

TIANLAI DISH ARRAY CONFIGURATION

R. ANSARI - JULY 2014

- Comparison of several configurations for the Tianlai 16-dish array, and survey strategy
- Based on work being done by Jiao Zhang
- Computation of reconstructed beams from visibilities, Transfer function and noise power spectrum
- Assume transit mode operation, with several scans along the declination, and complete beam knowledge
- assume stationary white noise for the visibilities as a function of time $V_{ij}(t) \rightarrow V_{ij}(\alpha)$

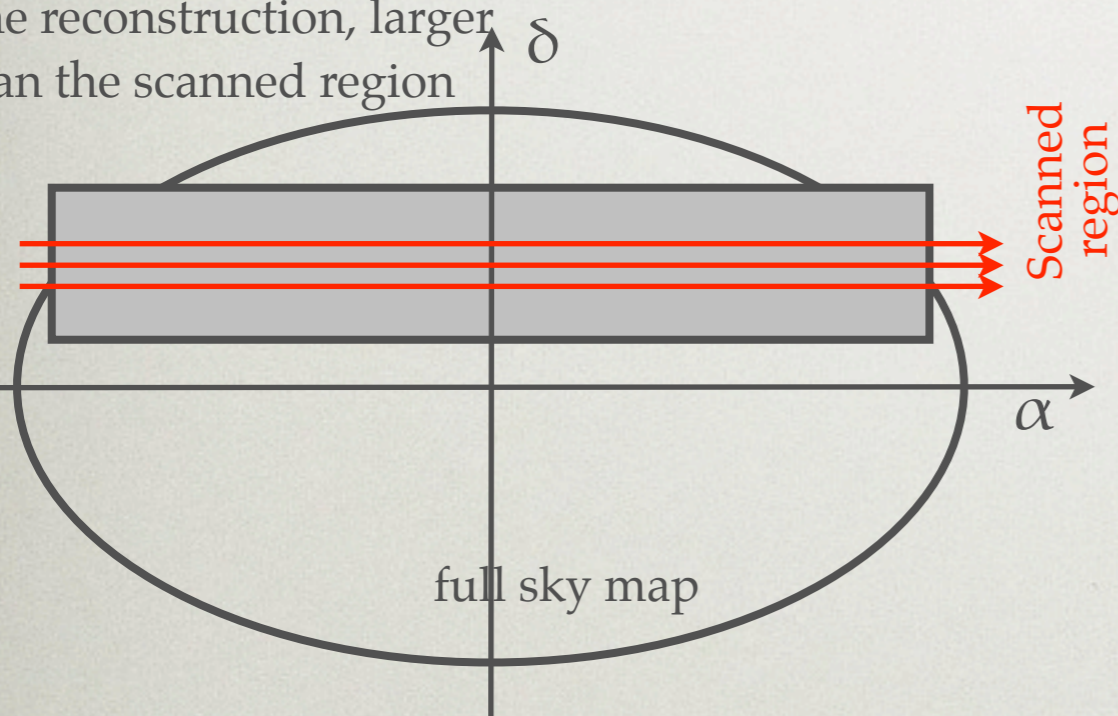
Sky : α (RA, East – West, EW)
 δ (DEC, North – South, NS)

Fourier : $(\alpha, \delta) \longrightarrow (u, v)$

Sky : $I(\alpha, \beta) \longrightarrow F(u, v)$

Visibilities : $V_{ij}(\alpha) \longrightarrow \tilde{V}_{ij}(u)$

Rectangular geometry used
in the reconstruction, larger
than the scanned region



$$\left(\tilde{V}_{ij}(u) \right) = [A_u] \times (F_u(v)) + (n)$$

$$\left(\hat{F}_u(v) \right) = [B_u] \times \left(\tilde{V}_{ij}(u) \right)$$

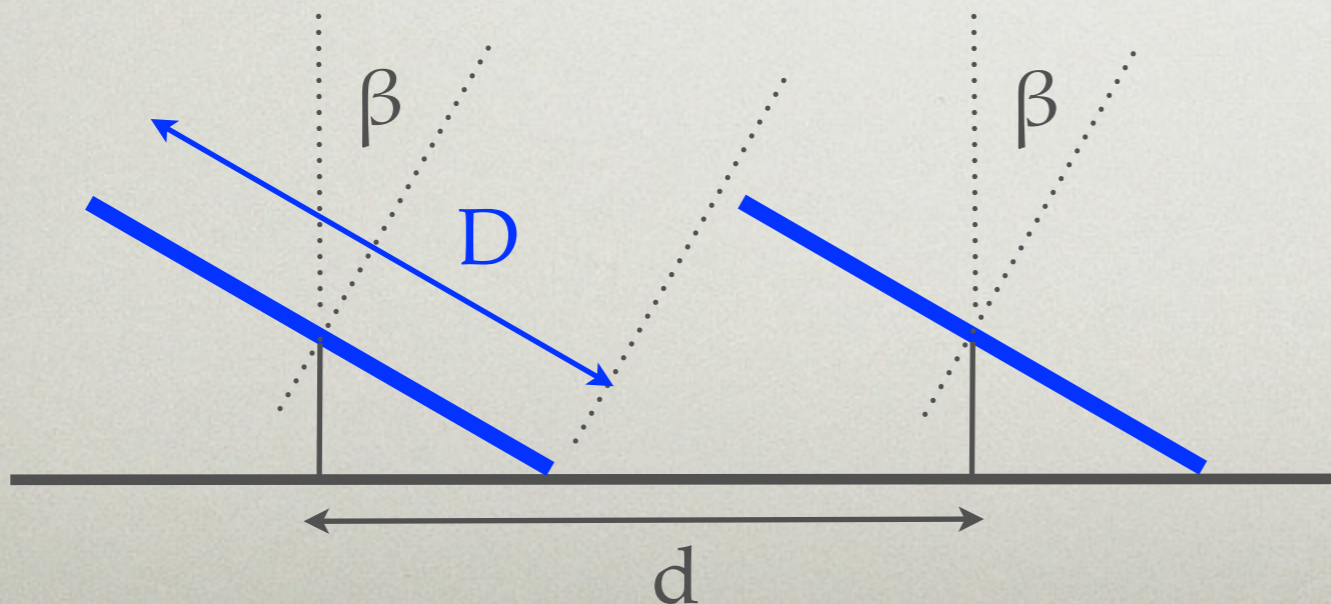
$$\left\{ \hat{F}_u(v) \right\} \longrightarrow \hat{F}(u, v)$$

$$\hat{F}(u, v) \longrightarrow \hat{F}_W(u, v) = \hat{F}(u, v) \times W(u, v)$$

$$\hat{F}_W(u, v) \longrightarrow \hat{I}(\alpha, \delta) \quad (\text{FFT})$$

CONFIGURATIONS

- 16=4x4 D=6 m dishes, $D_{\text{eff}}=\eta D=5.4$ m, base spacing $d=7$ m
- maximum $N_B = 8 \times 17 = 136$ baselines
- (a) regular array, $28 \times 28 \text{ m}^2$, $N_B = 25$ baselines
- (b) circular, 1+6+9, $\sim 32 \times 32 \text{ m}^2$, $N_B = 101$ baselines
- (c) irregular, 2+3+5+4+2, $\sim 32 \times 32 \text{ m}^2$, $N_B = 84$ baselines
- 9 scans : $\delta = \{0, \pm 1.5^\circ, \pm 3^\circ, \pm 4.5^\circ, \pm 6^\circ\}$

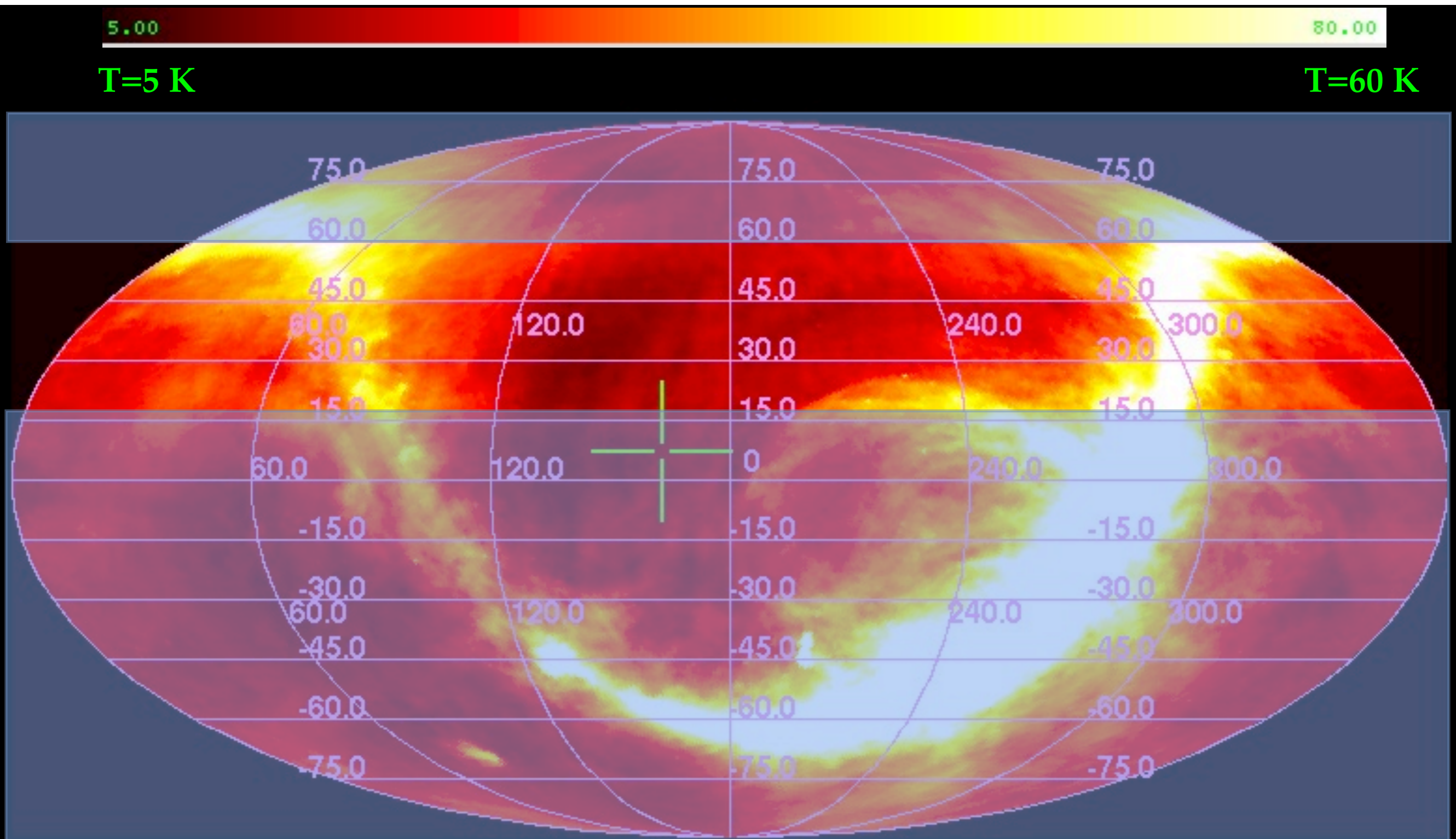


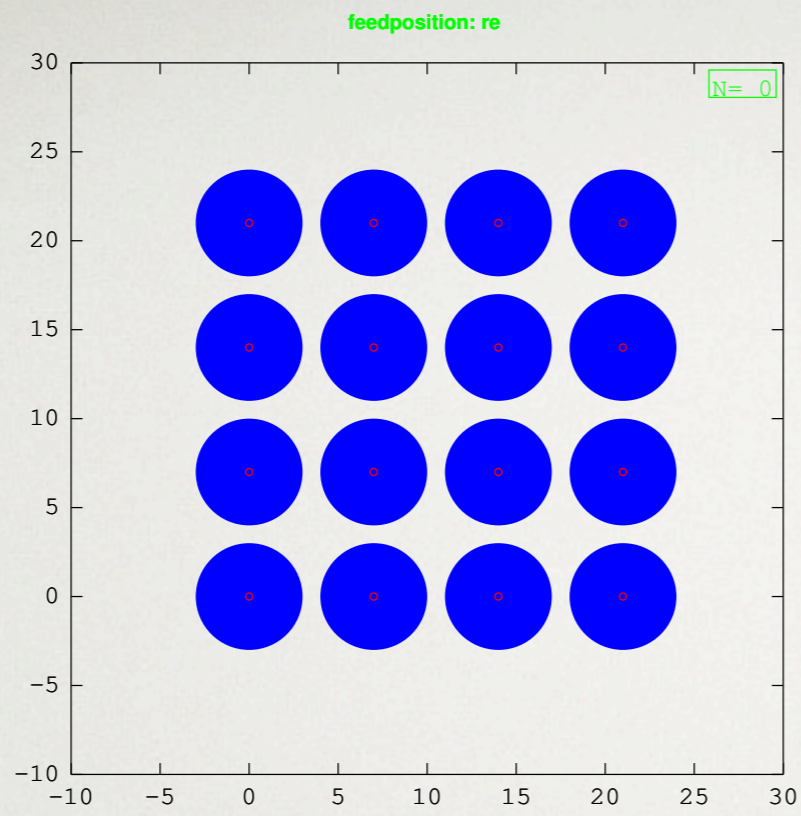
$$d \simeq \frac{D}{\cos(\beta_{\max})}$$
$$D = 6 \text{ m}, d = 7 \text{ m}$$
$$\beta_{\max} \simeq 30^\circ$$

Synchrotron map @ 400 MHz - Eq. Coordinates (ra,dec)

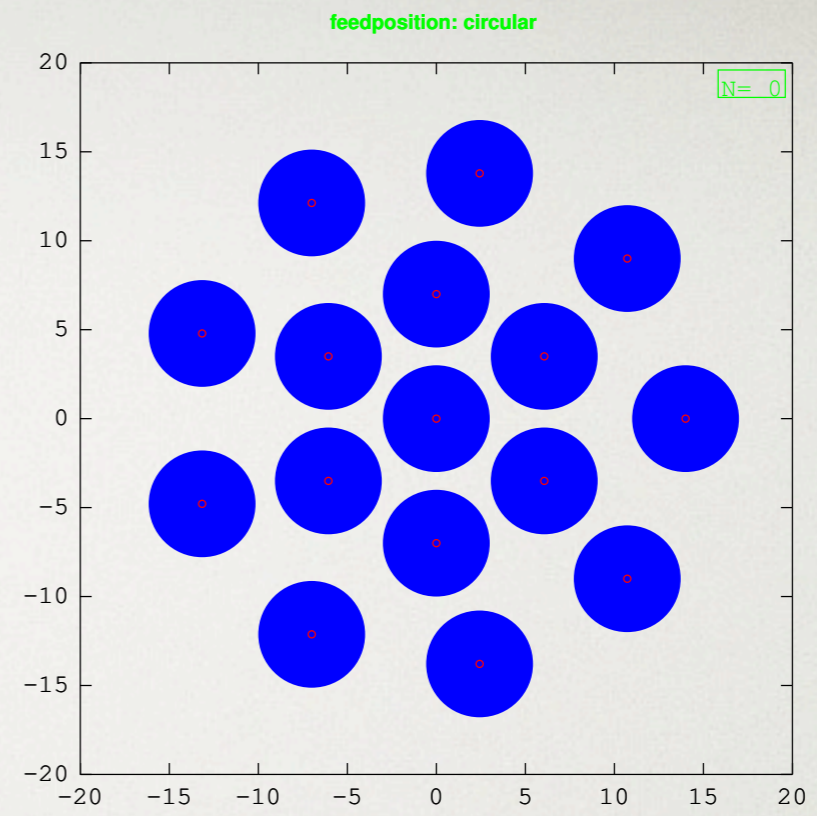
Tianlai-16dish accessible sky region

(45 N \pm 25 deg) \rightarrow 20 < δ < 60 in Xinjiang (45 N)

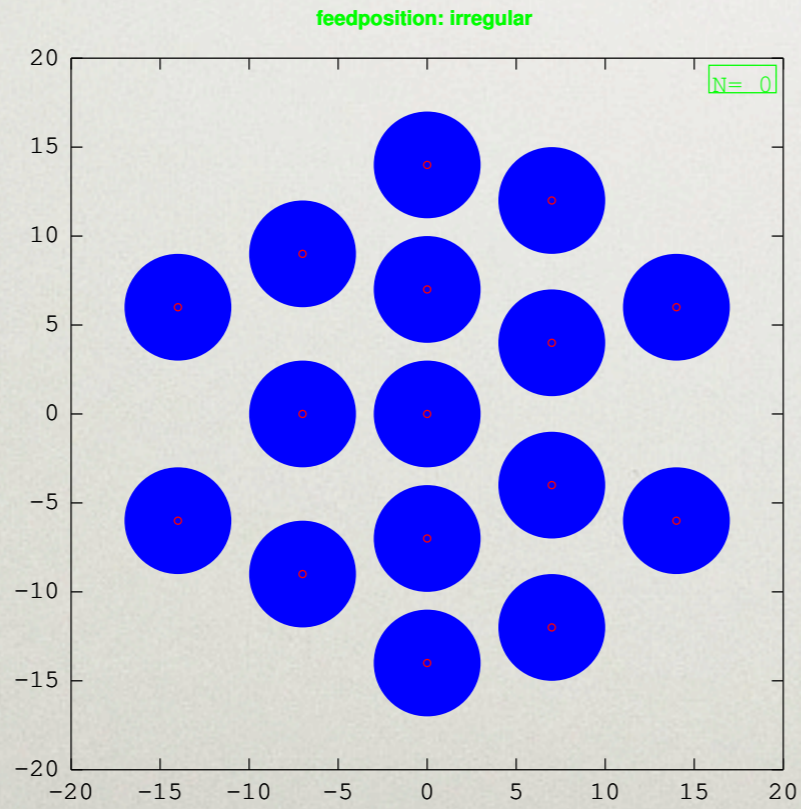




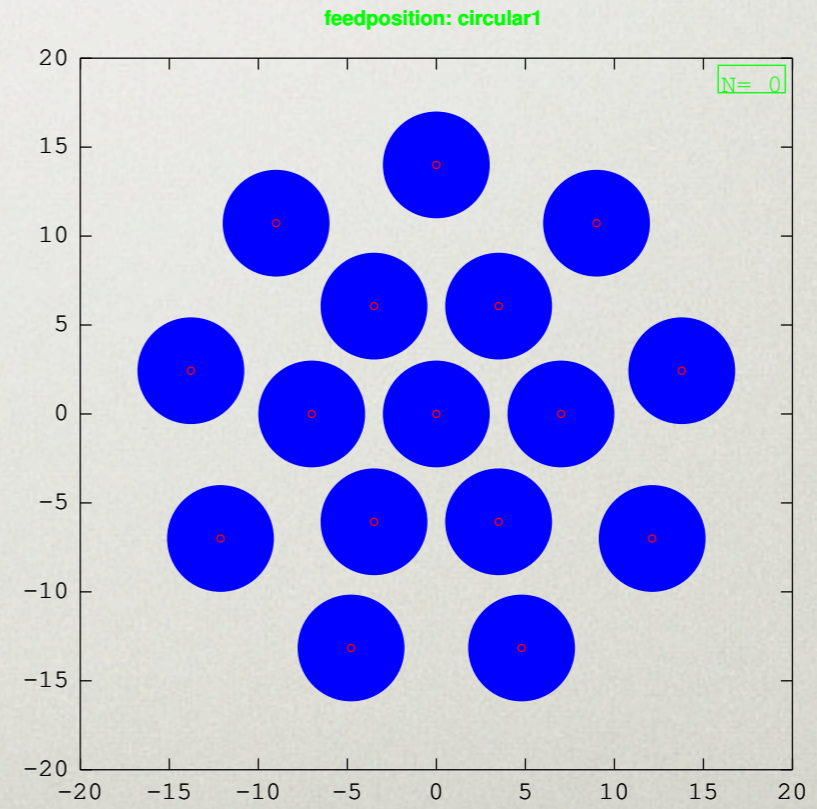
(a) regular



(b) circular



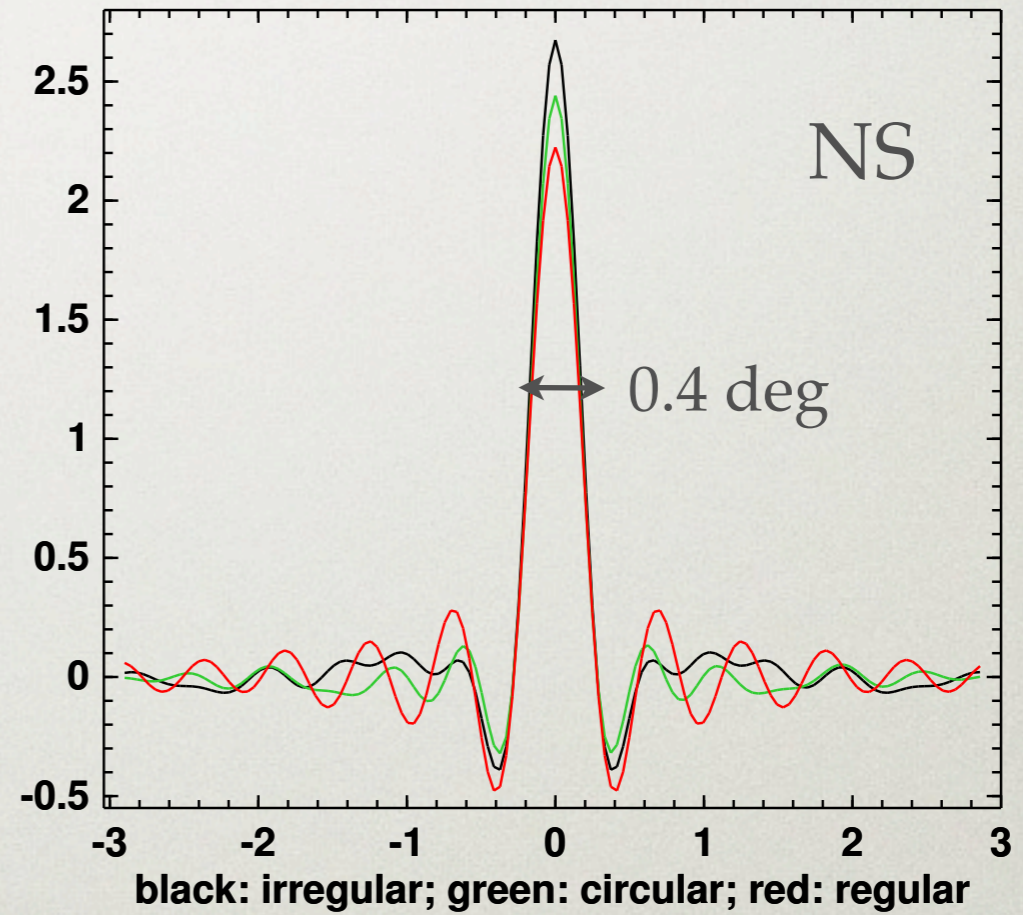
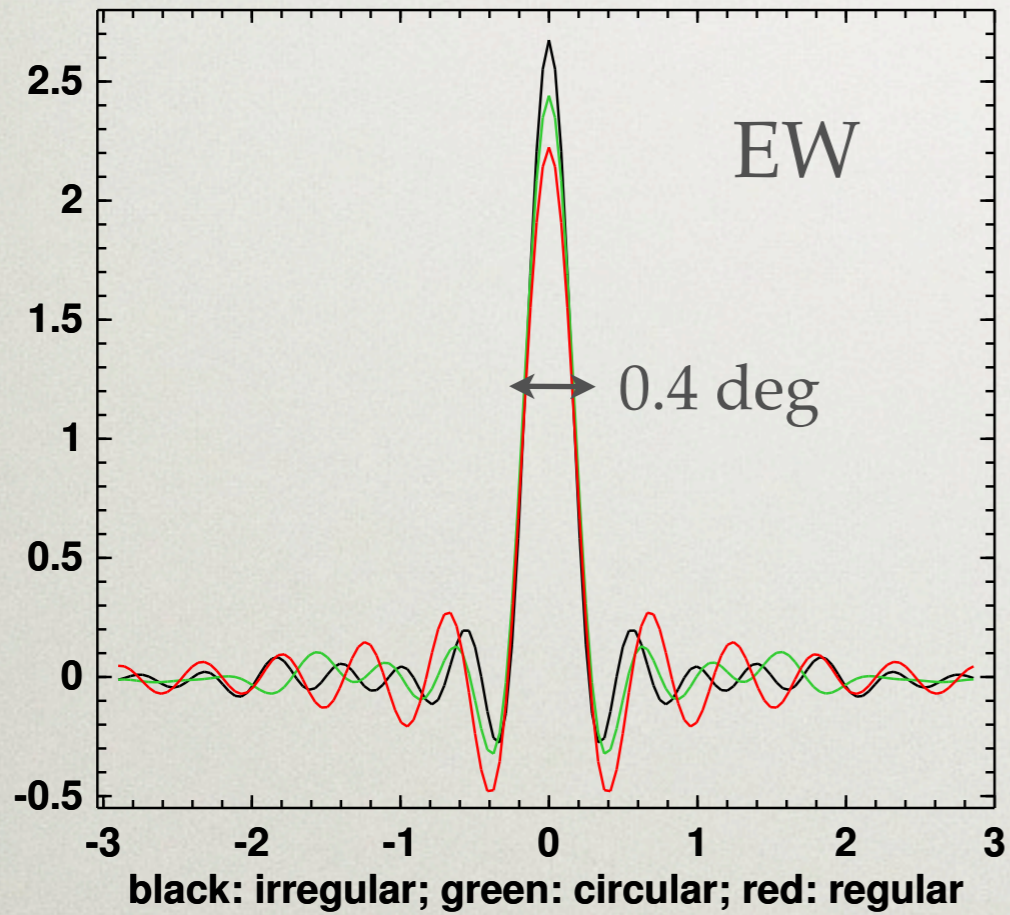
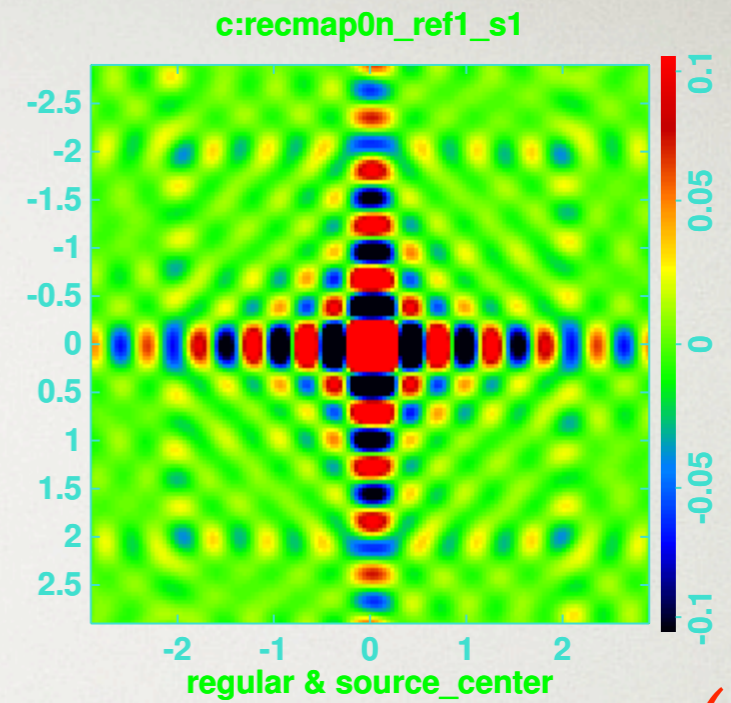
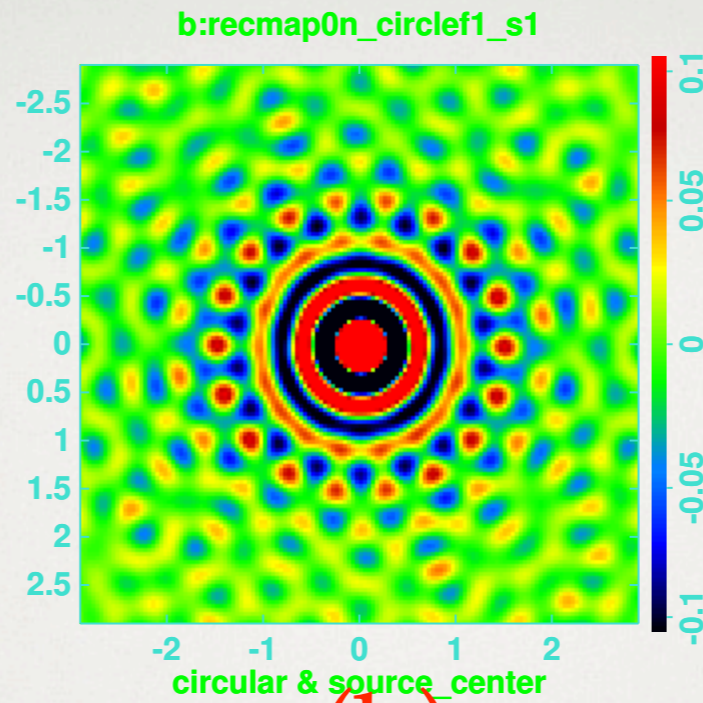
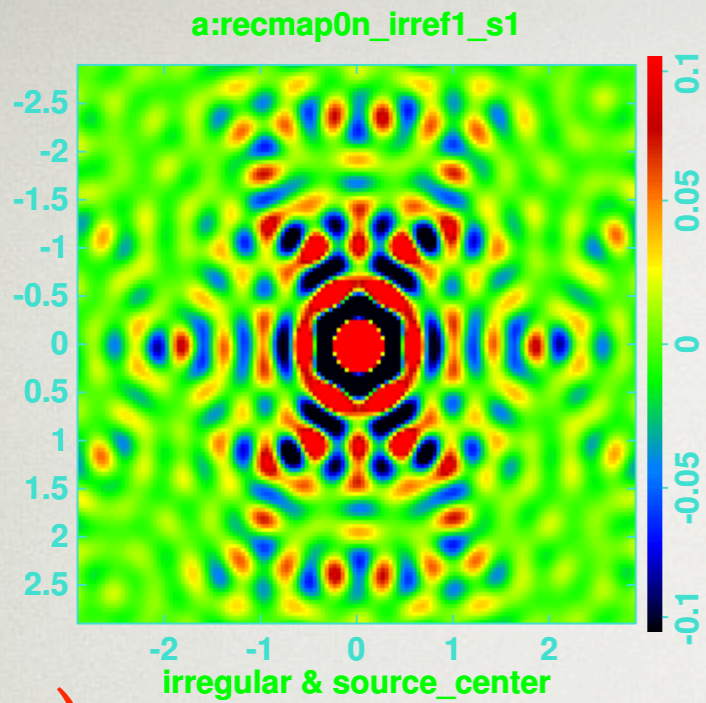
(c) irrregular



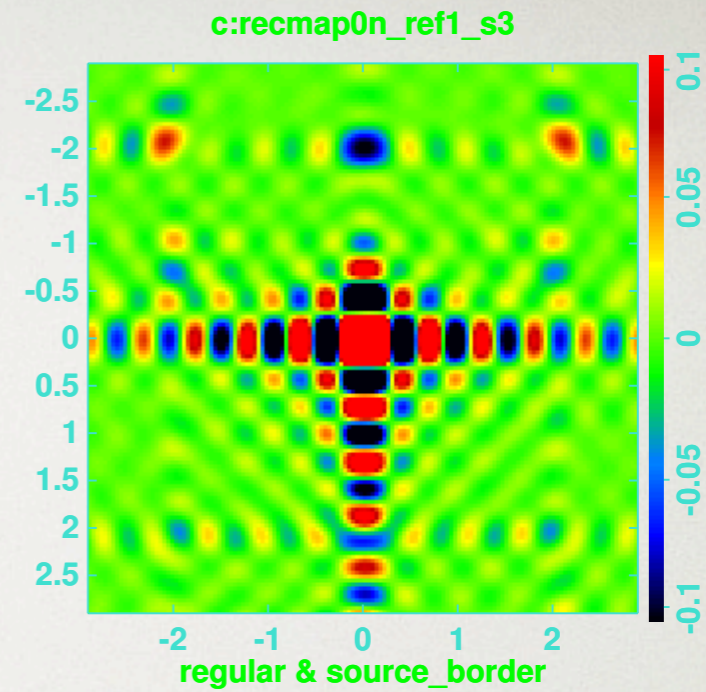
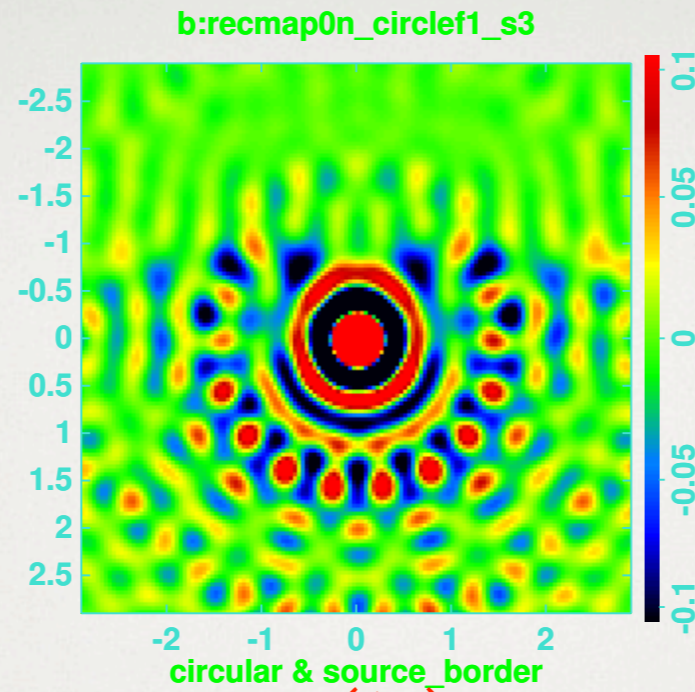
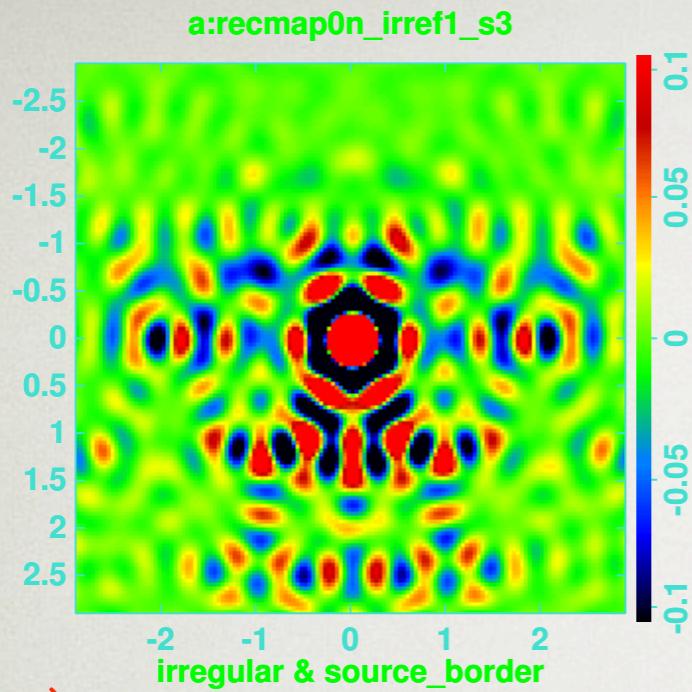
(d) circular-rotated

BEAM SHAPES

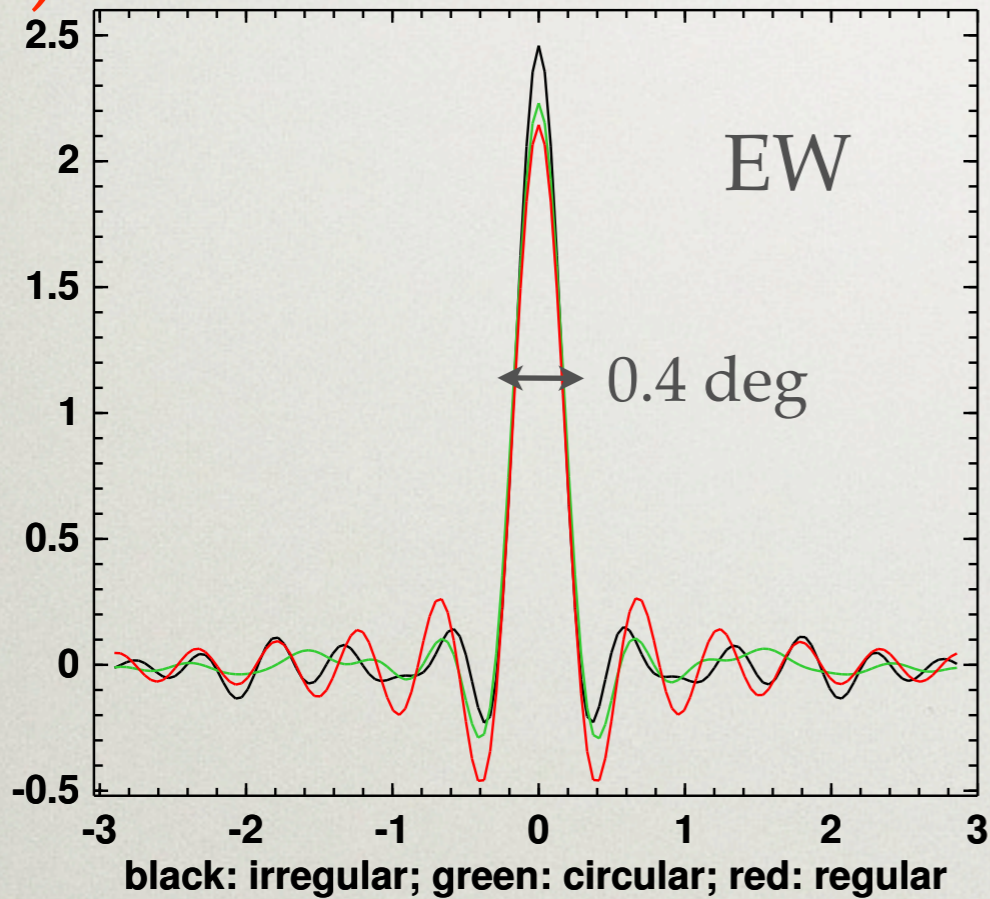
- Compute the reconstructed from the visibilities (without noise) for an input map with point sources at different declination
- The beam (response to a point source) depends on declination, but not on RA
- beam before and after applying weights on the (u,v) plane (cut/weight based on the computed noise covariance matrix, application of a frequency independent global beam)



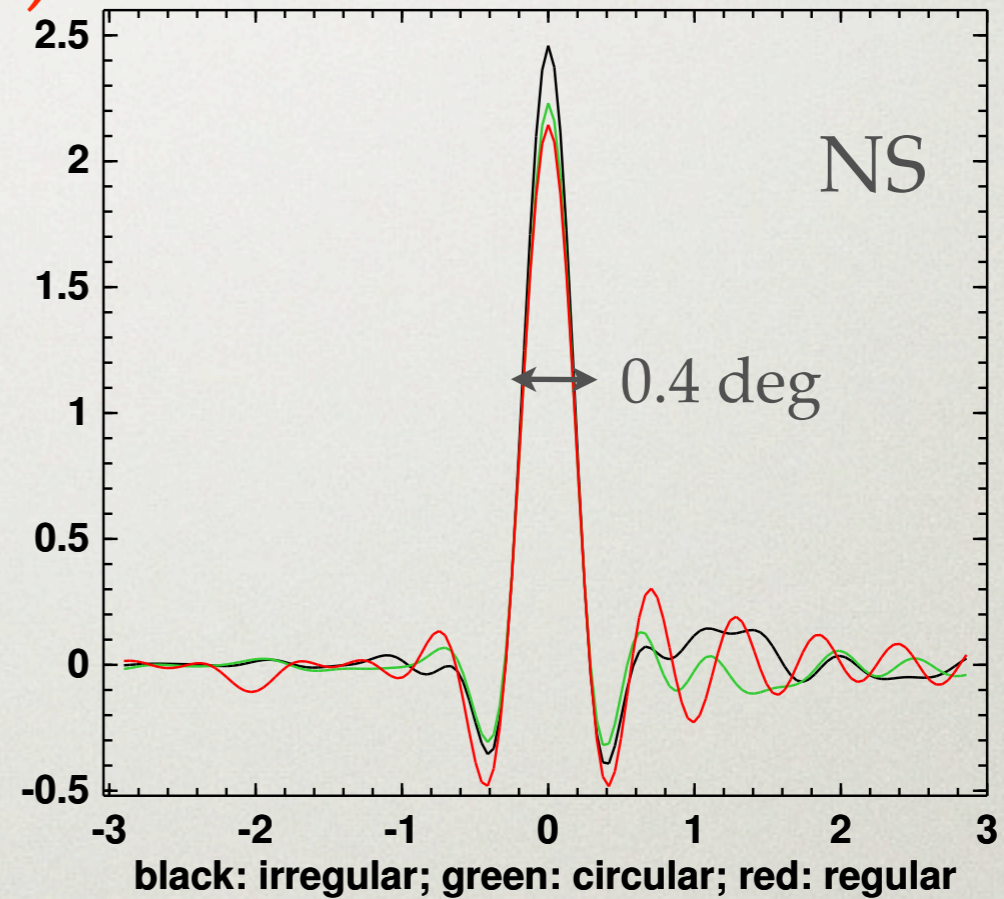
Beam at center (in δ) - 1200 MHz



(c) row_cut source_border

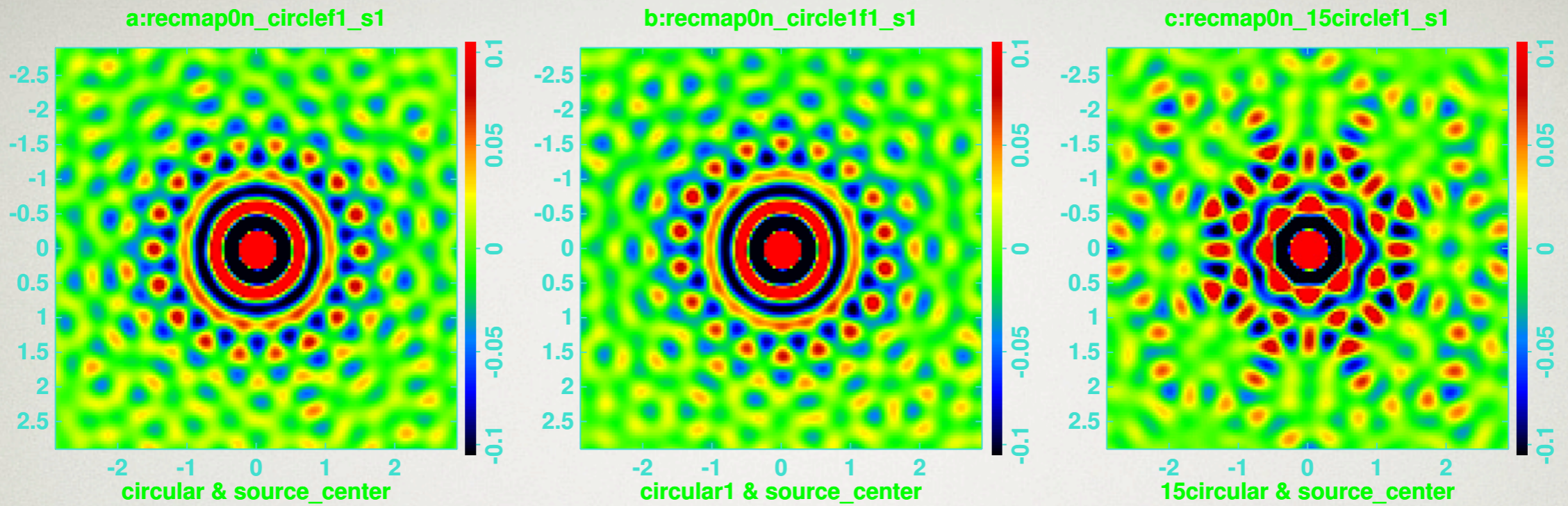


(b) column_cut source_border



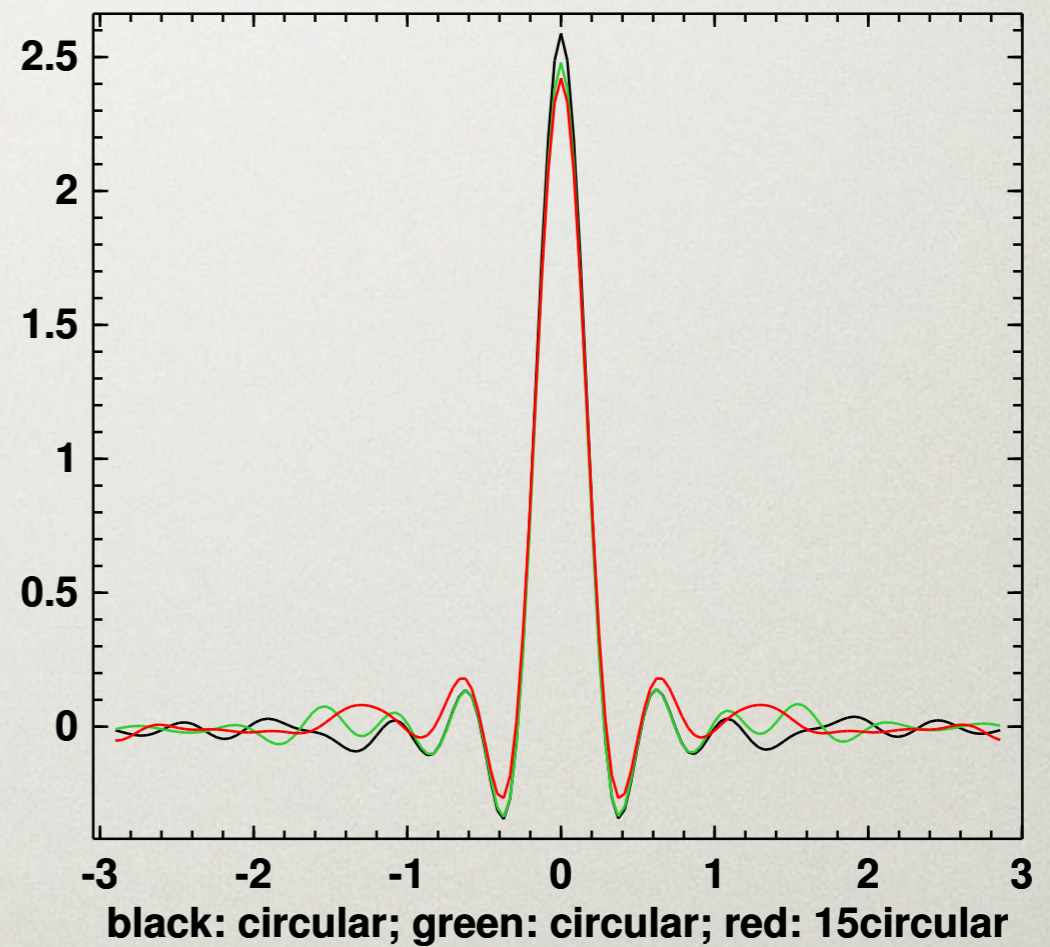
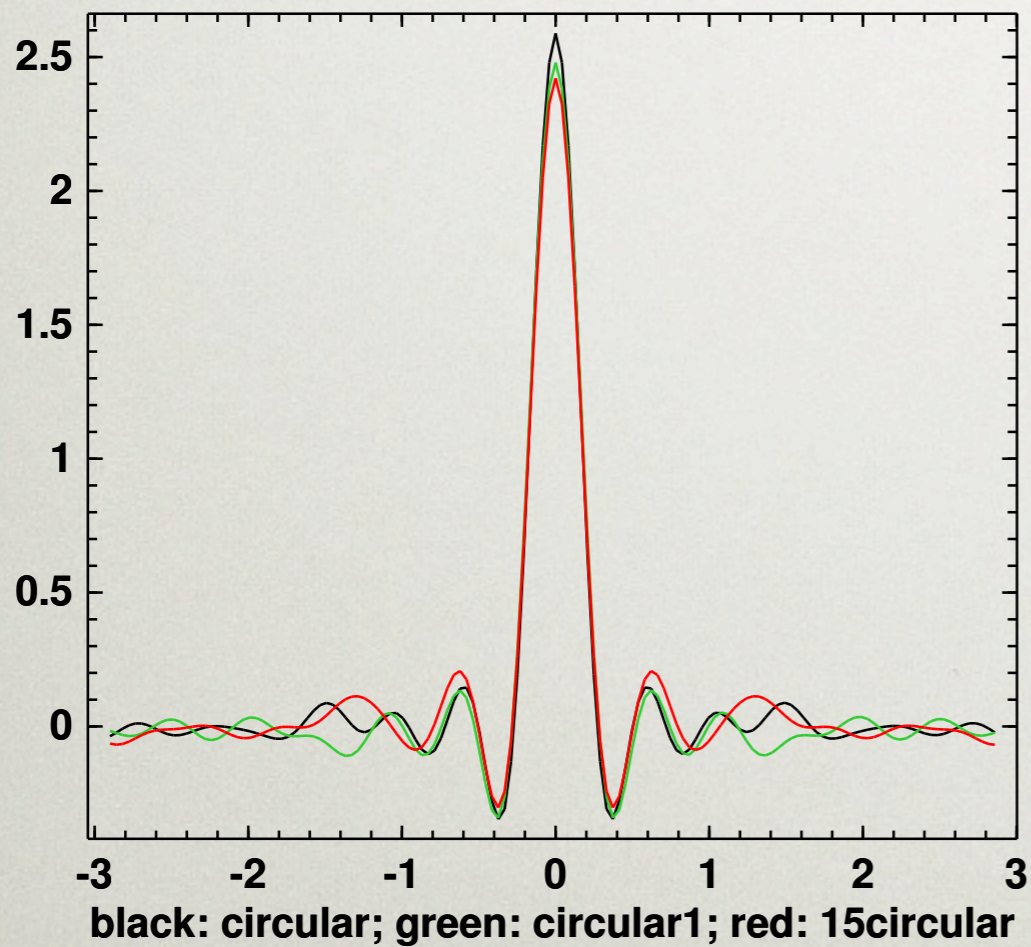
(a)

Beam at the edge (in δ) - 1200 MHz



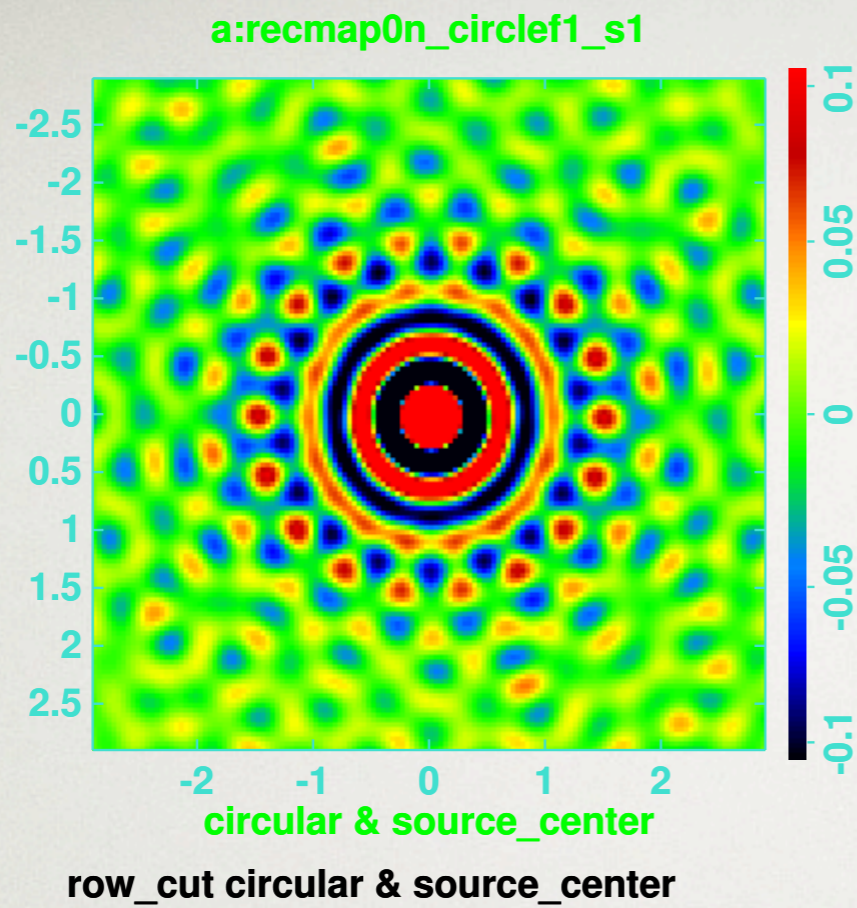
row_cut source_center

column_cut source_center

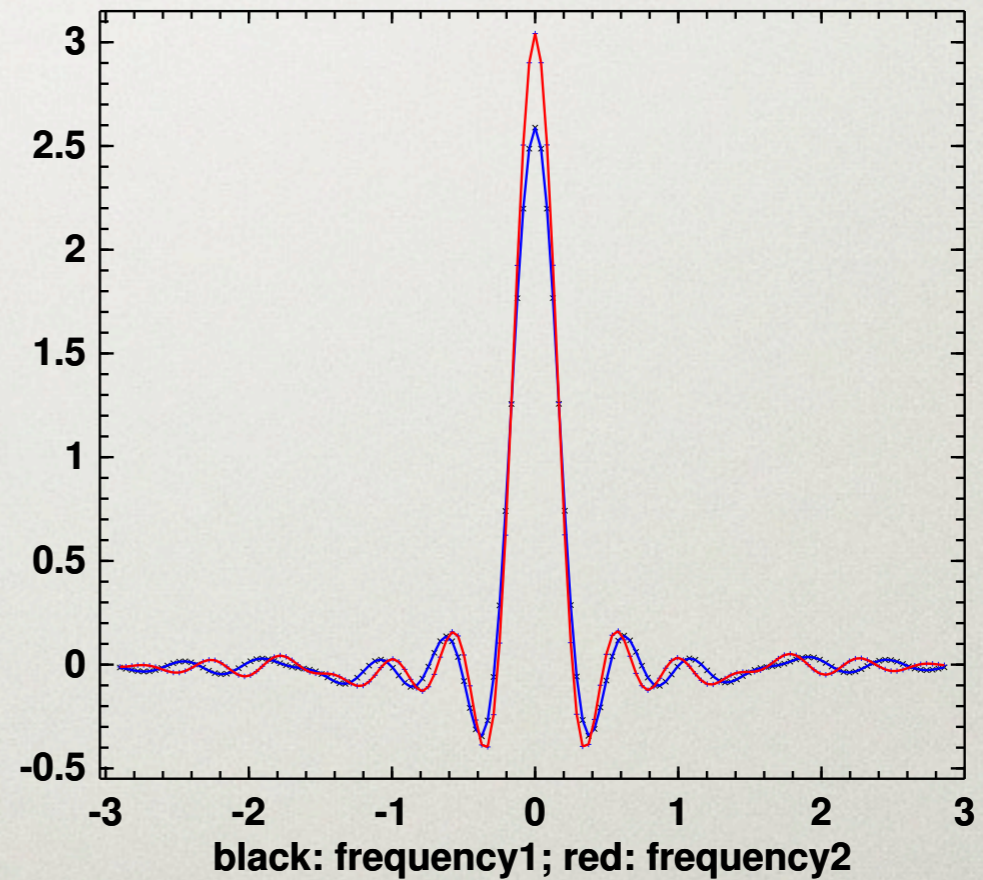
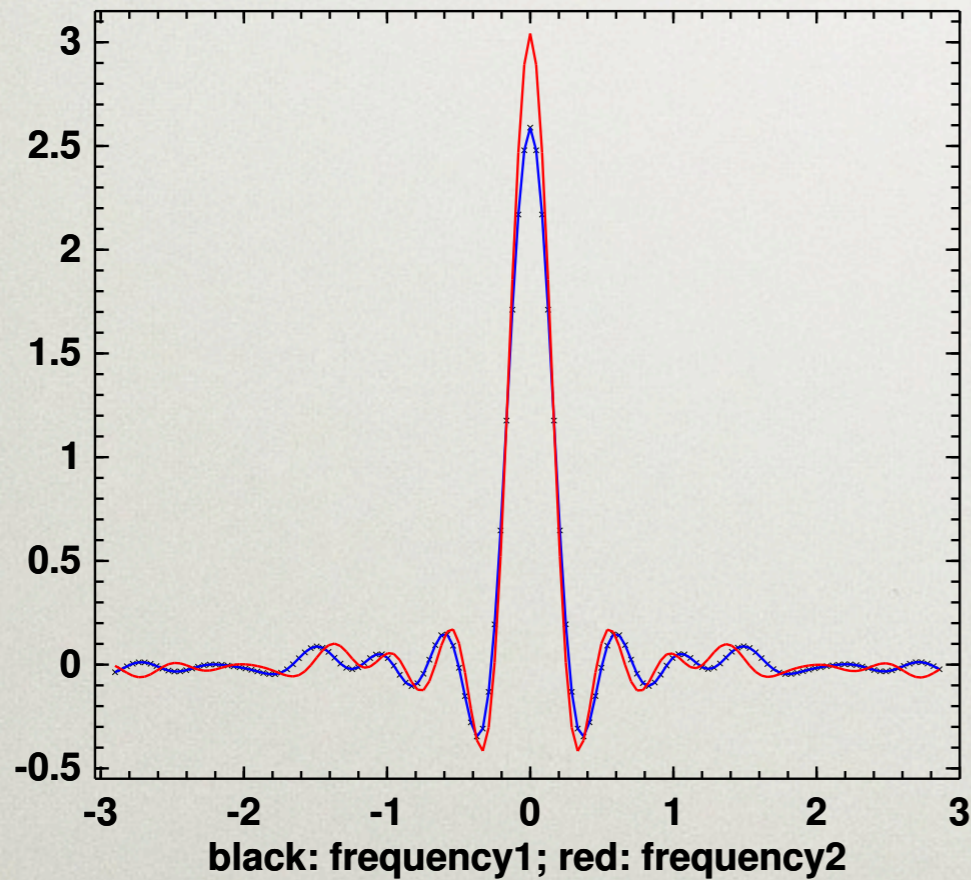
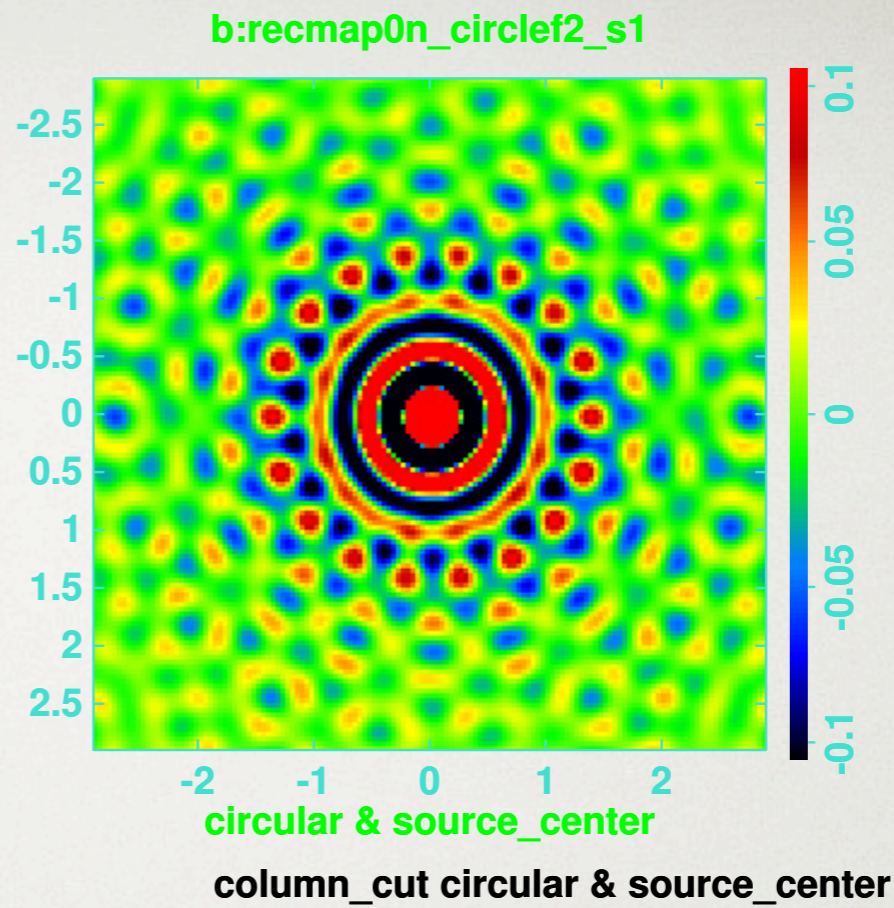


Beam at center for 2 16-dish circular configurations and one 15-dish circular

1200 MHz

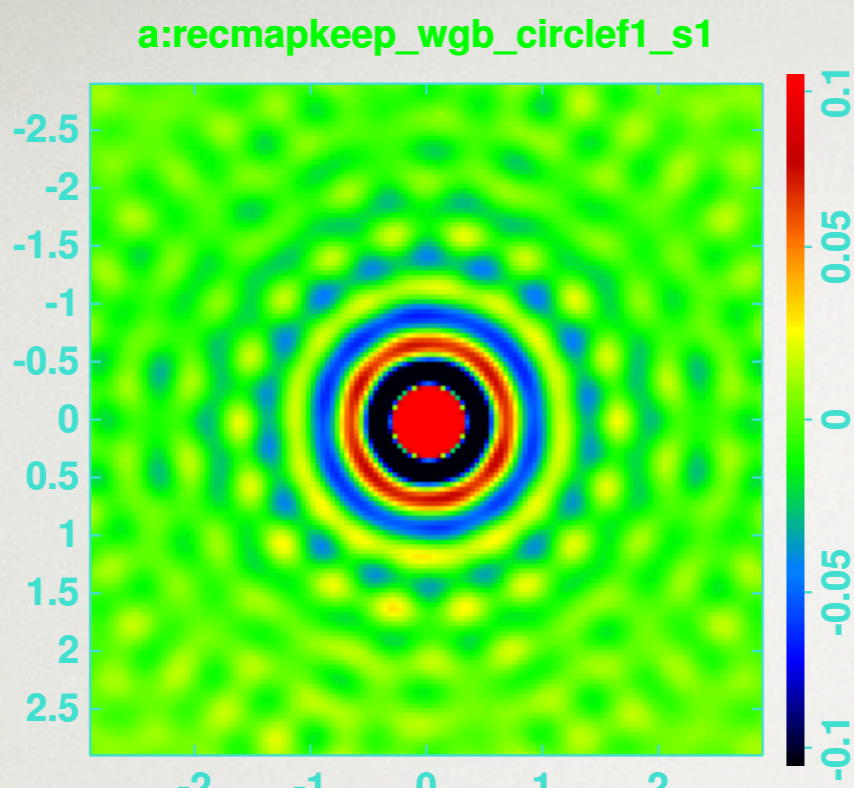


1300 MHz

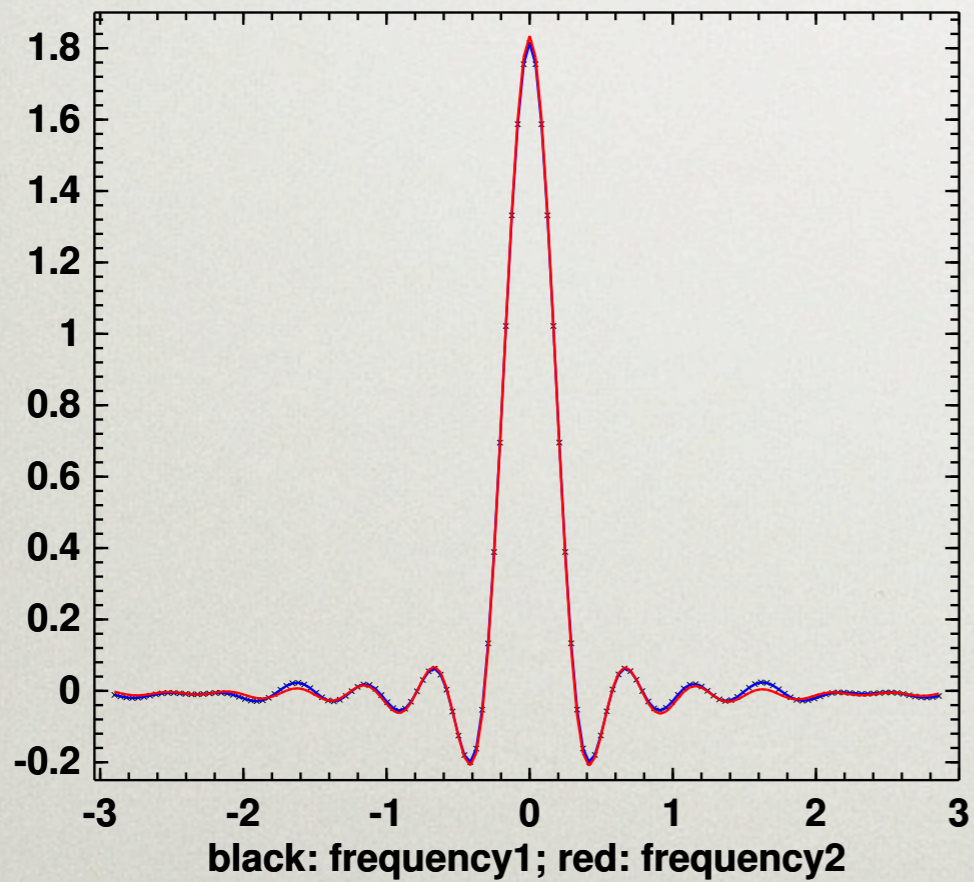


Beam frequency dependency - circular configuration (b) - 1200 MHz, 1300 MHz

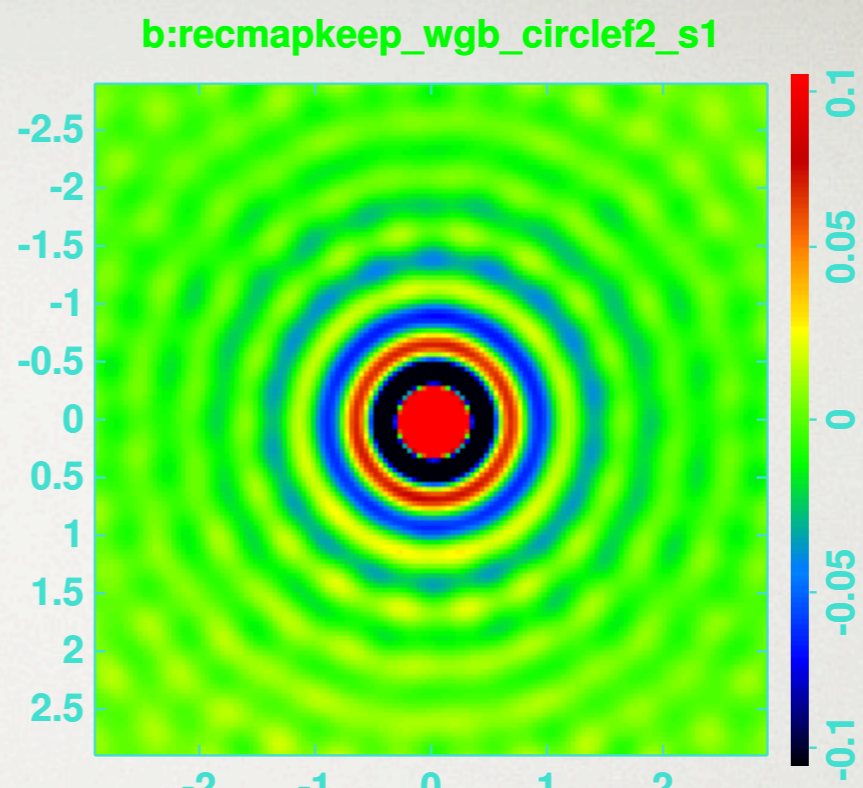
1200 MHz



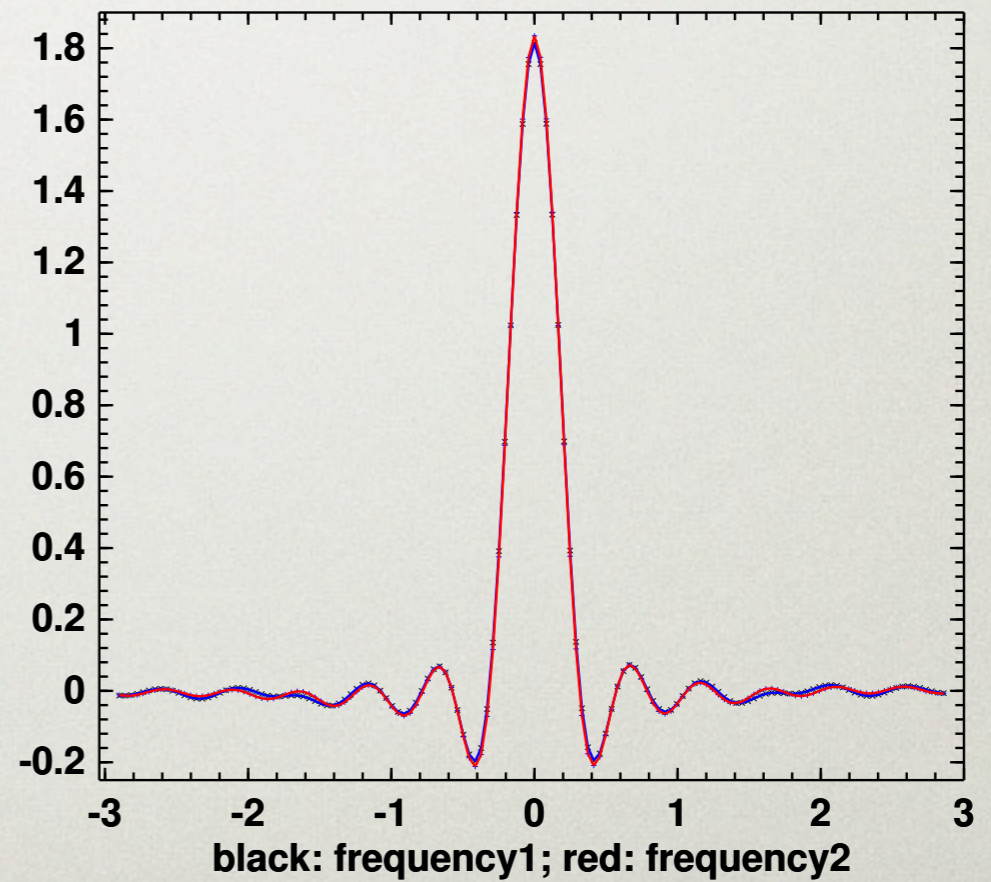
row_cut keep_circular & keep_source_center



1300 MHz

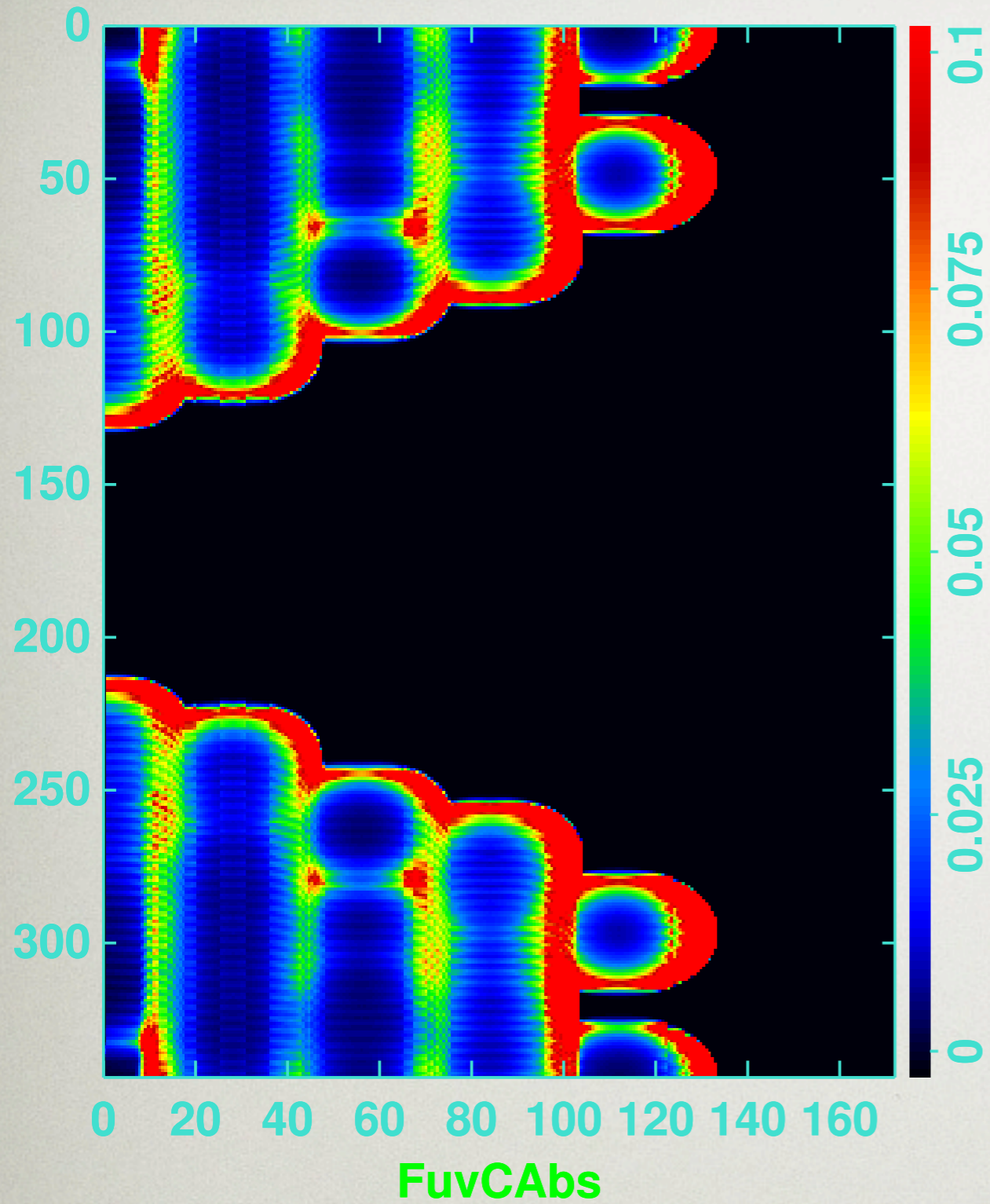


column_cut keep_circular & keep_source_center

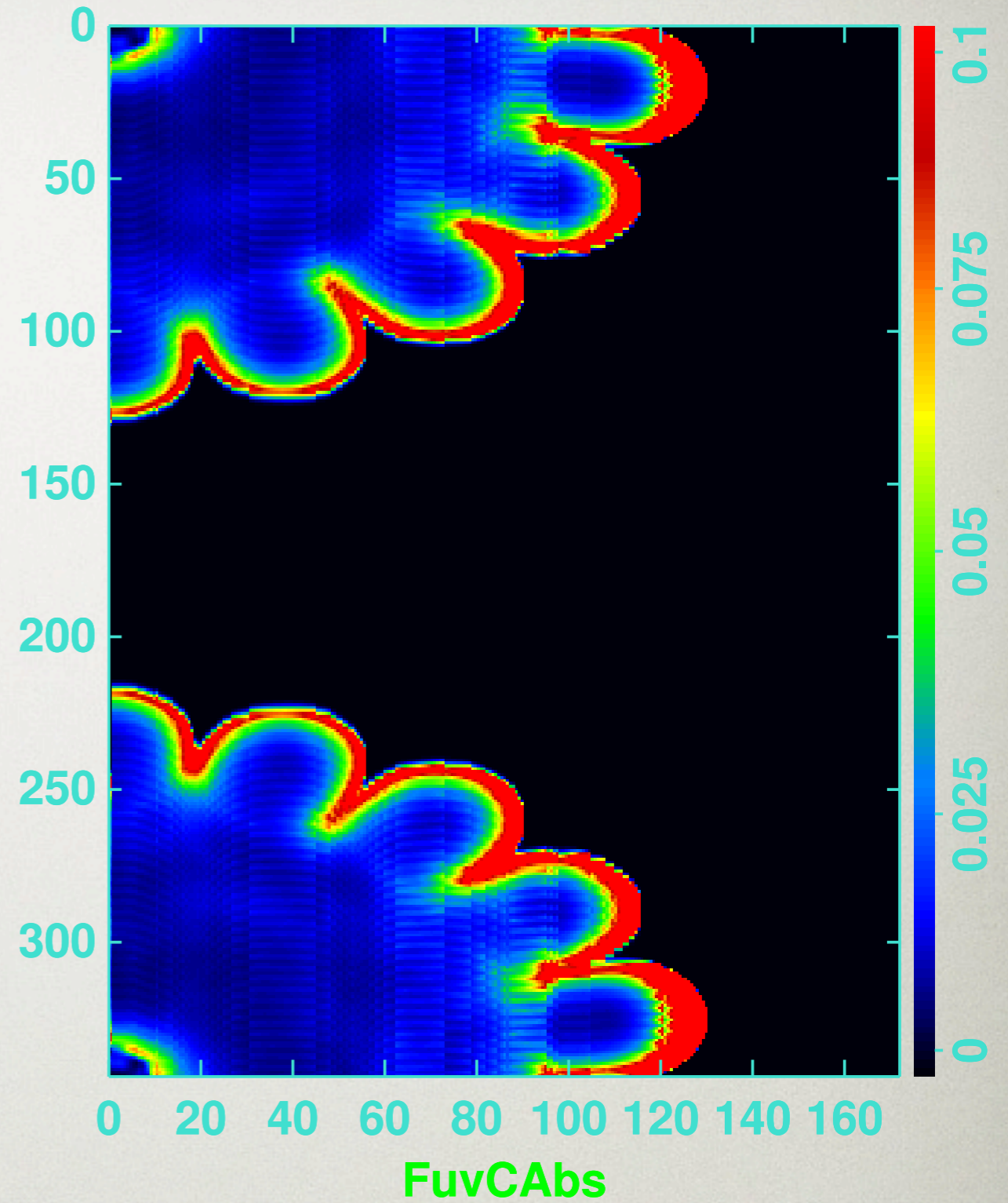


Applying a global weight function - circular configuration (b) - 1200 MHz, 1300 MHz

irregular



circular



Diagonal of the error covariance matrix for configurations (b),(c)

TRANSFER FUNCTION AND NOISE POWER SPECTRUM

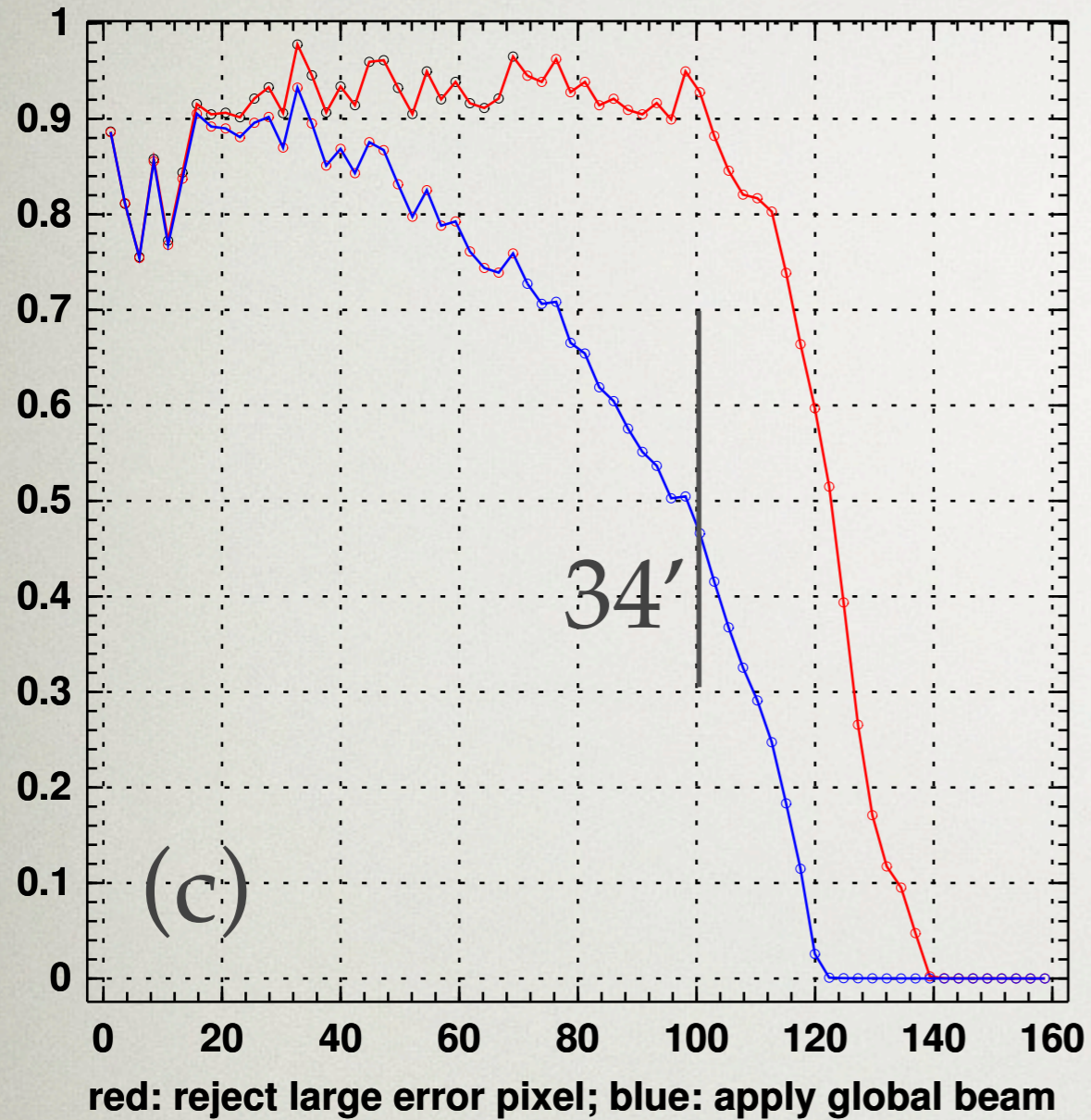
- $T(t_{\perp})$: Compute the reconstructed map for a white noise input map, compute the power spectrum of the reconstructed map
- Noise power spectrum: reconstruct the map with the visibility noise only ($F(u,v)=0$) and compute the power spectrum
- take the average over several input noise map / visibility noise realizations (single / few realizations right now)

$$t_{\perp} = \sqrt{u^2 + v^2}$$

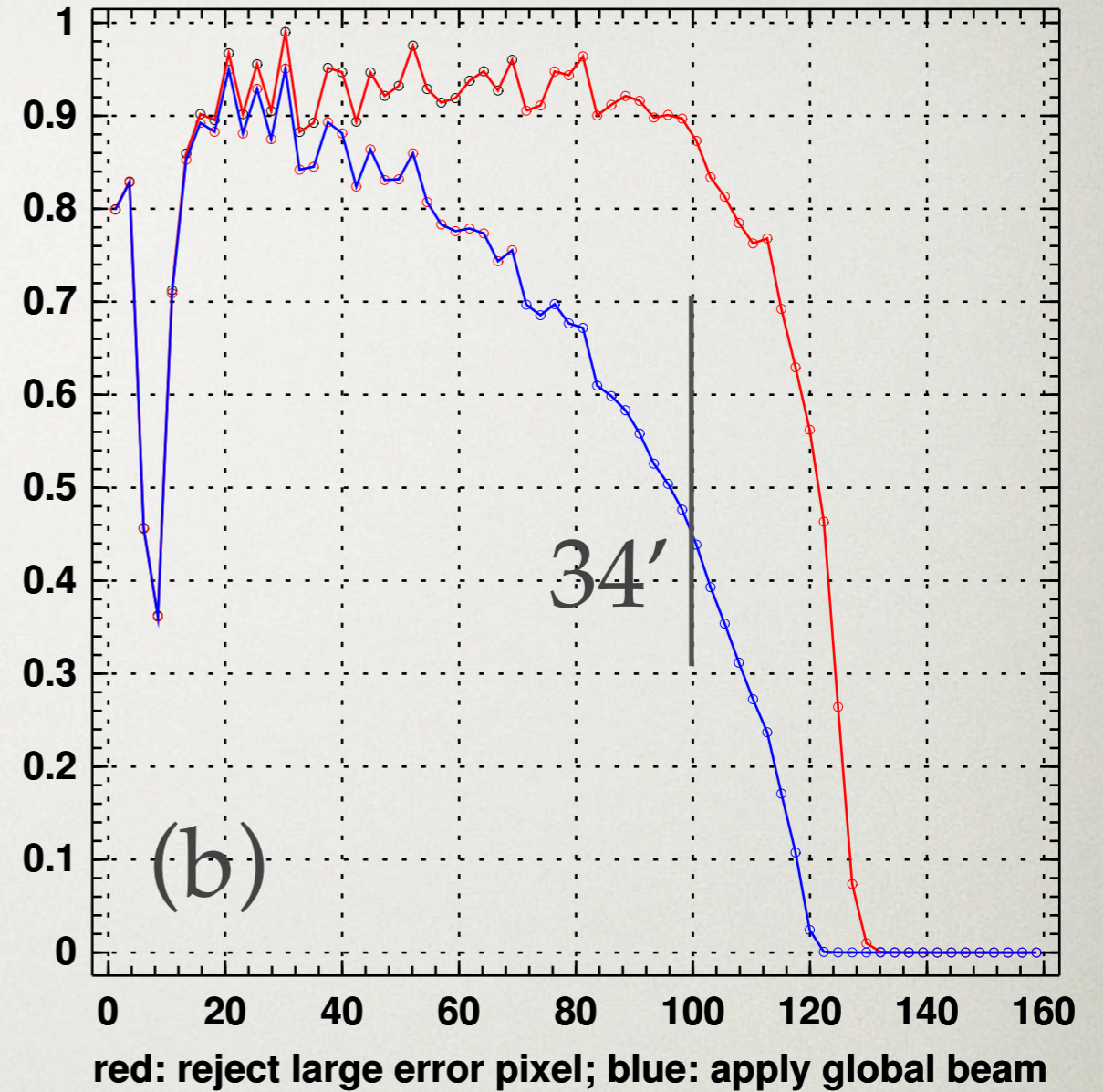
$$T(t_{\perp}) = \frac{P_{rec}(t_{\perp})}{P_{in}(t_{\perp})}$$

$$P_{noise}(t_{\perp}) = P_{noise-V}(t_{\perp})$$

transfer function for irre array

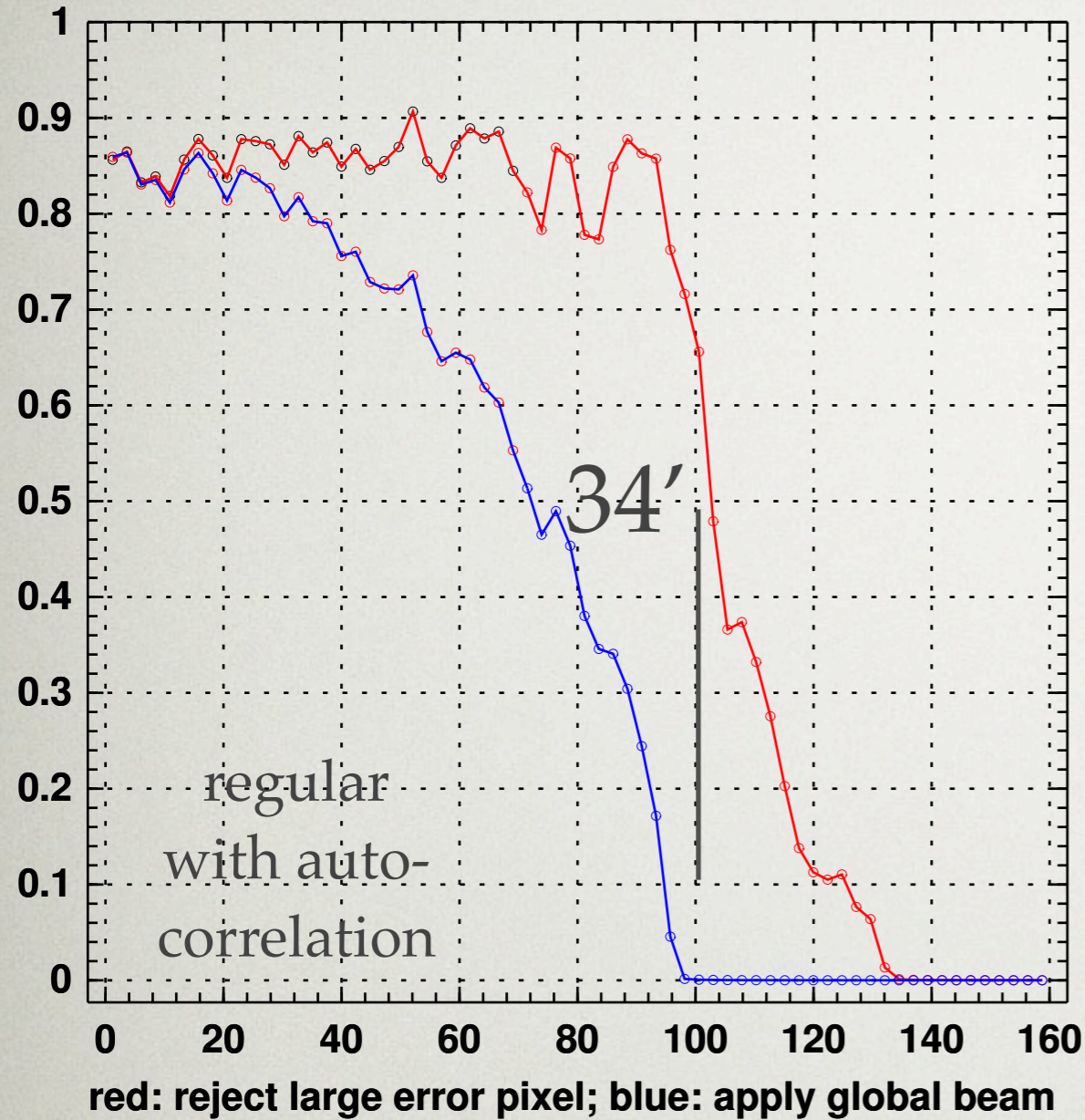


transfer function for circle array

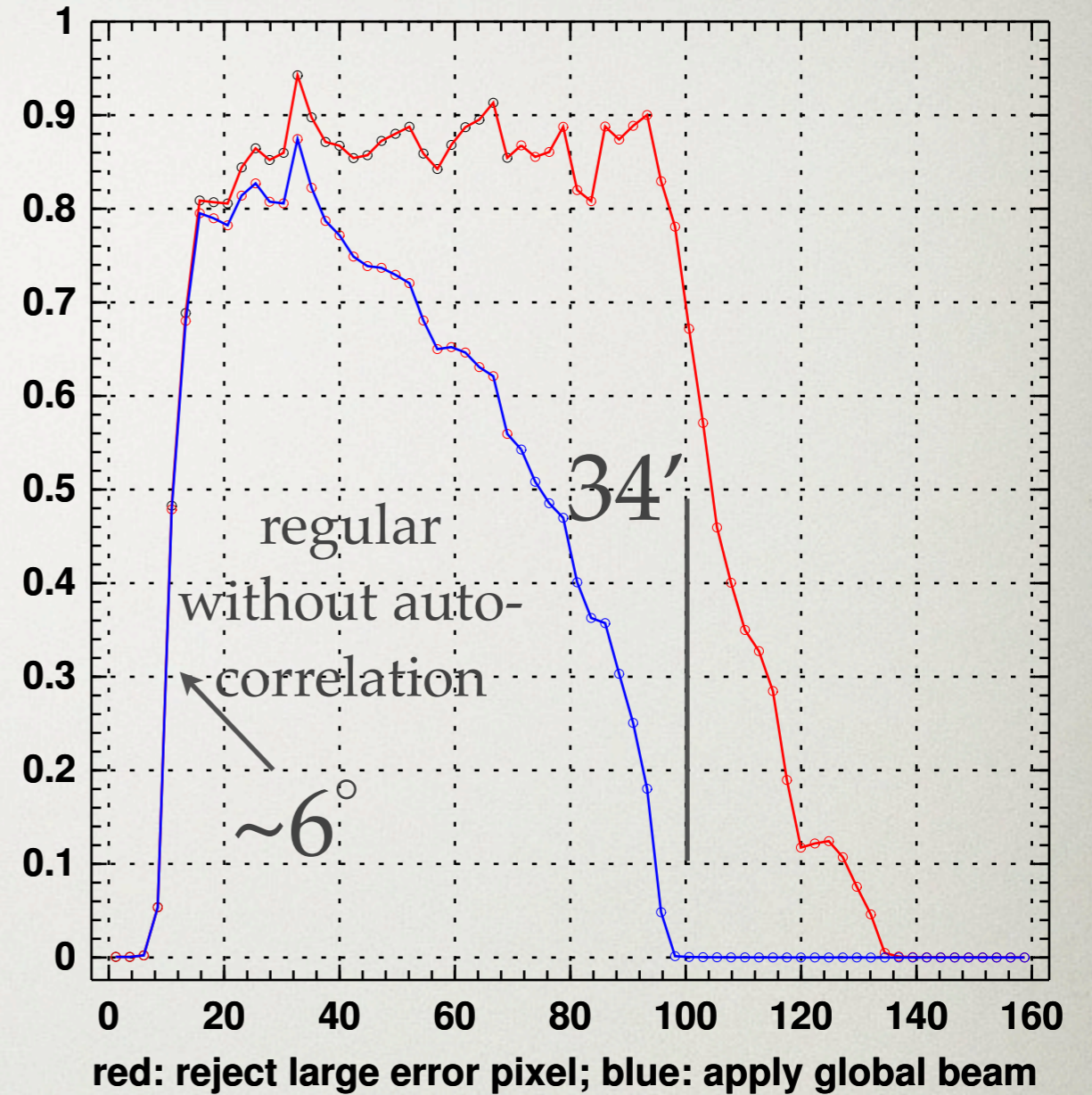


Transfer function for configurations (c)-
irregular and (b)-circular
rejecting high noise-variance modes (red),
and with global beam weighting (blue)

transfer function for re array



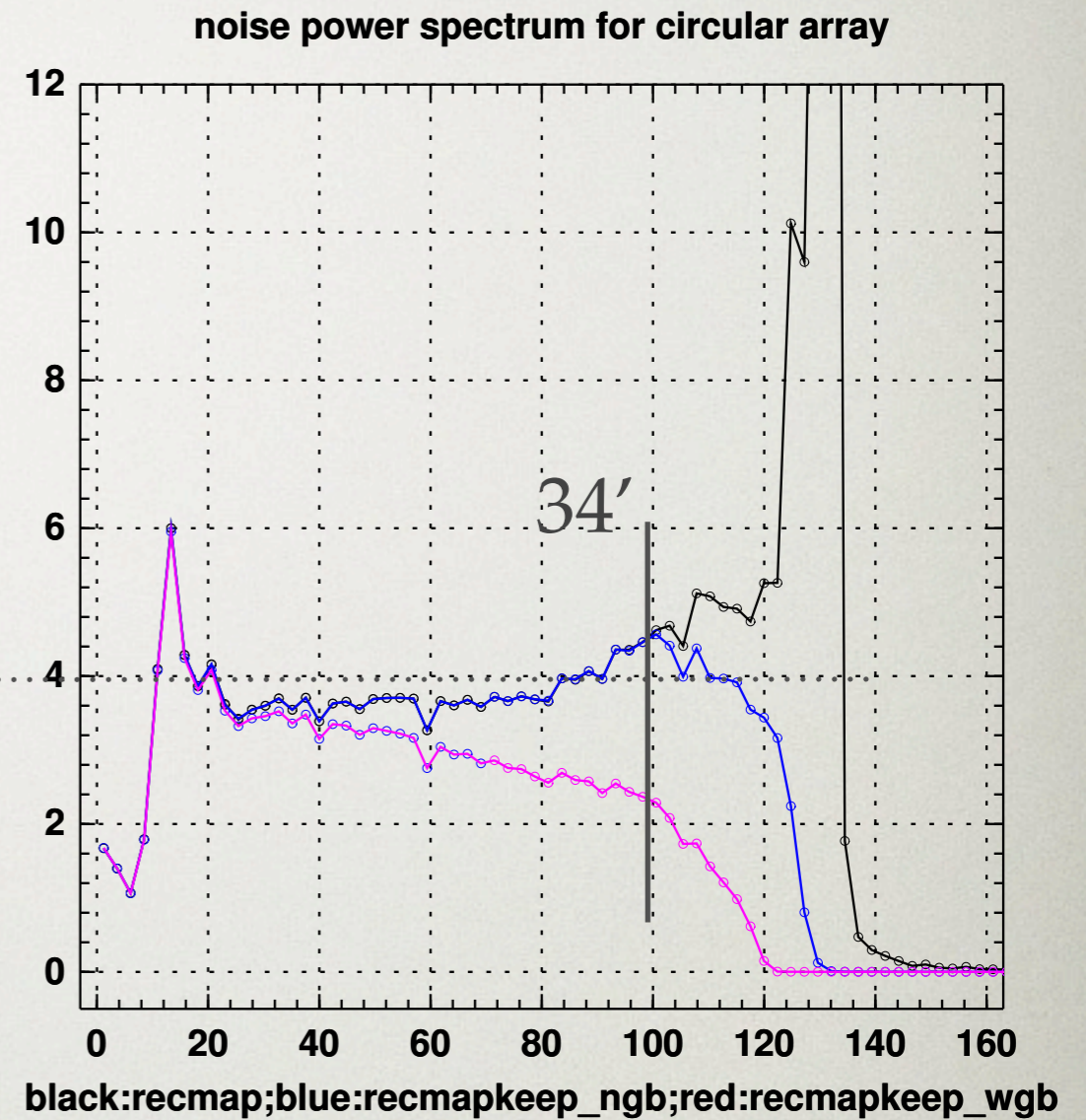
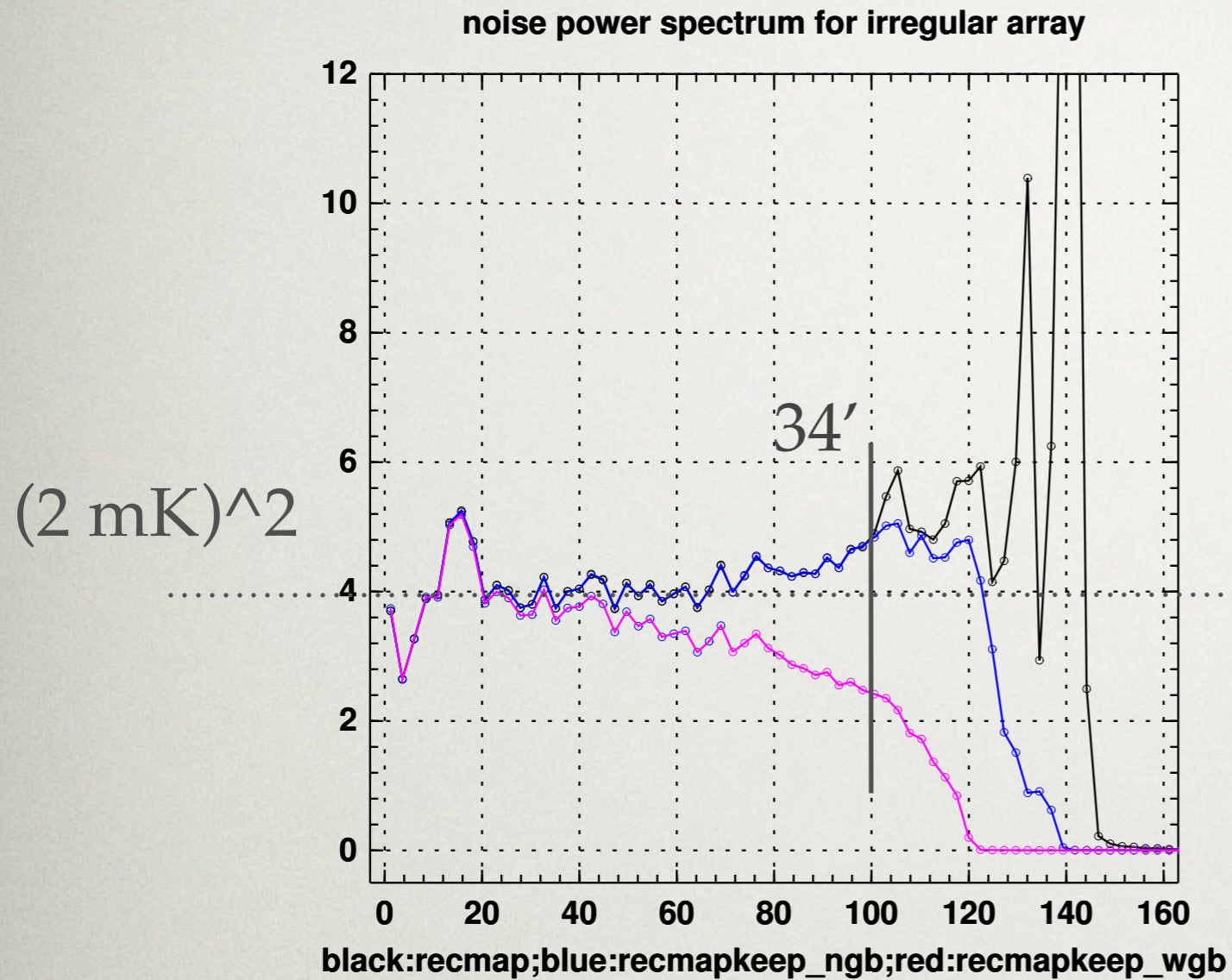
transfer function for regular_without_autocor array



Transfer function for configurations the regular array - with/without autocorrelations rejecting high noise-variance modes (red), and global beam weighting (blue)

Irregular array (c)

Circular array (b)

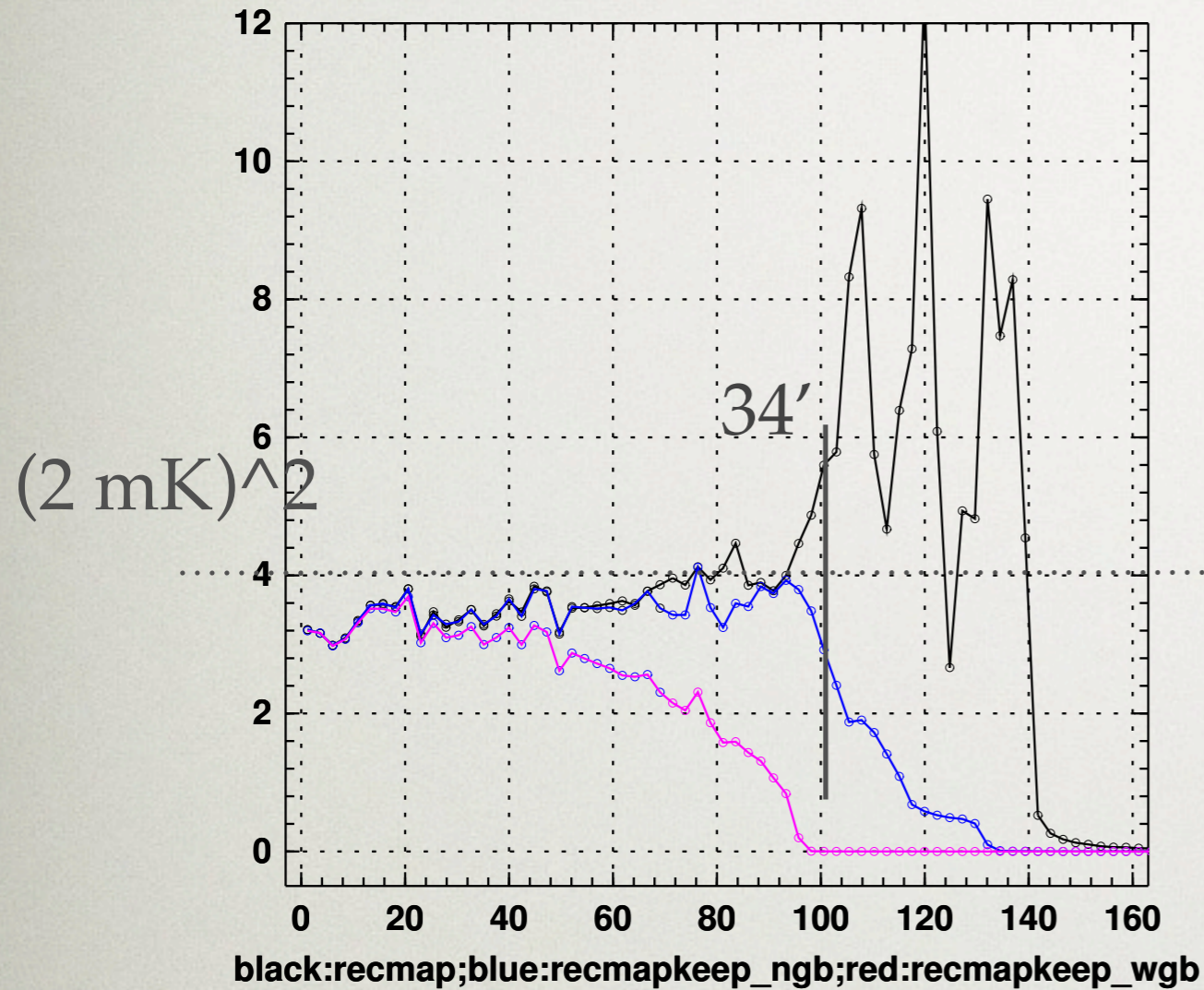


Noise power spectrum

$T_{\text{sys}} = 100 \text{ K}$, 6 month total observation time (9 scans), $\Delta\nu = 1 \text{ MHz}$, $\sim 250 (\alpha) \times 15 (\delta) \sim 3700 \text{ deg}^2$ covered (latitude $\sim 45 \text{ deg}$)

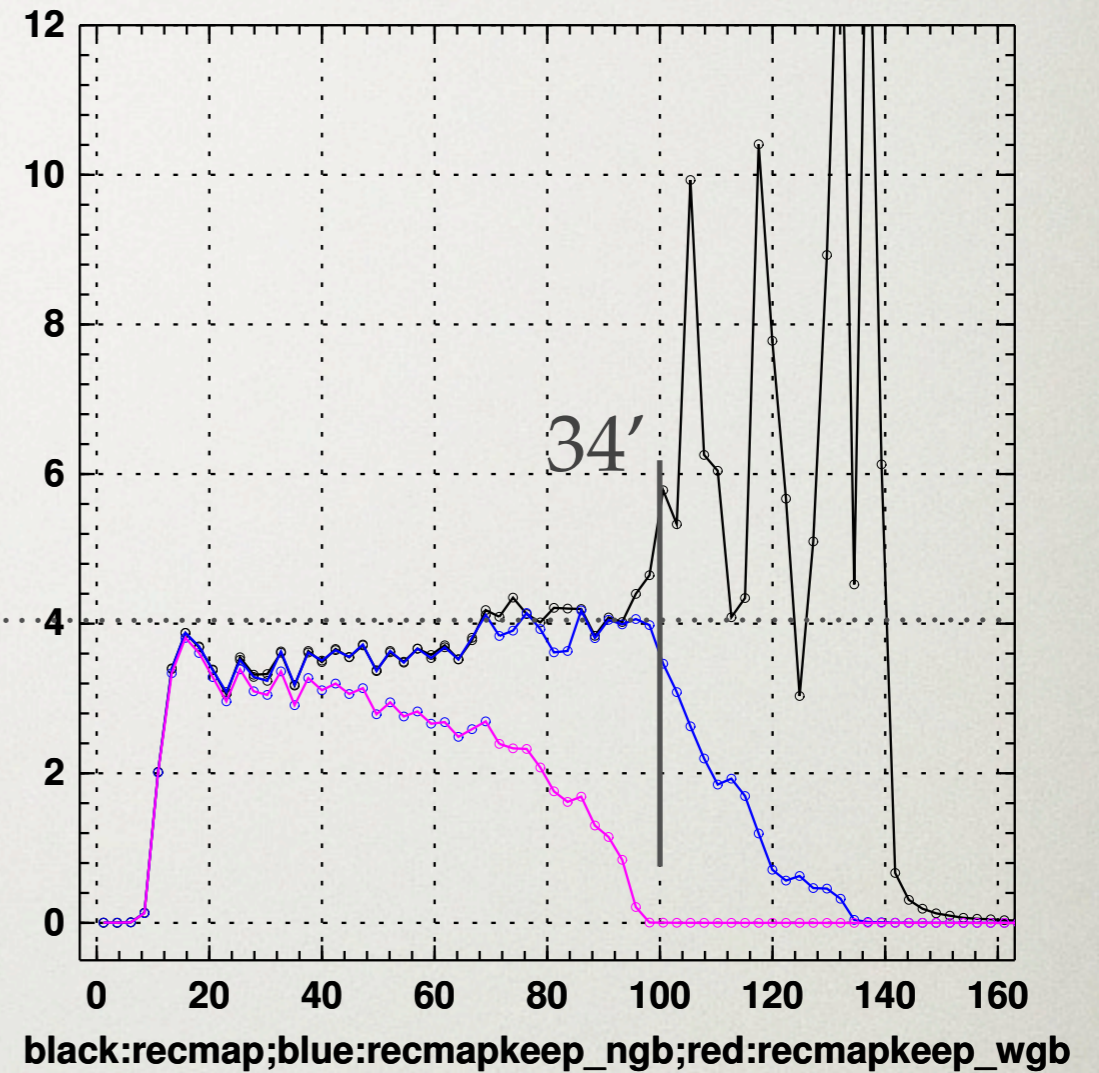
Regular array (a) with autocorrelation

noise power spectrum for regular array



Regular array (a) without autocorrelation

noise power spectrum for regular_without_autocor array



Noise power spectrum
regular array, with and without
autocorrelation

- better sky reconstruction with more independent baselines \rightarrow more uniform (u,v) plane coverage, better isotropy of the synthesized beam
- Possibility to optimize the beam, decreasing frequency dependency using weights on the reconstructed (u,v) plane
- Better reconstruction when increasing the number of δ scans (over the same sky area), without noise penalty
- Choice between (b)-circular or (c)-irregular configuration ?