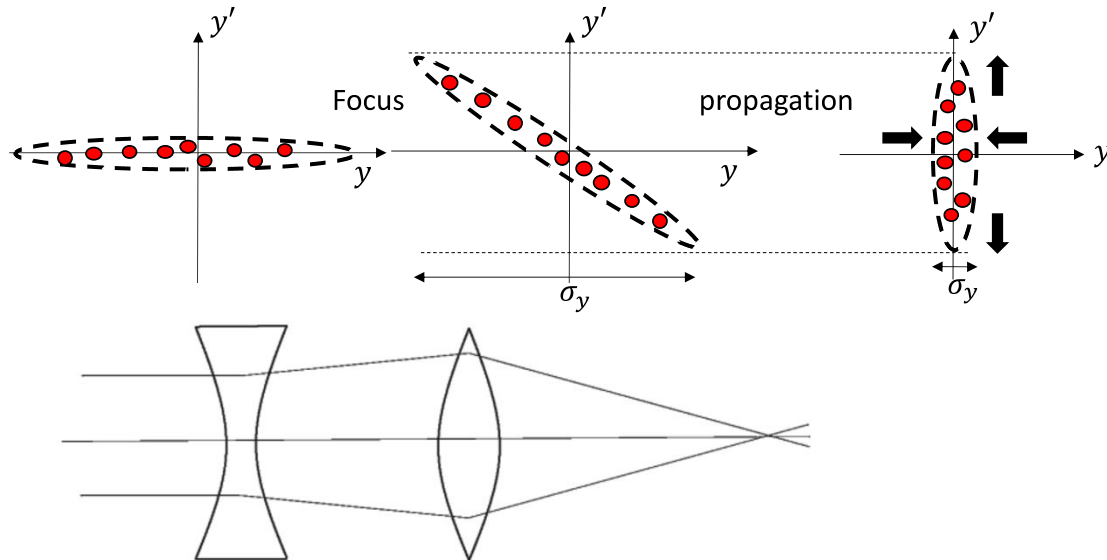


<https://home.cern/news/news/engineering/new-life-old-technology-canted-cosine-the-ta-magnets>

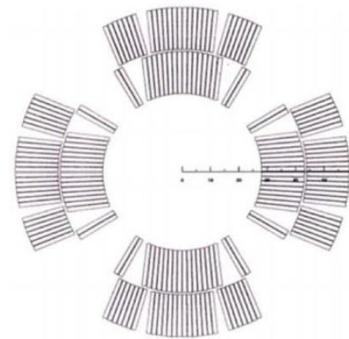
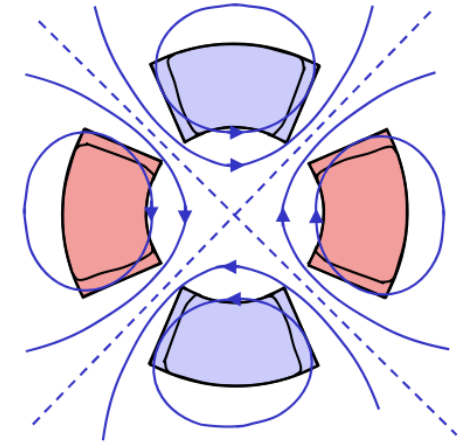
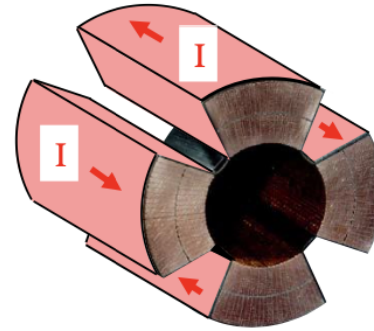
Lorentz force is not only for bending trajectory

$$\frac{d(mv_\theta)}{dt} \cdot \vec{u}_\theta - m \frac{v_\theta^2}{\rho} \cdot \vec{u}_r = eE_\theta \cdot \vec{u}_\theta + ev_\theta B_z \cdot \vec{u}_r$$

Focusing and defocusing of a group of charged particles (bunch) are crucial for beam transport and luminosity at collision



Implemented by quadrupole magnets



Courtesy G. d. Rij

$$p[\text{GeV}/c] = 0.3 \times \rho[\text{m}] \times B[\text{T}]$$

## SC magnet

- Strong field (>0.2 T) **steady state**
- Typically proton circular machine
- Ex) 7 TeV & 8.3 T at LHC

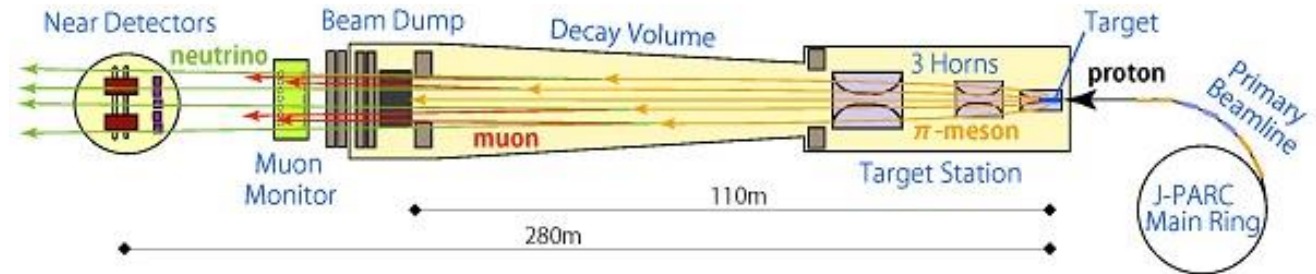
## NC magnet

- Weak field (<0.2 T) **steady state**
- Typically electron circular machine
- Ex) 90 GeV & 0.13 T at LEP

## Short pulsed NC magnet



<https://j-parc.jp/Neutrino/en/nu-facility.html>



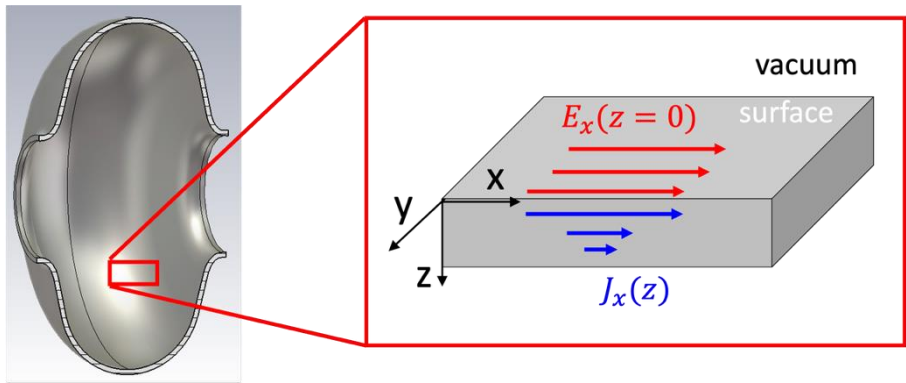
- Separate  $\pi^+$  and  $\pi^-$  for neutrino and anti-neutrino
  - Too high radiation  $\rightarrow$  SC magnet may not survive
  - Coincidence time window with neutrino detector
- Strong field (2 T) for **short pulse** 5  $\mu\text{s}$  (every 2-3 seconds)



- Introduction: thermodynamics and benefit of cooling (10 min)
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- Non-BCS superconductivity (5 min)
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- Superconducting magnet (10 min)
- **Superconducting RF cavities (20 min)**
- Conclusion



# RF resistance $R_s$ is non zero



## Local surface resistance

$$R_s \equiv \text{Re} \left( \frac{E_x(z=0)}{\int_0^\infty J_x(z) dz} \right)$$

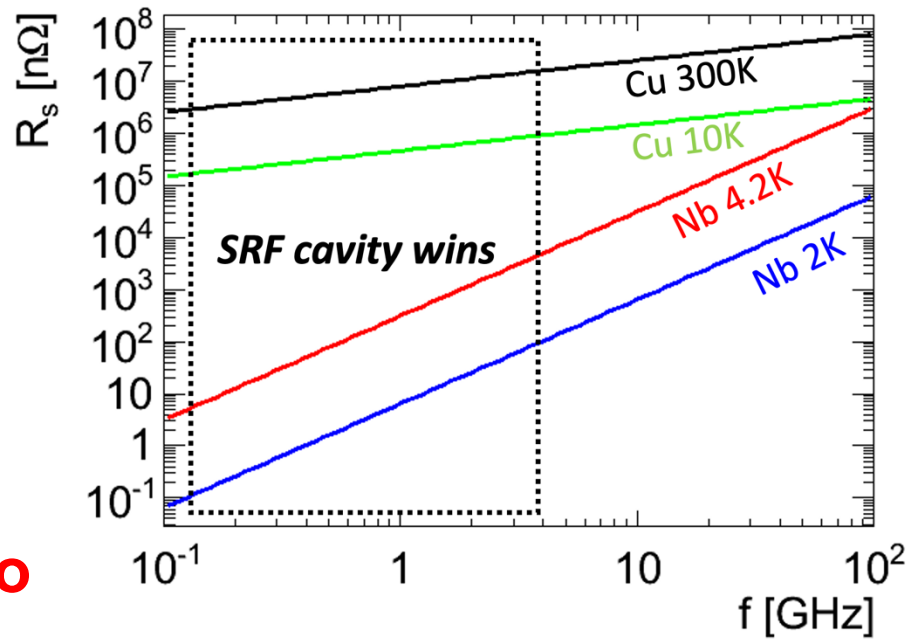
Normal conducting (Cu)

$$R_s = \sqrt{\frac{\pi f \mu_0}{\sigma}} \propto f^{1/2}$$

Super-conducting (Nb)

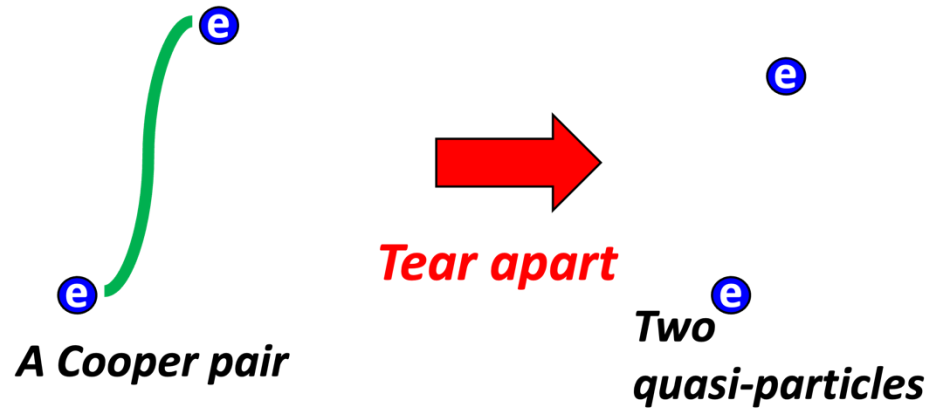
$$R_s = \frac{A f^2}{T} \exp\left(-\frac{\Delta}{k_B T}\right) \propto f^2$$

**Superconducting  $R_s$  is small but non zero**





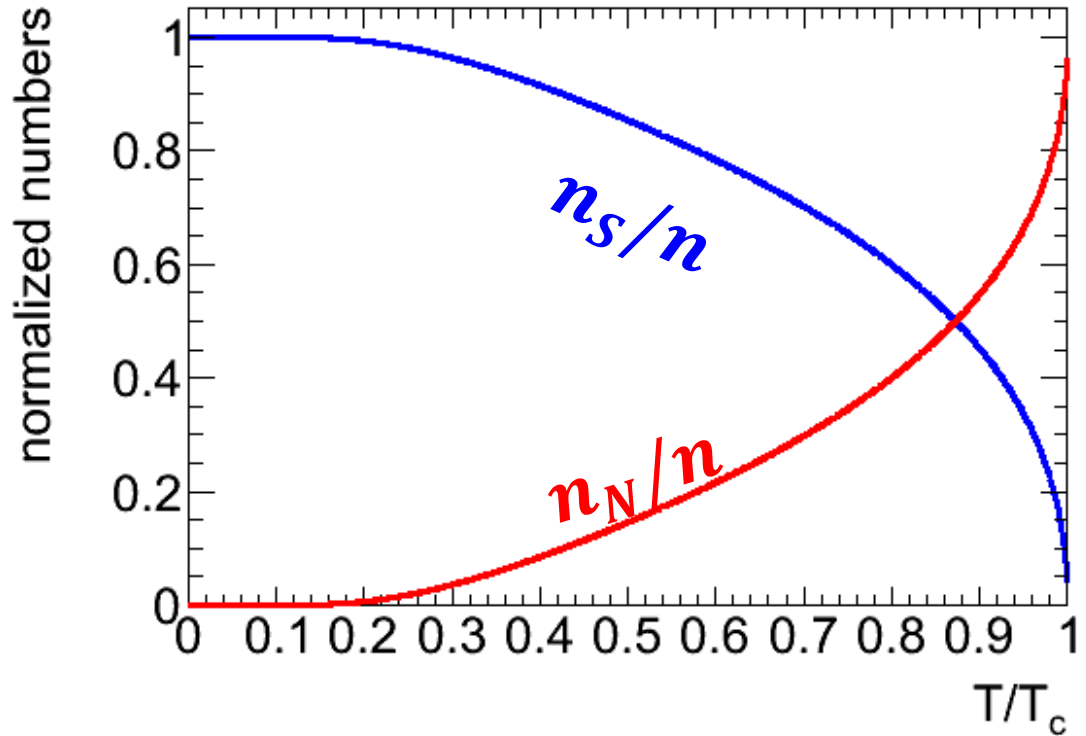
# Thermal excitation of quasi-particles



At finite temperature  $0 < T < T_c$ , these two states are **in thermal equilibrium**

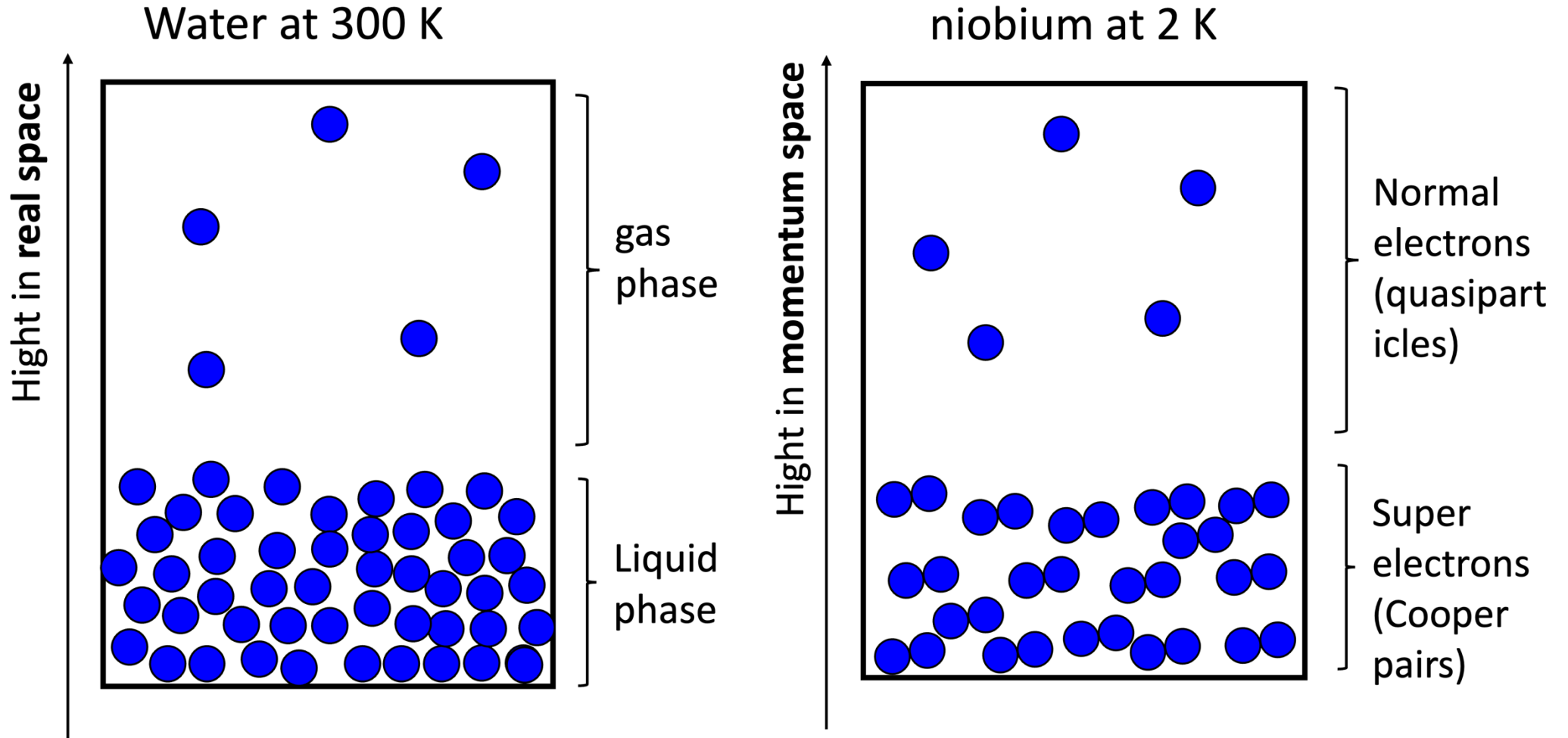
# of quasiparticles:  $n_N \sim \exp\left(-\frac{\Delta}{k_B T}\right)$

# of electrons in Cooper pairs:  $n_S \sim n - n_N$



Quasi-particles ( $\sim$ normal conducting electrons) still exist if  $T > 0$

# Coexistence of Cooper pairs and quasi-particles





## Supercurrent

$$\frac{\partial j_s}{\partial t} - \frac{n_s e^2}{m^*} E = 0$$

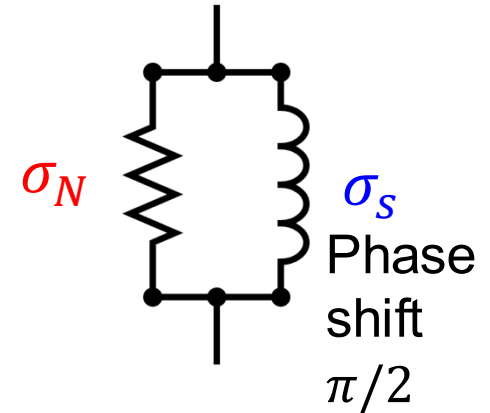
$$j_s = j_0 \exp(i\omega t)$$

$$j_s = -i \frac{n_s e^2}{m^* \omega} E \equiv \sigma_s$$

## Normal current

Ohm's law  $\rightarrow$

$$j_N = \frac{n_N e^2 \tau}{m^*} E \equiv \sigma_N$$



## Total current induced by RF

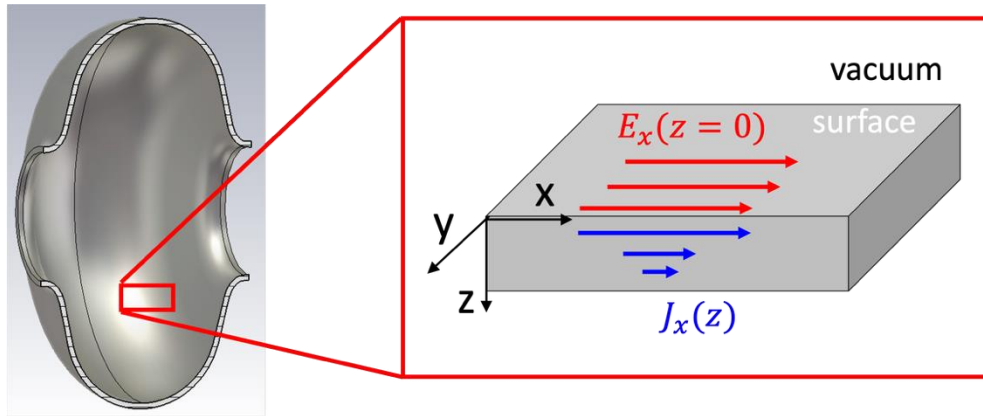
$$j = j_s + j_N \rightarrow j = (\sigma_N - i\sigma_S)E$$

Dissipation by quasi-particles  $\rightarrow$  resistive

Inertia of Cooper pairs  $\rightarrow$  inductive



# Surface resistance of superconductor



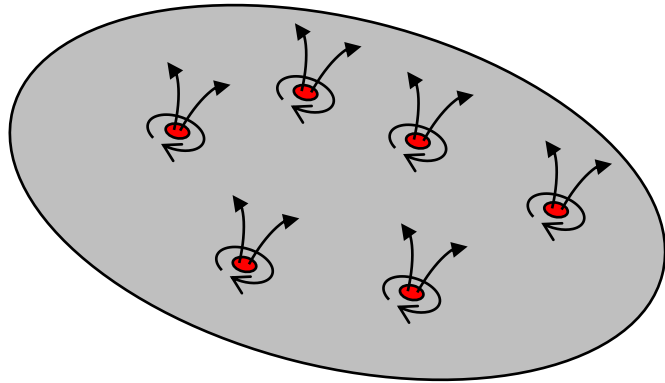
$$\sigma_N = \frac{e^2 n_N \tau}{m^*} \propto n_N \propto \exp\left(-\frac{\Delta}{k_B T}\right)$$

$$\begin{cases} j_x = (\sigma_N - i\sigma_S)E_x \\ E_x(z) = E_0 \exp(-z/\lambda_L) \end{cases} \rightarrow R_s \equiv \text{Re} \left( \frac{E_x(z=0)}{\int_0^\infty J_x(z) dz} \right) \sim \frac{1}{2} \frac{\sigma_N}{\sigma_S} \sqrt{\frac{\omega \mu_0}{\sigma_S}} = \frac{\mu_0^2}{2} \lambda_L^3 \sigma_N \omega^2 > 0$$

## Lessons

- One origin of the finite  $R_s$  of superconductors is quasi-particles
- Quasi-particles are thermally activated from Cooper pairs at  $0 < T < T_c$
- $R_s$  exponentially decreases by lower  $T$  because quasi-particles are frozen out
- Higher RF frequency increases  $R_s \sim \omega^2$
- Order of magnitude is 10 nΩ

# Static trapped magnetic field in SC cavities



Normal  
conducting  
area

$$R_{\text{mag}} \sim N \times \pi \xi_0^2 \times R_n \sim \frac{B_{\text{ext}}}{2B_{c2}} R_n$$

Flux number density      Normal conducting

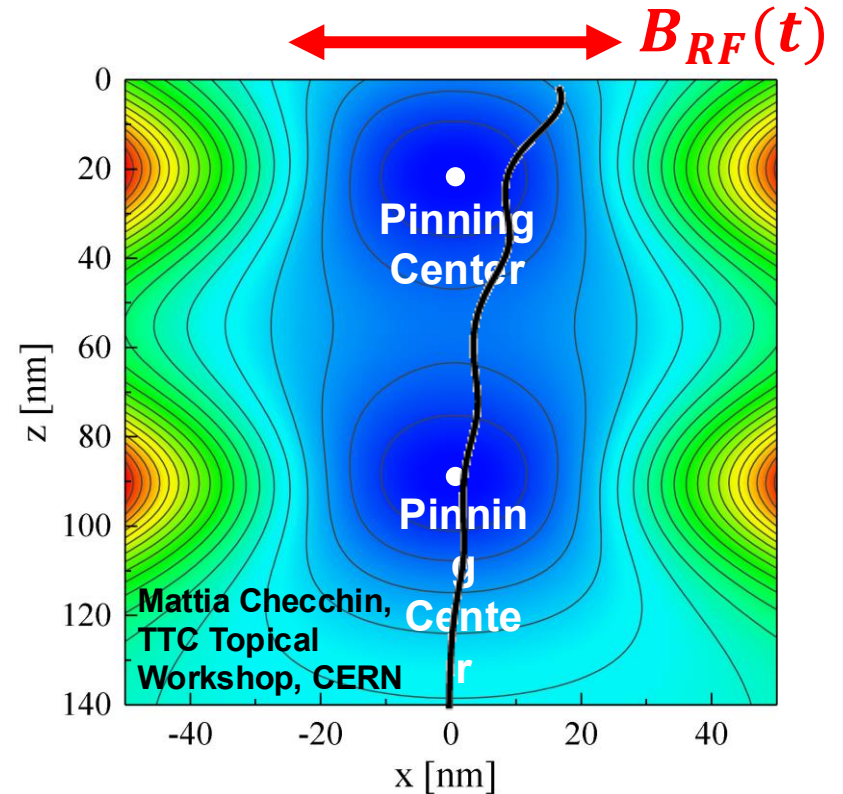
Earth field  $B_{\text{ext}} = 50 \mu\text{T}$

$B_{c2} \sim 400 \text{ mT (Nb)}$

$R_n \sim 1.3 \text{ m}\Omega \text{ at } 1.3 \text{ GHz (Nb)}$

$$R_{\text{mag}} \sim 80 \text{ n}\Omega > R_{\text{BCS}}(2\text{K}) \sim 10 \text{ n}\Omega$$

An excellent magnetic shield is mandatory for SC cavities

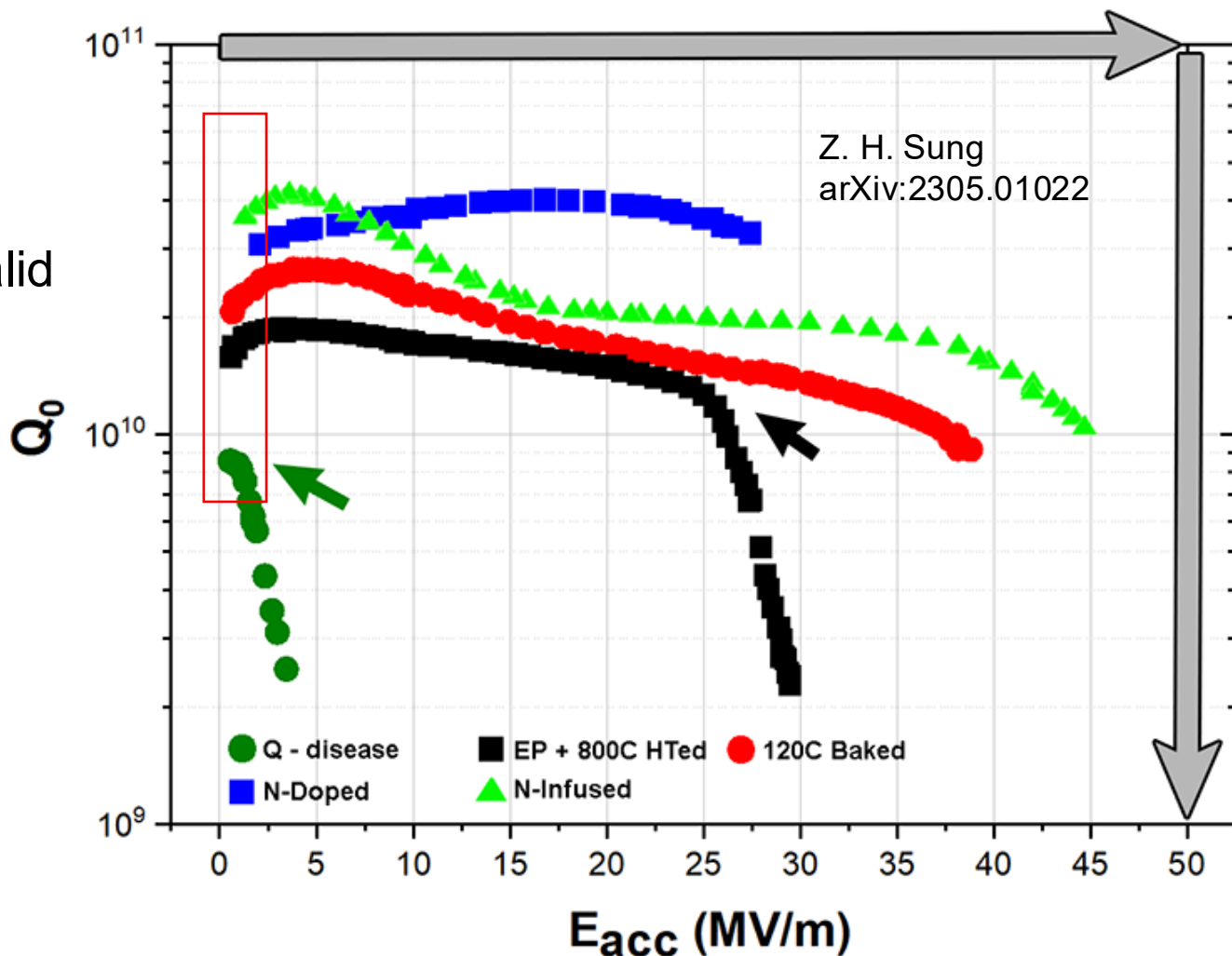


# Quality factor vs accelerating gradient

$$Q_0 \equiv \frac{\omega U}{P_c} = \frac{1}{R_s} \omega \mu \frac{\int_V H^2 dV}{\int H^2 dS}$$

geometrical

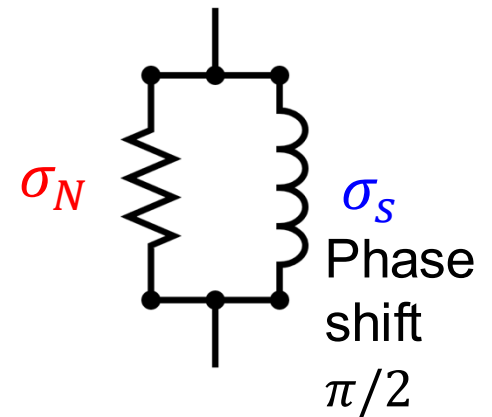
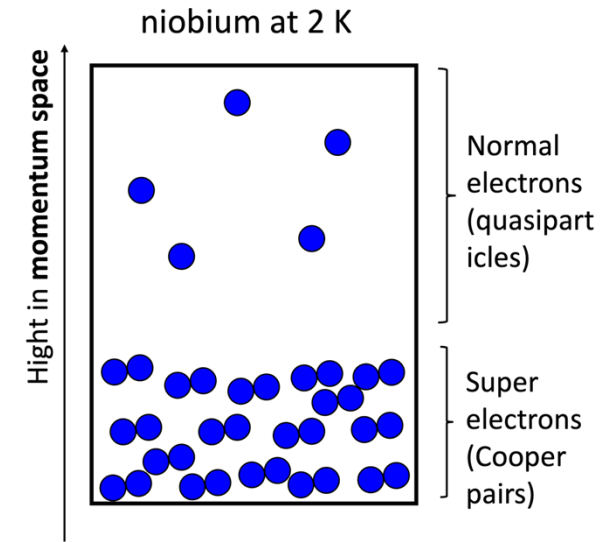
- The established theory is only valid for low external RF field
- The simplest nonequilibrium problem is solved in the linear response theory
- Very tiny difference in surface impacts the results (<10 nΩ physics!)
- We do not have complete theory that explains the nonlinear phenomena in Q vs E  
→ Open research field!





# Comparison: magnet vs cavity

- Magnets are operated in strong DC fields
  - The two-fluid circuit is short  $\rightarrow$  no loss
  - Finite loss during ramping up and down the field
  - Magnetic fields are trapped in Mixed state
    - Strong pinning force is manipulated to avoid flux flow (otherwise, loss)
- Cavities are operated in RF fields
  - The phase shift due to Cooper pairs' inertia causes finite loss in quasiparticles
  - Oscillating trapped flux kills the cavity performance
  - Operation in as clean as the Meissner state
    - RF field itself does not penetrate due to superheating effect and surface barrier





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- Non-BCS superconductivity (5 min)
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- Superconducting RF cavities (20 min)
- **Conclusion**



# Conclusion: *Superconductivity and Cryogenics for Particle Accelerators*

- **Cooling down improves loss but becomes less efficient**
  - Superconducting vs normal conducting under the ideal Carnot cycle
  - Carnot cycle is NOT realistic at all: trade off in efficiency and power evacuation
- **Superconducting devices are typically operated inside liquid helium**
  - Cryogenics is enabled by physics and engineering of thermodynamics
- **Superconductivity is macroscopic quantum phenomenon**
  - Meissner effect is the most characteristic phenomenon (spontaneously broken Gauge symmetry in the ground stage)
  - Zero DC loss is caused by Cooper pairs
  - Classical electrodynamics can give us some insight with limitation
- **Several different superconducting mechanisms are known**
  - Only BCS-type SCs are well understood (phonon-mediated correlation) and Copper oxide & iron-based SC are still under debate
- **SC magnet are operated in the Mixed state of type-II superconductors**
- **SC cavities are operated in the Meissner state of type-II superconductors**
  - Non-equilibrium phenomenon is the remaining challenge of BCS-type SCs
  - Two-fluid model gives us some insight with limitations



# Conclusion: *rich physics in the research field of accelerators*

