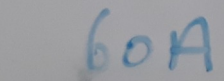
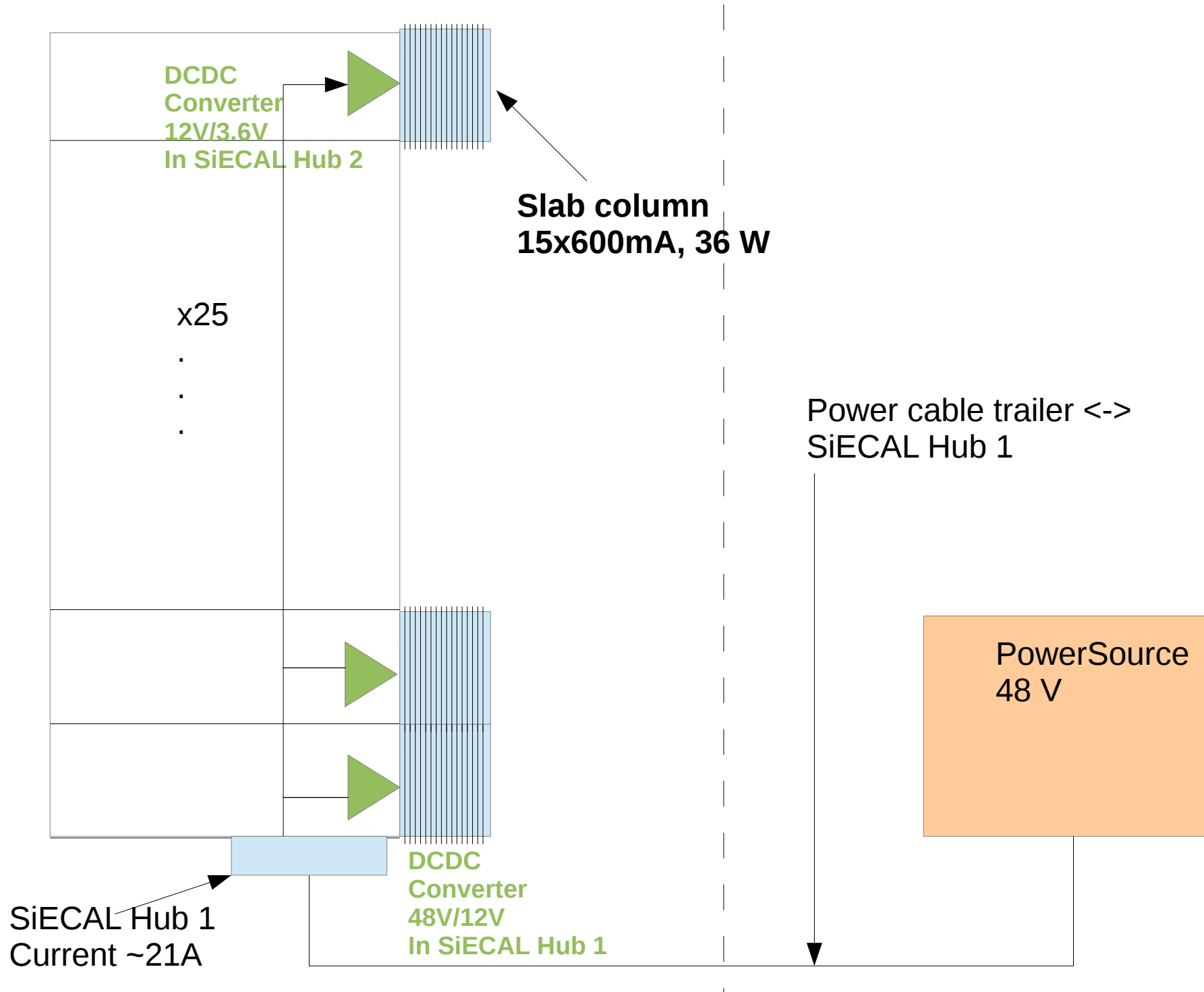


$1 \mu s \rightarrow 10 \text{ ms}$



$$R = 0,01 \text{ L}$$

Scheme of LV power supply for a stave



Scheme of LV power supply for a stave

0) Prologue: Specific Resistance of Copper $\rho = 0.0171 \text{ [Ohm} \times \text{mm}^2/\text{m]}$

1a) The (continuous) current consumption of a column of slabs is driven

i) by the consumption of the SL-Boards is (at approx. 4V): $I_{\text{SL}} = 200 \text{ mA} \Rightarrow 400 \text{ mA/slab}$

ii) by the charging current for the capacitances.

The inrush current will be limited to $I_{\text{C,max}} = 100 \text{ mA/layer}$. However, at $t > t_0$ the current will drop progressively according to $I = (U_B/R) \times \exp(-t/RC)$ with U_B = Voltage of power source and R = Resistance to limit the inrush current, e.g for $U_B = 4 \text{ V}$, $I_{\text{C,max}} = 100 \text{ mA} \Rightarrow R = 50 \text{ Ohm}$

1b) In this scenario it follows that the maximal consumption of a slab is

Current: $I_{\text{S,max}} = 2 \times (200 \text{ mA} + 100 \text{ mA}) = 600 \text{ mA}$

Power: $P_{\text{slab}} = P_{\text{SL}} + P_{\text{RC}} = 2 \times (4 \text{ V} \times 0.2 \text{ A} + 4 \text{ V} \times 0.1 \text{ A}) = \mathbf{2.4 \text{ W}}$ (again this drops as the capacitances get charged)

Power consumption of a column of slabs = $15 \times 2.4 \text{ W} = 36 \text{ W}$

1c) The 4V for SL-Board and capacitance charging is provided by 12V/4V DCDC Converters that sit in Hub2. This hub hosts also the data concentrator cards and that by itself consumes around 5 W. These 5 W add to the 36 W above, leading to a total power consumption of a slab column of 41 W.

Scheme of LV power supply for a stave

1) The total power consumption of a stave 41 W (=25 columns) is about

$$25 \times 41\text{W} = 1000\text{ W}$$

2) These 1000W have to be provided by the main power supply of 48 V from which it follows that current drawn from the power supply is 100

$$1000\text{W}/48\text{V} = 21\text{ A}$$

These 21 A arrive at the SiECAL Hub 1

3) According to a survey on the web 21 A require a cable with a cross section of about 1.5 mm² maybe 2.5 mm². The voltage drop per meter on such a cable at 21 A is

$$\Delta U = (0.0171/1.5)\text{Ohm} \times 21\text{A} = 0.24\text{ Volt} \Rightarrow \sim 5\text{ Volt after 20m in case of } 1.5\text{ mm}^2$$

with a thermal dissipation of $0.24\text{V} \times 21\text{A} \sim 5\text{W/m}$

$$\Delta U = (0.0171/2.5)\text{Ohm} \times 21\text{A} = 0.14\text{ Volt} \Rightarrow \sim 3\text{ Volt after 20m in case of } 2.5\text{ mm}^2$$

with a thermal dissipation of $0.14\text{V} \times 21\text{A} \sim 3\text{W/m}$

$$\Delta U = (0.0171/4)\text{Ohm} \times 21\text{A} = 0.09\text{ Volt} \Rightarrow \sim 1.8\text{ Volt after 20m in case of } 4\text{ mm}^2$$

with a thermal dissipation of $0.09\text{V} \times 21\text{A} \sim 2\text{W/m}$

Concerning the cable thickness we need to find a compromise between material budget and thermal dissipation

=> Propose to choose 2.5 mm² for the time being (requires coordination with other detector components)

“External” Material budget on cables

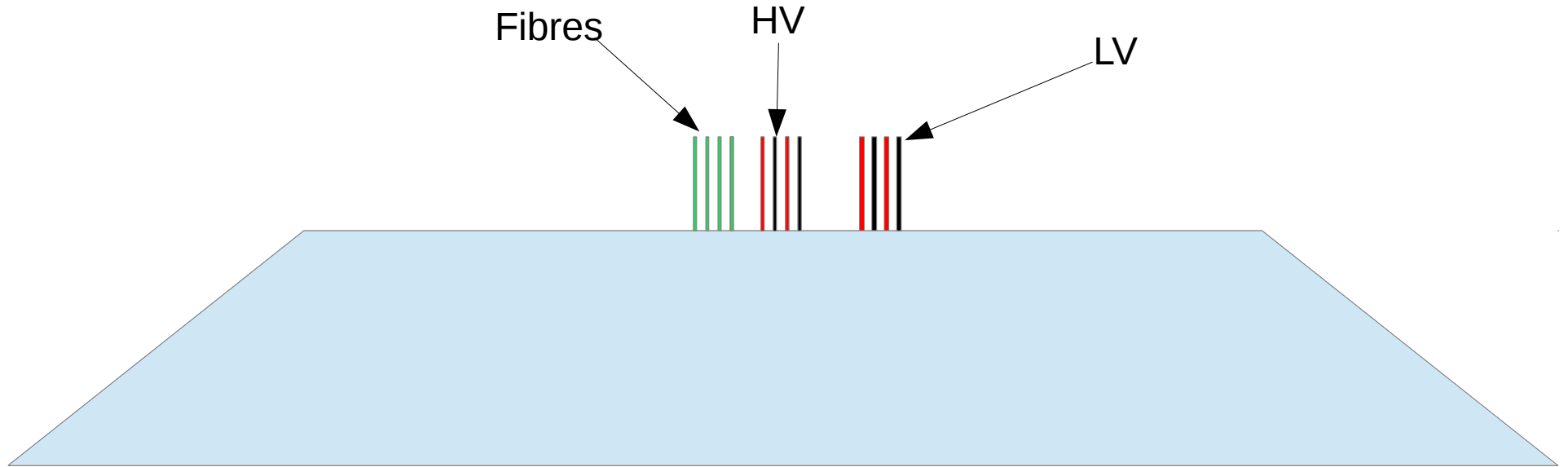
i.e. Cables arriving at SiECAL Hub 1

- 1) A copper cable of 2.5mm^2 has a diameter of about 1.8mm
The copper cables for the LV will occupy a space of about $7.2 \times 1.8\text{ mm}^2$
This assumes one cable for the ingoing current and another one for the return current (x2 for redundancy)

Remark: The radiation length of copper is 14.36 mm

- 2) The budget added by the HV can be neglected (Current $\ll 1\text{A}$)
- 3) There will/may be also optical fibres for data transfer and clock distribution
Let's assume four including redundancy
The additional material budget is however negligible

“External” Material budget on cables – Simple Drawing



- Not to scale!!!
- To be turned into a professional drawing

Backup

<http://www.learnabout-electronics.org/PSU/psu31.php>

<https://www.maximintegrated.com/en/app-notes/index.mvp/id/2031>

Scheme of LV power supply for a stave – On DCDC Converters

... a poor man's point of view

- The advantage of a DCDC converter is that it realises the step down of the voltage **without** ohmic losses (in contrast to a “simple” linear regulator)

- From a “crash course” on DCDC converters I have learned that energy is stored in an inductor during time t_{on} and released during a time t_{off}

The output of a (Buck) DCDC Converter is $V_{out} = V_{in} \times t_{on} / (t_{on} + t_{off})$

The duty cycle V_{out} / V_{in} determines the average current that is drawn from the power source V_{in}

- At each layer the voltage 4V is available from a 12V/4V DCDC Converter.
The total current of a layer is 200mA (regard SL-Boards only for simplicity)

- Therefore the average current drawn from the power source is in this case
 $(4/12) \times 200\text{mA} = 66\text{mA}$