



# Lattice design and optimisation of the 250 MeV version of PERLE

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**Motivation for 250 MeV stage** ( pros and cons )

**Lattice design** ( maximal compatibility with 500 MeV design prepared by Alex Bogacz )

- general layout
- common beam pipe sections
- spreaders / mergers

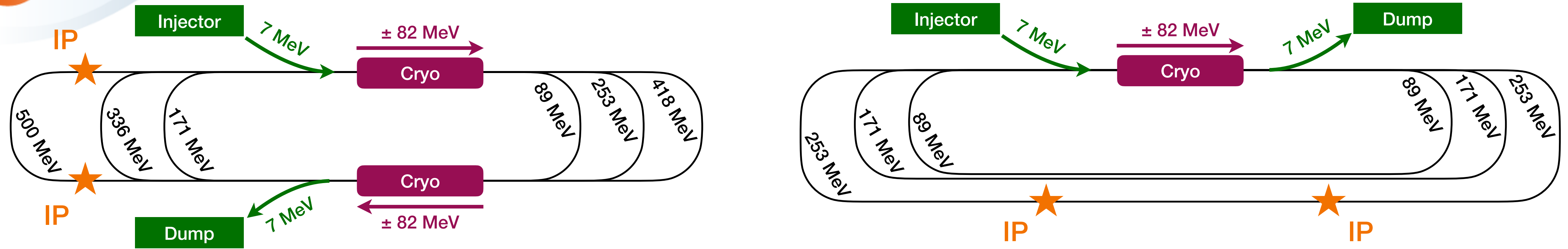
**Filling patterns** ( optimal for lower energies )

**Optim6 → MadX** ( optimal for lower energies )

**Conclusions**



# 500 MeV → 250 MeV ?



## Pros:

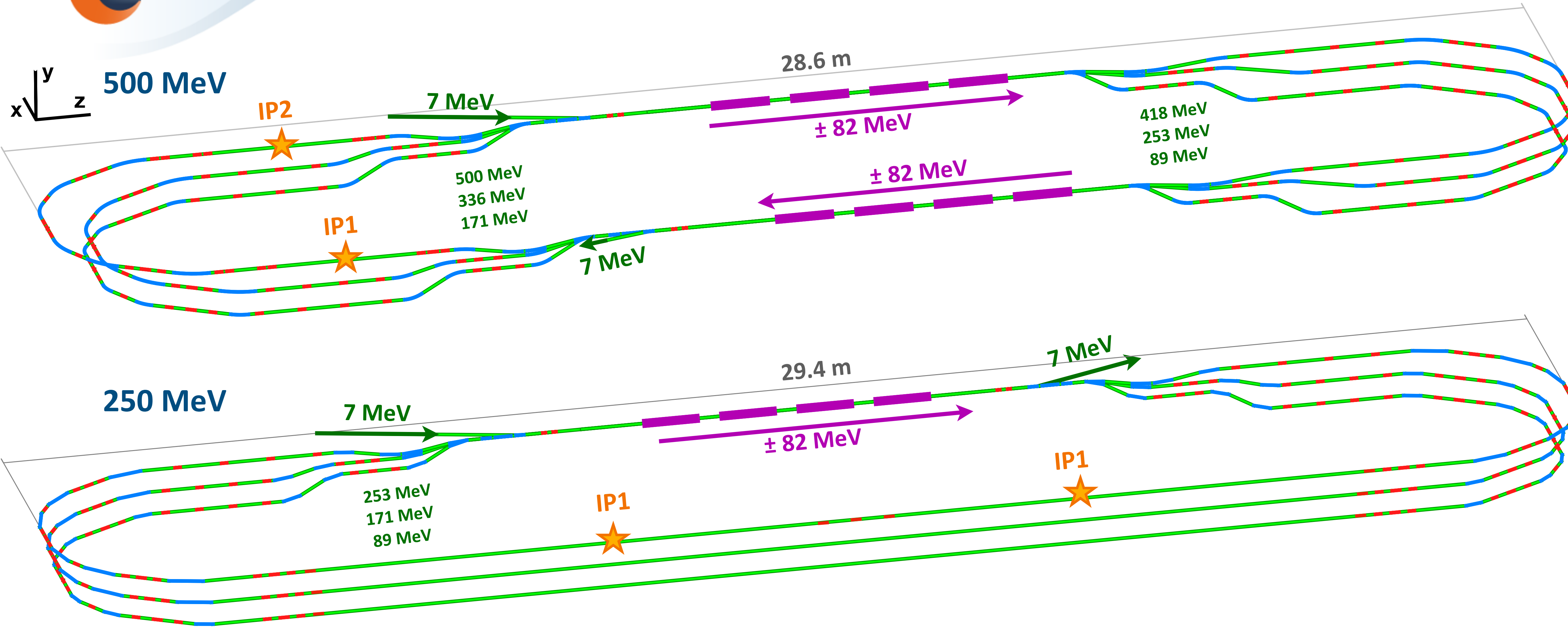
- **reduction of immediate expenses (time for the first results)** ( second cryo-module and 18 dipoles can be purchased later )
- **demonstration of ERL with 6 paths at high current** ( same as in 500 MeV version, but with half of the power )
- more space for experimental areas

## Cons:

- **additional expenses / manpower / shutdown time** ( rebuilding / recommissioning for the full power machine )
- about 30 meters of extra beam pipes ( all other main elements are chosen to be compatible with both versions )
- a slightly larger footprint ( 28.6 m → 29.4 m )



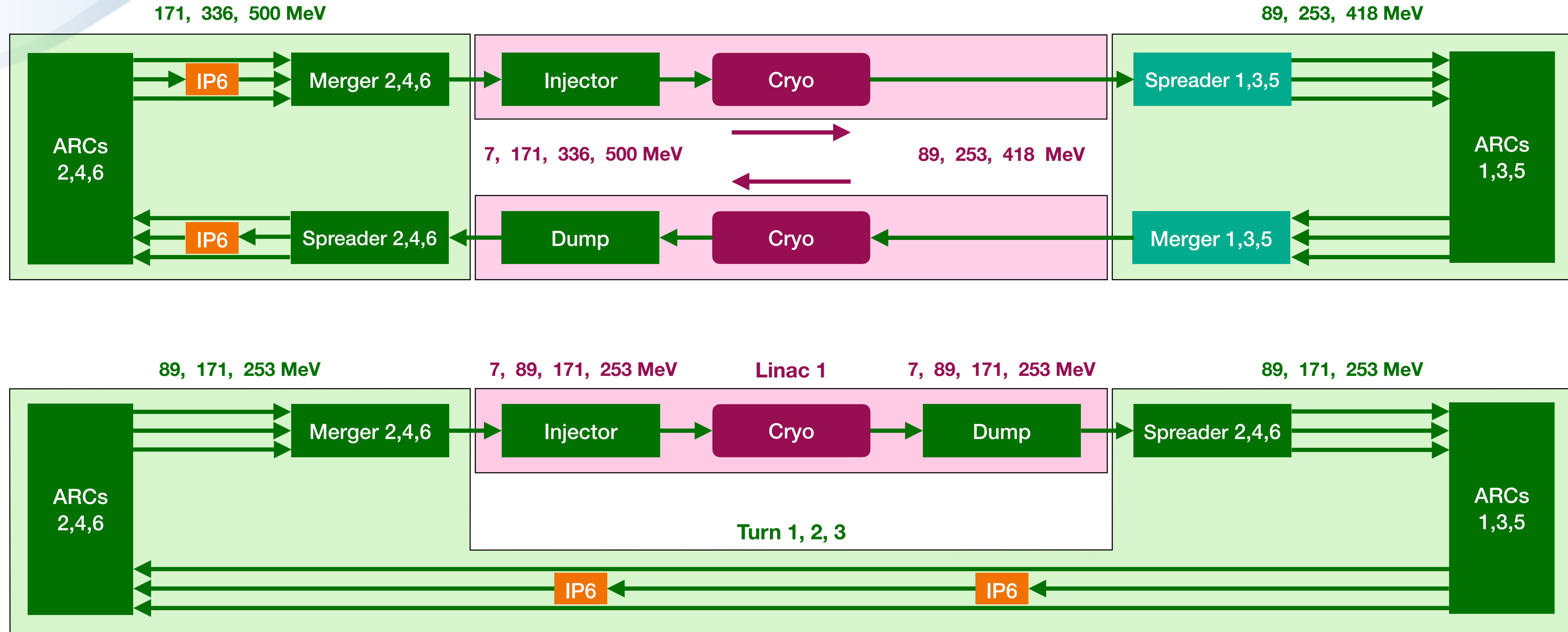
# Lattice design. 500 MeV vs 250 MeV versions



\* Flipping the lattice vertically → IP with access from the top



# Lattice design. 500 MeV vs 250 MeV versions



## 500 MeV (two cryo-modules)

- two common sections: Injector+Cryo and Cryo+Dump (~10m)
- two Spreader and two Merger sections

## 250 MeV (one cryo-module)

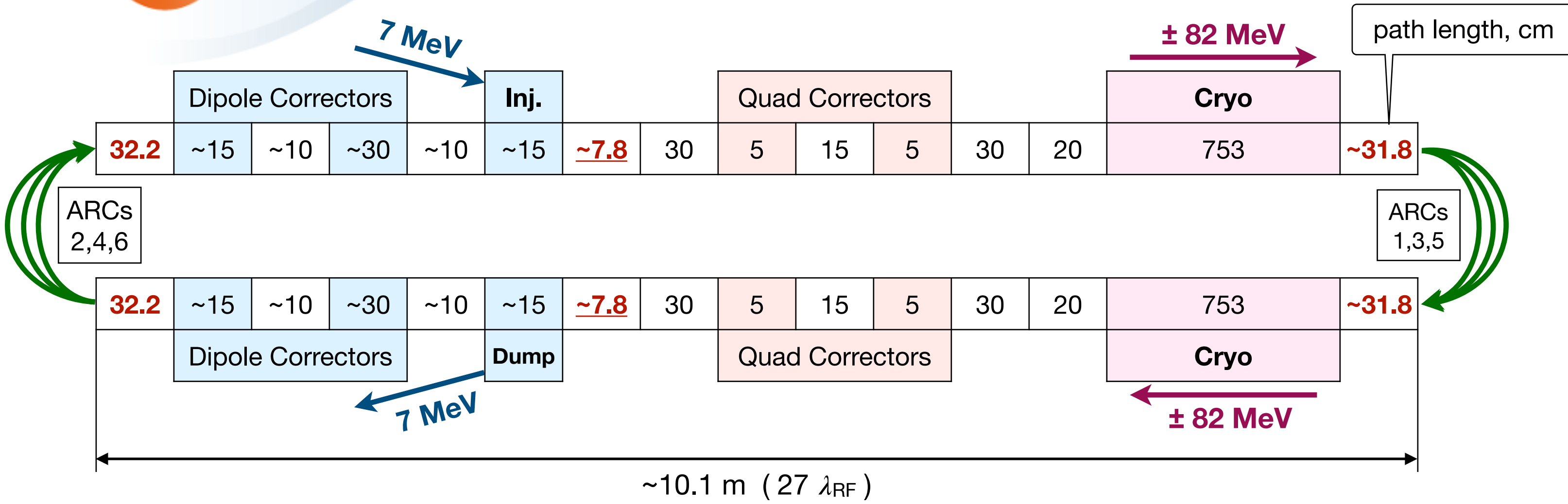
- one common sections: Injector+Cryo+Dump (~12m)
- one Spreader and one Merger section



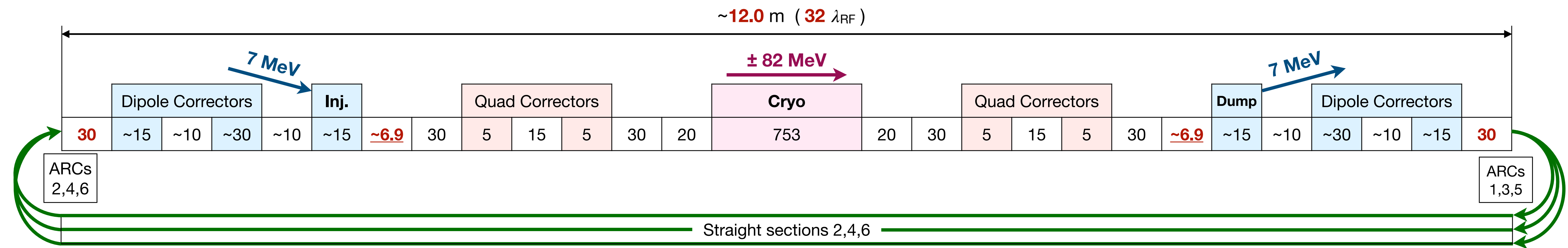
# Section(s) with common beam pipe



500 MeV → 250 MeV



- **Injection and Dump** are on the same side
- Drifts around **Dipole Correctors** shortened by **1-2 cm**
- Length of the straight section  $27\lambda \rightarrow 32\lambda$  ( $\lambda = 37.4$  cm)  
10.1 m → 12.0 m
- Can we move **Quad Correctors** to **Injection Line** ?  
- it can save up to 0.75 m (1.9 m) of the length  
- reduce the number of Quads by 2





# Spreader / Mergers

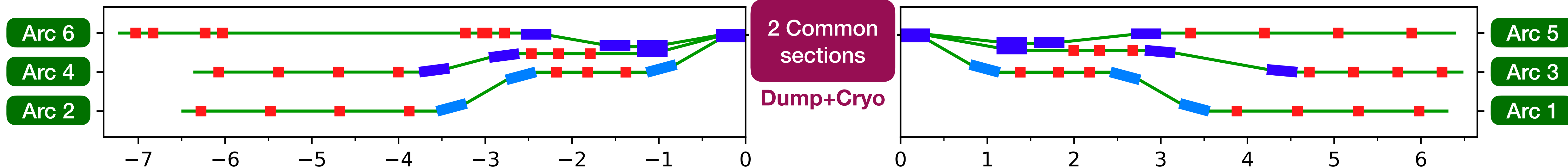


## 500 MeV

### Merger + Spreader

### Injection+Cryo

### Spreader + Merger

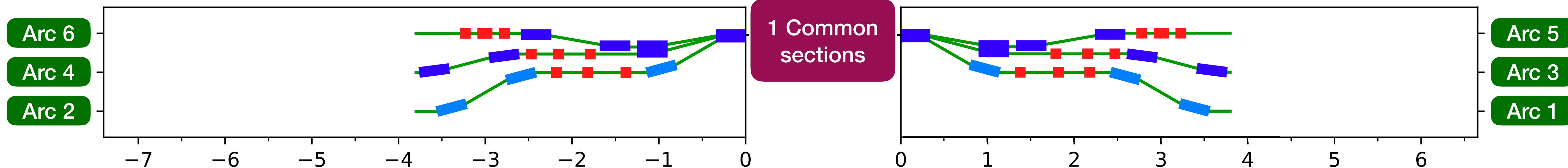


## 250 MeV

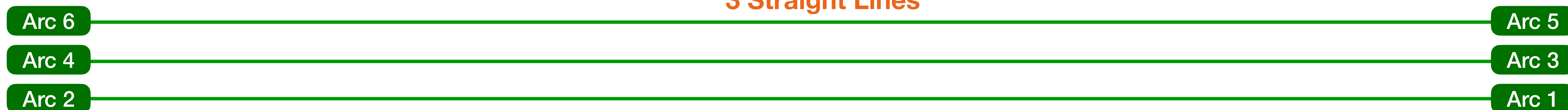
### Merger

### Injection+Cryo+Dump

### Spreader



### 3 Straight Lines





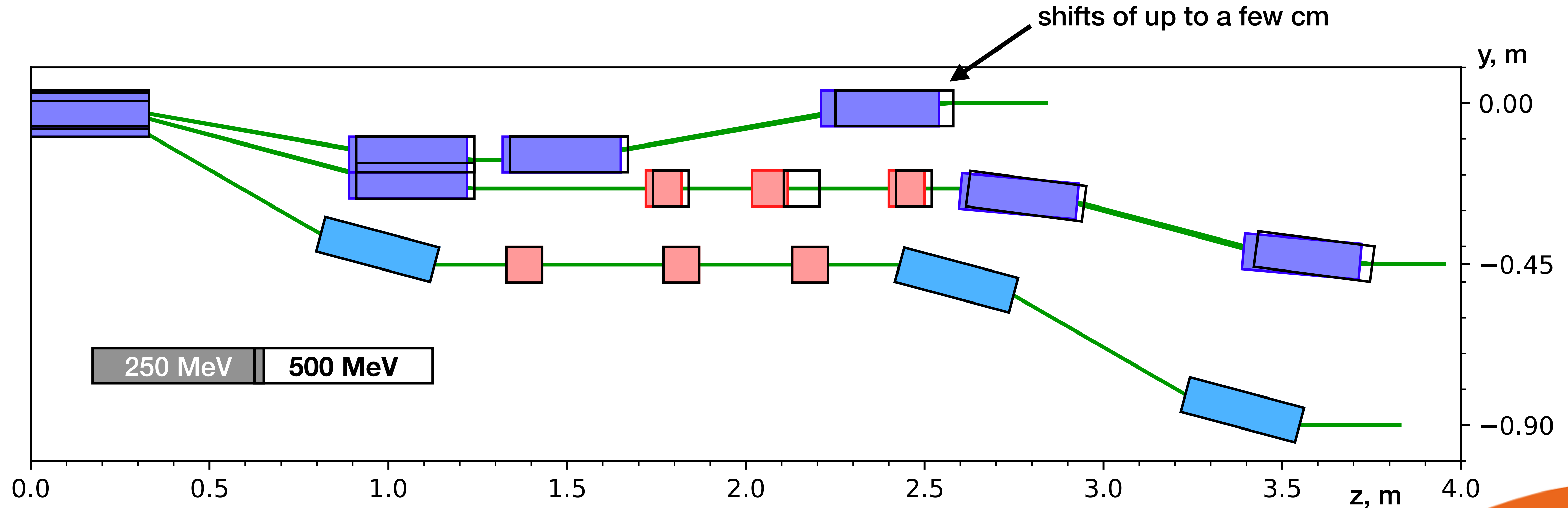
# Spreader / Mergers



The ratio of the energies in 250 MeV version is very close to the one in Arcs 2,4,6

→ we can use the same magnets, **but the lattice should be adjusted** (pipe lengths and tilts)

$$\Delta E + E_0 / 2\Delta E + E_0 / 3\Delta E + E_0 \approx 2\Delta E + E_0 / 4\Delta E + E_0 / 6\Delta E + E_0$$







# Filling pattern

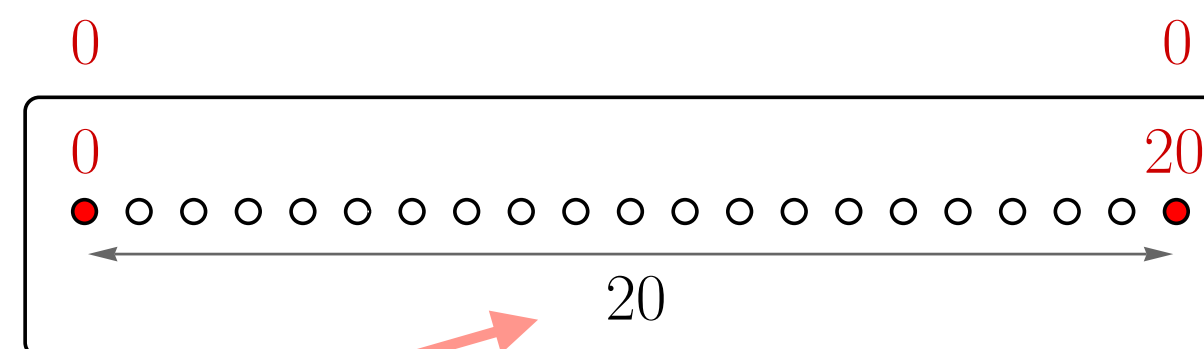
(size of the Arcs)



# Filling pattern



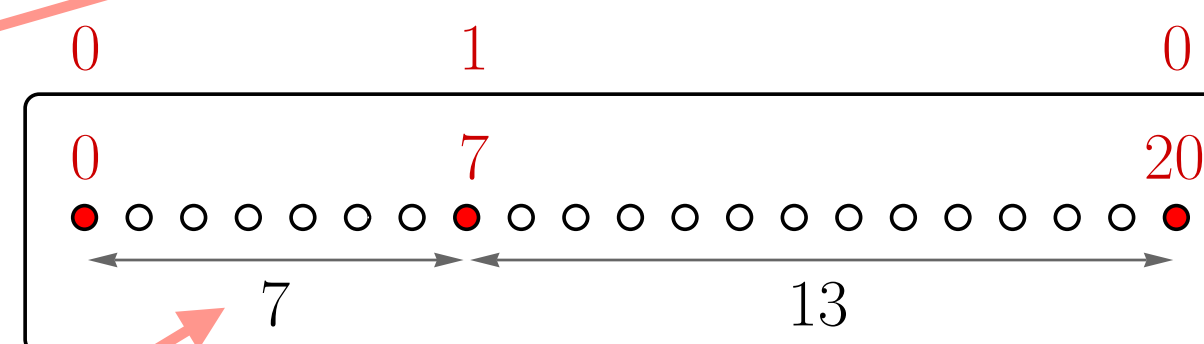
Consecutive injections ( $\nu_{inj} = 40$  MHz)



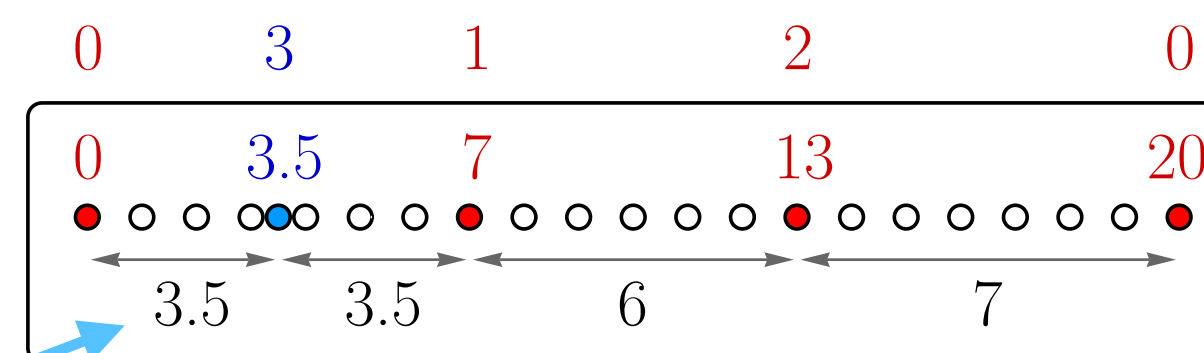
RF cavity ( $\nu_{RF} = 801.58$  MHz)

→ spacing between injections  $20 \times \lambda_{RF}$

$$\nu_{RF} / \nu_{inj} \approx 20, \lambda_{RF} = 34.7 \text{ cm}$$



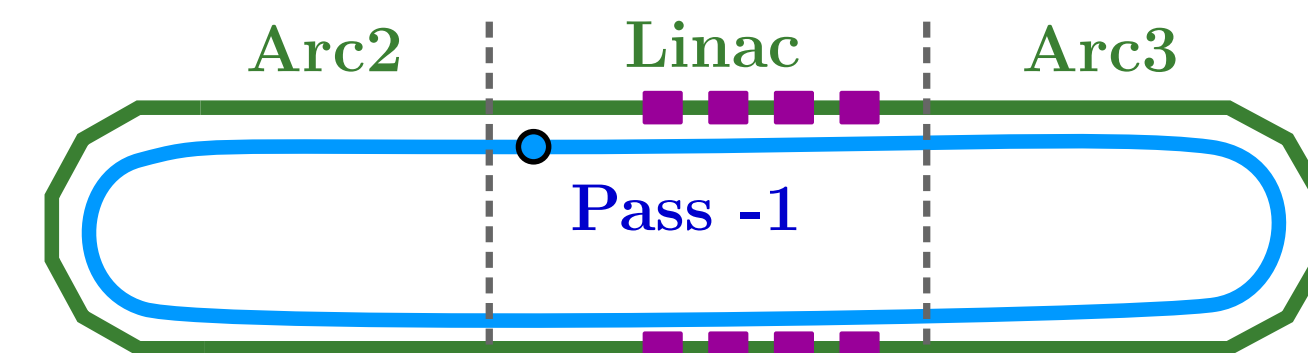
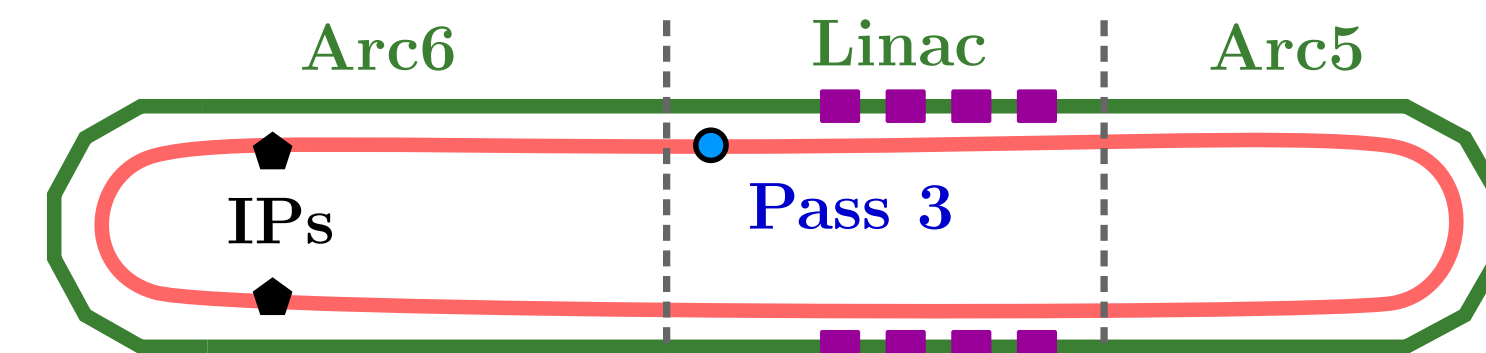
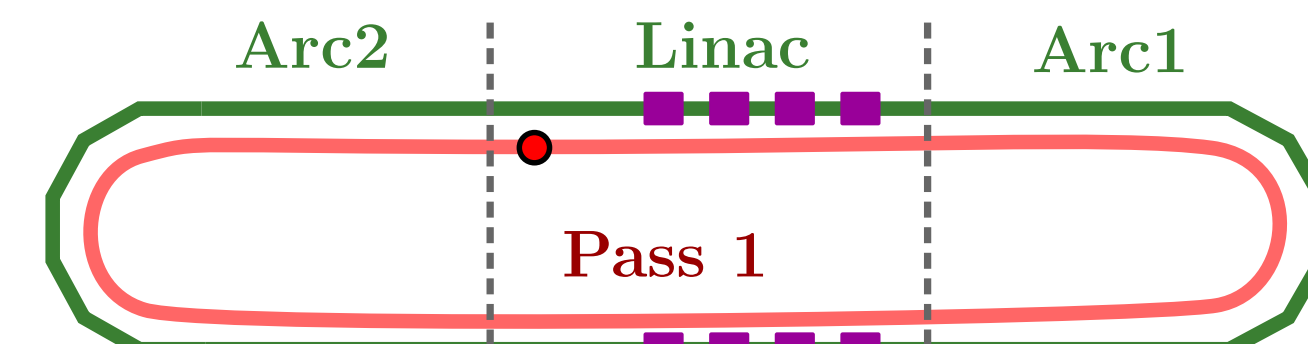
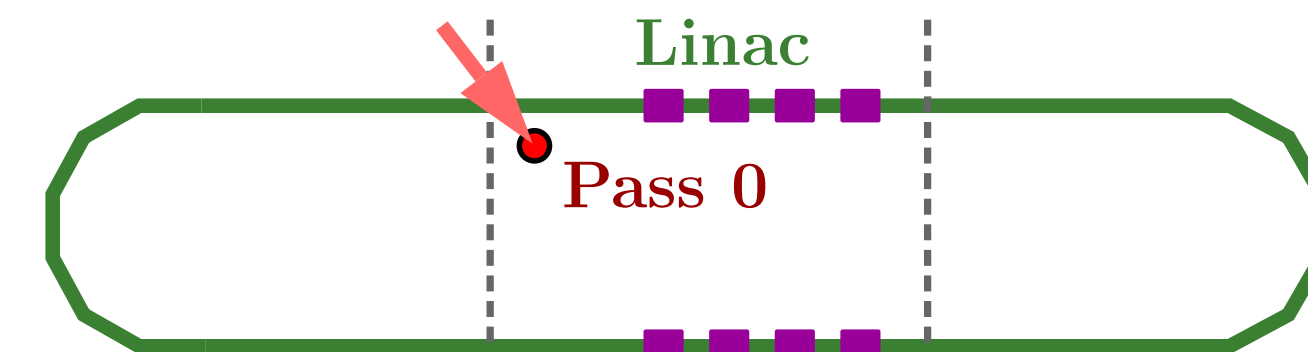
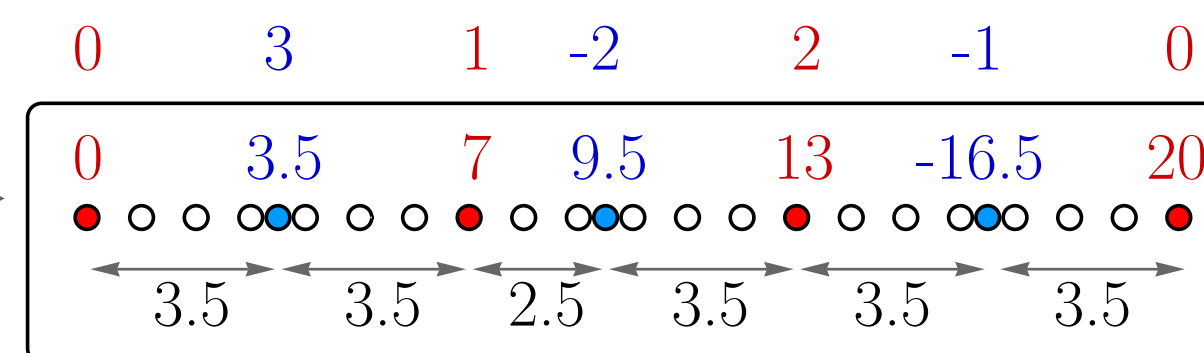
Pass length of first turn is  $20 \times n + 7$



Pass length of third turn is  $20 \times n + 7 + 3.5$

deceleration phase

After 6 turns → uniform bunch filling pattern



\* studies of Alex Bogacz, Peter Williams and Robert Apsimon



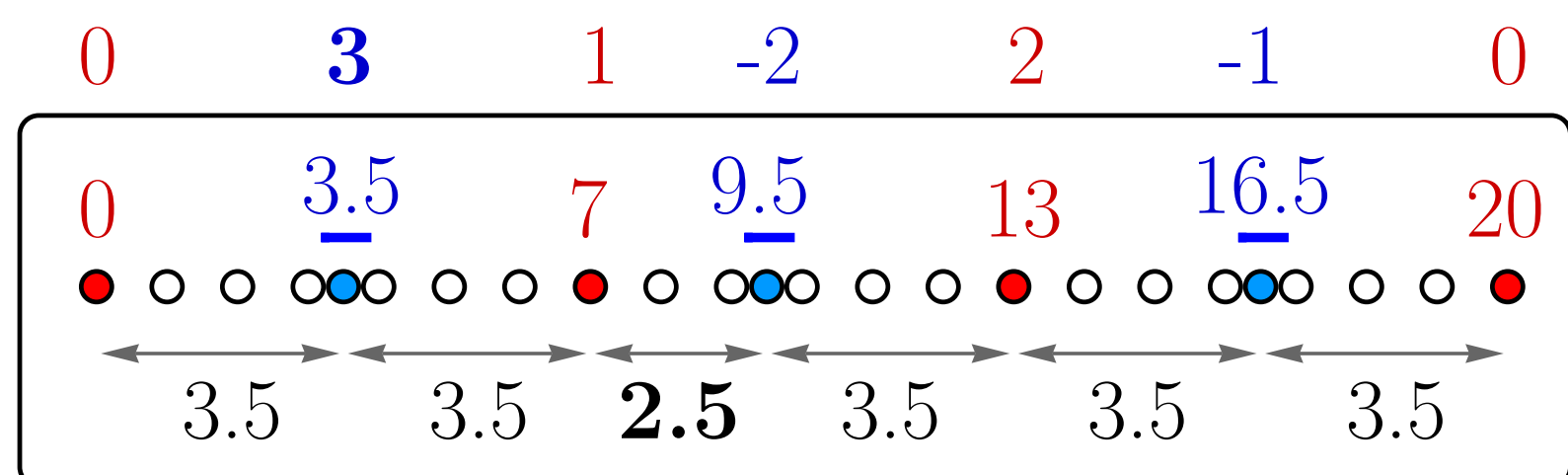
Adjusting the drifts lengths in spreader section → Match the filling pattern:

Linac section length  $27 \lambda_{RF}$  ( $32 \lambda_{RF}$  for 250 MeV)

Full length of one turn  $>160 \lambda_{RF}$  ( $<180 \lambda_{RF}$  for 250 MeV)  
( 2 Arcs + 2 Linacs )

Length of the Arc without a shift:

$$\frac{160 \lambda_{RF} - 2 \times 27 \lambda_{RF}}{2} = 53 \lambda_{RF}$$



| Arc |                               |  | Pass  |   |    |
|-----|-------------------------------|--|---|---|----|
| #   | Length<br>$L_A, \lambda_{RF}$ | Shift ( $L_A - 53$ )<br>$\Delta L_A, \lambda_{RF}$ | Shift ( $\Delta L_A + \Delta L_A$ )<br>$\Delta L_P, \lambda_{RF}$ | Position ( $\sum \Delta L_P$ )<br>$S, \lambda_{RF}$ | #  |
| 0   | 0                             | -  | -   | 0   | 0  |
| 1   | 57                            | 4  | 7   | 7   | 1  |
| 2   | 56                            | 3  |   |   |    |
| 3   | 57                            | 4  | 6   | 13  | 2  |
| 4   | 55                            | 2  |   |   |    |
| 5   | 57                            | 4  | 10.5  | 20 + 3.5  | 3  |
| 6   | 59.5                          | 6.5  |   |   |    |
| 5   | 57                            | 4  | 6   | 20 + 9.5  | -2 |
| 4   | 55                            | 2  |   |   |    |
| 3   | 57                            | 4  | 7   | 20 + 16.5   | -1 |
| 2   | 56                            | 3  |   |   |    |



# Filling pattern



## Chosen for 500 MeV

- shifts after each turn:  $\Delta = 7, 6, 10.5, 6, 7$   
 → 2.7 m free space at IPs  
 → total length 28.6 m

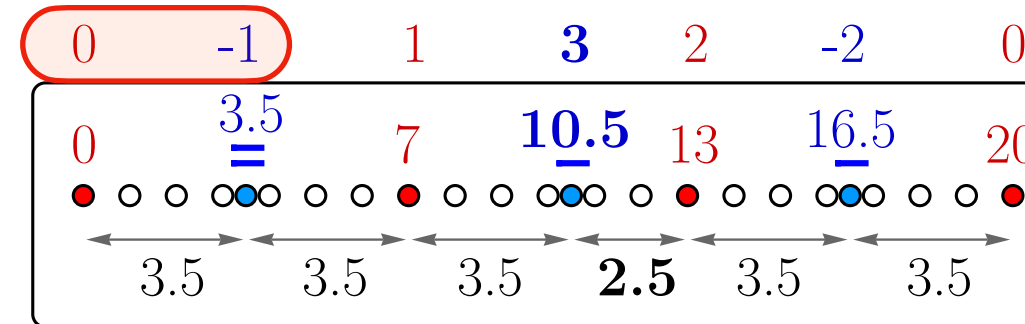
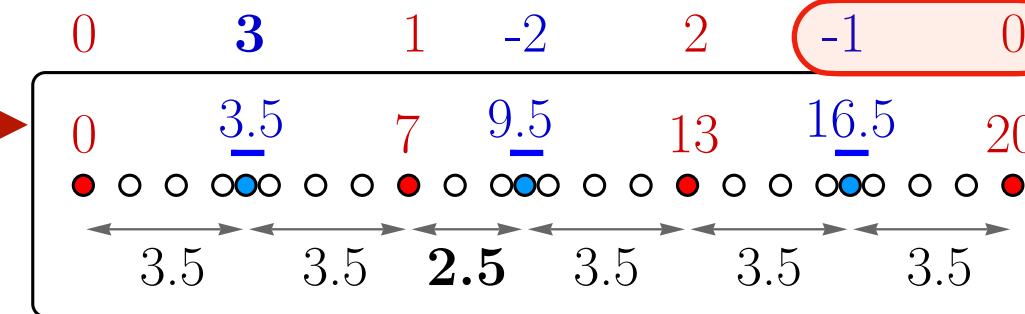
## Optimal filling pattern

- shifts after each turn:  $\Delta = 7, 7, 2.5, 7, 7$   
 → separation of lowest energies bunches  
 → more important for 250 MeV version

## Possible adjustments

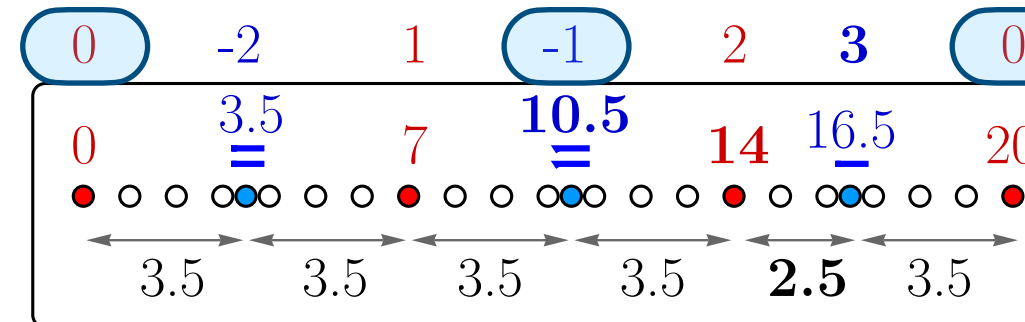
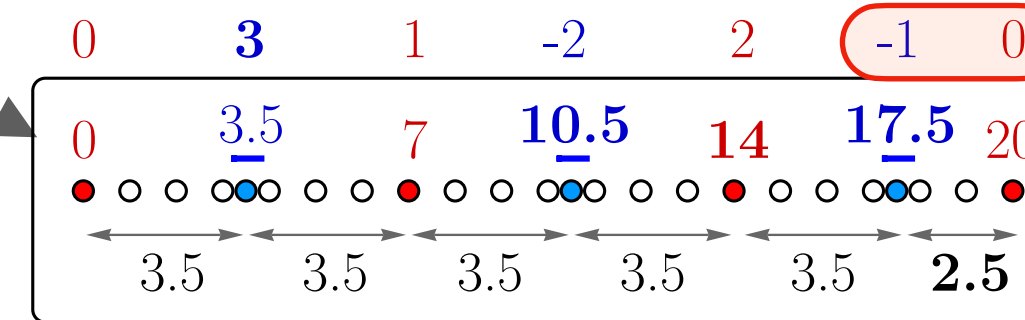
- the lengths of each even Arcs can be reduced by the same value as each of all odd Arcs increased (and vice versa)
- length of any Arc can be adjusted by integer number of 20 ( $\Delta \rightarrow \Delta \pm 20n$ )
- all shifts can be inverted ( $\Delta \rightarrow -\Delta$ )

|    |      |     |      |   |     |     |
|----|------|-----|------|---|-----|-----|
| A1 | 57   | 4   | 7    |   | 7   |     |
| A2 | 56   | 3   |      | 7 |     | +20 |
| A3 | 57   | 4   | 6    |   | 13  | +20 |
| A4 | 55   | 2   |      | 6 |     | 9.5 |
| A5 | 57   | 4   | 10.5 |   | 3.5 |     |
| A6 | 59.5 | 6.5 |      |   |     |     |



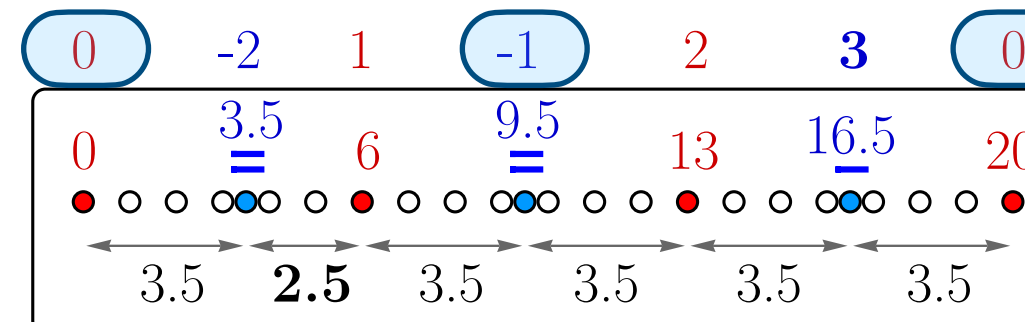
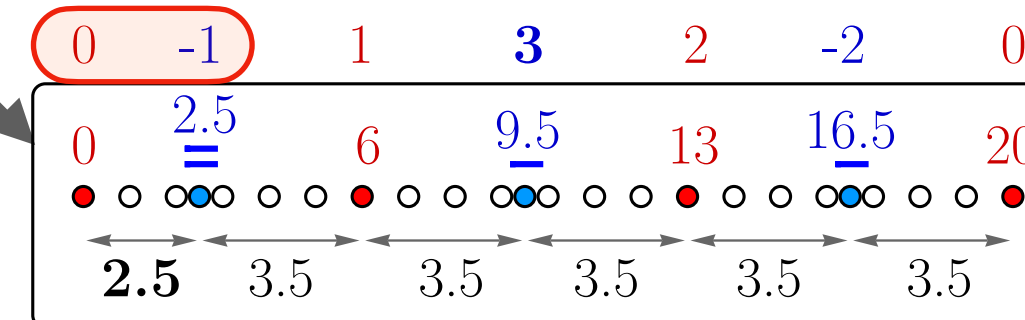
|    |      |      |      |   |      |      |
|----|------|------|------|---|------|------|
| A1 | 57   | 4    | 7    |   | 7    |      |
| A2 | 56   | 3    |      | 7 |      | +40  |
| A3 | 57   | 4    | 6    |   | 13   | +20  |
| A4 | 55   | 2    |      | 6 |      | 16.5 |
| A5 | 57   | 4    | 17.5 |   | 10.5 |      |
| A6 | 66.5 | 13.5 |      |   |      |      |

|    |      |     |     |   |     |      |
|----|------|-----|-----|---|-----|------|
| A1 | 57   | 4   | 7   |   | 7   |      |
| A2 | 56   | 3   |     | 7 |     | +20  |
| A3 | 57   | 4   | 7   |   | 14  | +20  |
| A4 | 56   | 3   |     | 7 |     | 10.5 |
| A5 | 57   | 4   | 9.5 |   | 3.5 |      |
| A6 | 58.5 | 5.5 |     |   |     |      |



|    |      |      |      |   |      |     |
|----|------|------|------|---|------|-----|
| A1 | 57   | 4    | 7    |   | 7    |     |
| A2 | 56   | 3    |      | 7 |      | +40 |
| A3 | 57   | 4    | 7    |   | 14   | +40 |
| A4 | 56   | 3    |      | 7 |      | 3.5 |
| A5 | 57   | 4    | 22.5 |   | 16.5 |     |
| A6 | 78.5 | 18.5 |      |   |      |     |

|    |      |      |      |   |     |      |
|----|------|------|------|---|-----|------|
| A1 | 57   | 4    | 6    |   | 6   |      |
| A2 | 55   | 2    |      | 6 |     | +40  |
| A3 | 57   | 4    | 7    |   | 13  | +20  |
| A4 | 56   | 3    |      | 7 |     | 16.5 |
| A5 | 57   | 4    | 16.5 |   | 9.5 |      |
| A6 | 72.5 | 12.5 |      |   |     |      |



|    |      |      |      |   |      |     |
|----|------|------|------|---|------|-----|
| A1 | 57   | 4    | 6    |   | 6    |     |
| A2 | 55   | 2    |      | 6 |      | +40 |
| A3 | 57   | 4    | 7    |   | 13   | +40 |
| A4 | 56   | 3    |      | 7 |      | 3.5 |
| A5 | 57   | 4    | 23.5 |   | 16.5 |     |
| A6 | 79.5 | 19.5 |      |   |      |     |



## 500 MeV

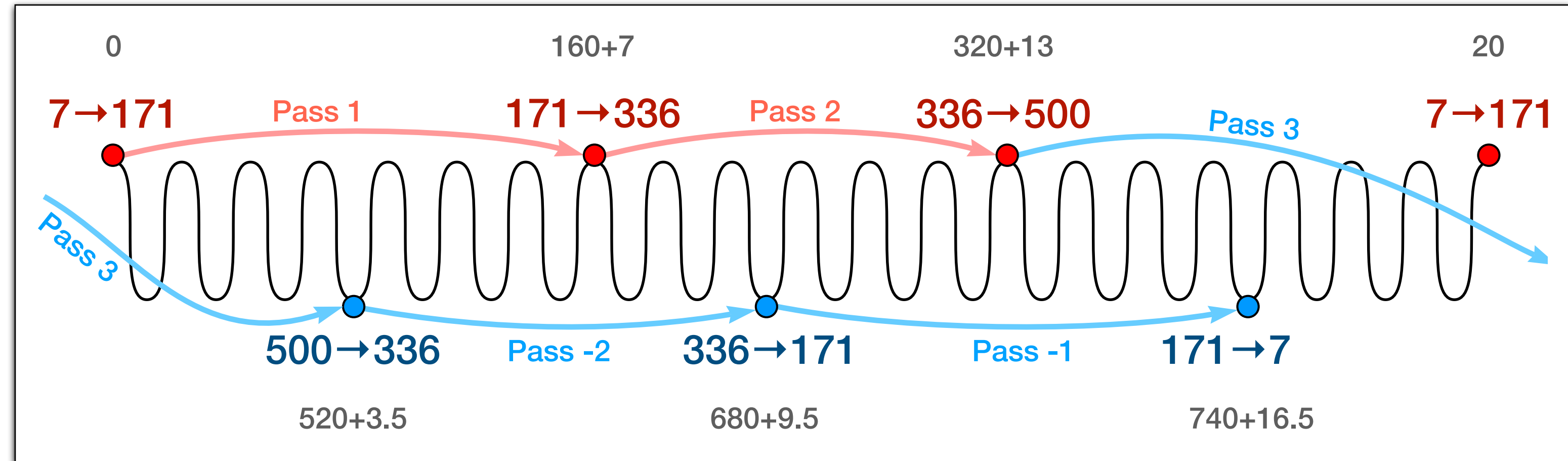
Full length of one turn:  $(160 + \Delta) \lambda_{RF}$

chosen shift:  $\Delta = 7, 6, 10.5, 6, 7$

→ 2.7 m at IPs (28.6 m total)

optimal shift

→ 4.7 m at IPs (30.6 m total)

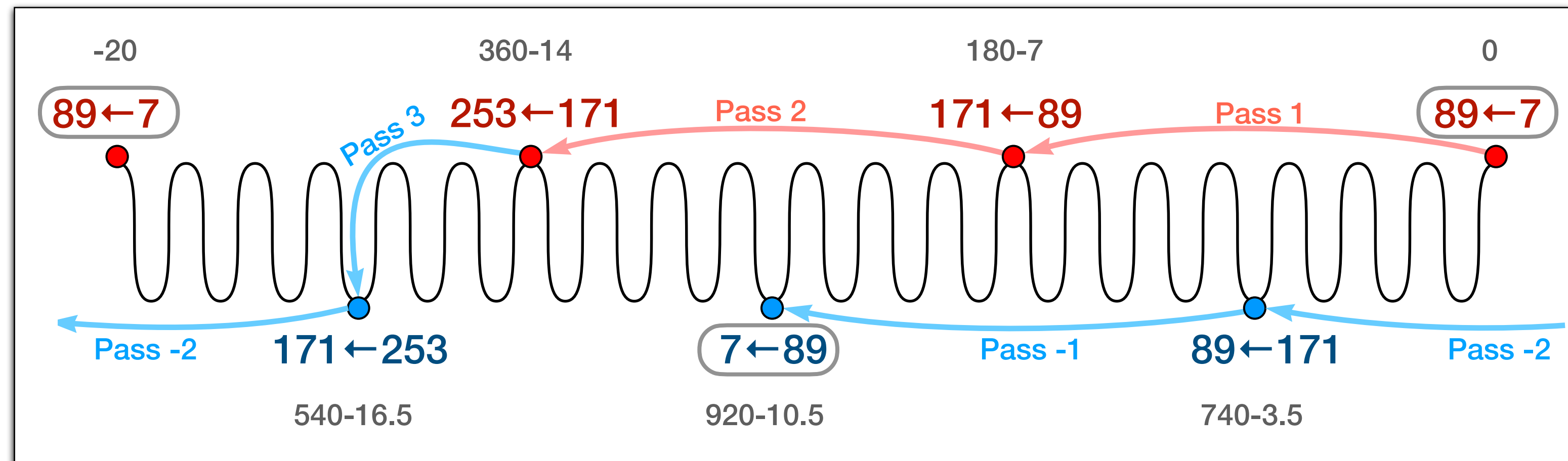


## 250 MeV

Full length of one turn:  $(180 - \Delta) \lambda_{RF}$

optimal shift:  $\Delta = 7, 7, 2.5, 7, 7$

→ bunches of lowest energies are separated  
(more important than for 500 MeV version)





# Optim6 → MadX



# Transition between Optim6 and MadX



Optim6 generates MadX sequence file with some errors, that have to be corrected:

**OptiM6** (all in vertical plane:  $TILT = \pi/2$ )

```
g1S01 B[kG]=-4.506411 Angle[deg]=0 EffLen[cm]=2
b1S01 L[cm]=34.55752 B[kG]=-4.506411 G[kG/cm]=0
G1S01 B[kG]=-4.506411 Angle[deg]=30 EffLen[cm]=3.849
```

**MadX (generated by OptiM6)**

```
b1S01: SBEND, L= 0.3455752, ANGLE=- $\pi/6$ , E1= 0, FINT =0.5, HGAP =0.02,
E2=- $\pi/6$ , FINTX=0.5, HGAPX=0.01039...;
```

**MadX (corrected)**

```
b1S01a: DIPEDGE, H=1.5151515, E1=0, FINT=0.5, HGAP=0.02;
b1S01b: SBEND, L=0.3455752, ANGLE=- $\pi/6$ ;
b1S01c: DIPEDGE, H=1.5151515, E1=- $\pi/6$ , FINT=0.5, HGAP=0.02;
```

**OptiM6**

```
A1 L[cm]=93.50048 Ncell=5 Eff_L[cm]=10
A[MeV]=20.54167 Phase[deg]=0 WaveL[cm]=37.4002
```

**MadX (generated by OptiM6)**

```
A1: LCAV, L= 0.9350048, DELTAE=20.54167, PHI0=0, FREQ=801580040.1;
```

**MadX (corrected)**

```
A1a: RFCAVITY, L=0.9350048, VOLT=20.54167, LAG=0,
FREQ=801580040.1;
```



# Transition between Optim6 and MadX



## Optim6

```
g1S01 B[kG]=-4.506411 Angle[deg]=0   EffLen[cm]=2
b1S01 L[cm]=34.55752  B[kG]=-4.506411 G[kG/cm]=0
G1S01 B[kG]=-4.506411 Angle[deg]=30  EffLen[cm]=3.849
```

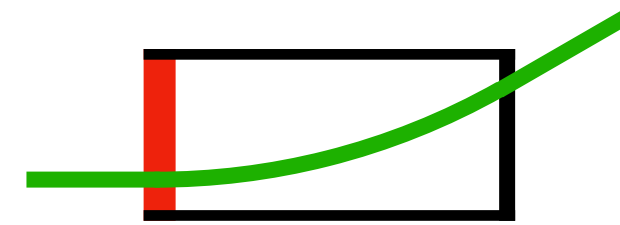
## MadX

```
b1S01a: DIPEDGE, H=1.5151515, E1=0,      FINT=0.5, HGAP=0.02;
b1S01b: SBEND,    L=0.3455752, ANGLE=-π/6;
b1S01c: DIPEDGE, H=1.5151515, E1=-π/6,  FINT=0.5, HGAP=0.02;
```

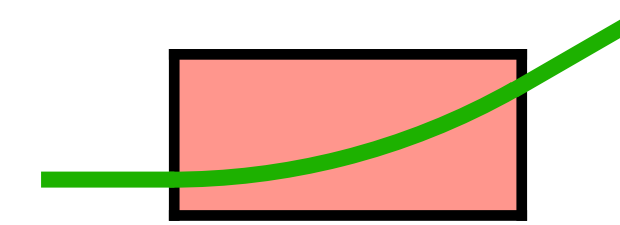
(all in vertical plane: TILT =  $\pi/2$ )

## Matching

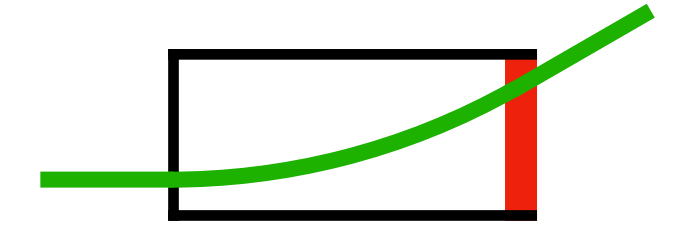
|                        | Place  | Inital            | Matched          |
|------------------------|--------|-------------------|------------------|
| Field gradient,<br>T/m | qq1s01 | -4.26551          | -4.265 <b>82</b> |
|                        | qq1s02 | 4.87074           | 4. <b>92812</b>  |
|                        | qq1s03 | -4.96549          | -4.96547         |
|                        | qq1s04 | -5.28356          | -5.28 <b>686</b> |
|                        | qq1s05 | 4.07249           | 4.07 <b>428</b>  |
| $\alpha_x$             | center | -0.0 <b>14401</b> | 0                |
| $\alpha_y$             | center | 0.000 <b>17</b>   | 0                |



|                 |   |   |   |   |   |
|-----------------|---|---|---|---|---|
| 1               |   |   |   |   |   |
| 0.0459 <b>1</b> | 1 |   |   |   |   |
|                 |   | 1 |   |   |   |
|                 |   |   | 1 |   |   |
|                 |   |   |   | 1 |   |
|                 |   |   |   |   | 1 |



|   |         |                  |         |   |                  |
|---|---------|------------------|---------|---|------------------|
| 1 | 0.34558 |                  |         |   |                  |
| 0 | 1       |                  |         |   |                  |
|   |         | 0.86603          | 0.33    |   | -0.08842         |
|   |         | -0.75758         | 0.86603 |   | -0.5000 <b>0</b> |
|   |         | -0.5000 <b>0</b> | 0.08842 | 1 | -0.01556         |
|   |         |                  |         |   | 1                |



|                 |   |         |   |   |   |
|-----------------|---|---------|---|---|---|
| 1               |   |         |   |   |   |
| -0.78 <b>64</b> | 1 |         |   |   |   |
|                 |   | 1       |   |   |   |
|                 |   | 0.87477 | 1 |   |   |
|                 |   |         |   | 1 |   |
|                 |   |         |   |   | 1 |

|                 |   |   |   |   |   |
|-----------------|---|---|---|---|---|
| 1               |   |   |   |   |   |
| 0.0459 <b>3</b> | 1 |   |   |   |   |
|                 |   | 1 |   |   |   |
|                 |   |   | 1 |   |   |
|                 |   |   |   | 1 |   |
|                 |   |   |   |   | 1 |

|   |         |                  |         |   |                  |
|---|---------|------------------|---------|---|------------------|
| 1 | 0.34558 |                  |         |   |                  |
| 0 | 1       |                  |         |   |                  |
|   |         | 0.86603          | 0.33    |   | -0.08842         |
|   |         | -0.75758         | 0.86603 |   | -0.5000 <b>1</b> |
|   |         | -0.5000 <b>1</b> | 0.08842 | 1 | -0.01556         |
|   |         |                  |         |   | 1                |

|                 |   |         |   |   |   |
|-----------------|---|---------|---|---|---|
| 1               |   |         |   |   |   |
| -0.78 <b>85</b> | 1 |         |   |   |   |
|                 |   | 1       |   |   |   |
|                 |   | 0.87477 | 1 |   |   |
|                 |   |         |   | 1 |   |
|                 |   |         |   |   | 1 |

The edge focusing of a dipole is not identical in two codes  
 With a small correction (~1%) of the filed gradient  
 in quadrupoles the lattice can be symmetrized





# Transition between Optim6 and MadX



## Optim6

```
g1S01 B[kG]=-4.506411 Angle[deg]=0   EffLen[cm]=2
b1S01 L[cm]=34.55752  B[kG]=-4.506411 G[kG/cm]=0
G1S01 B[kG]=-4.506411 Angle[deg]=30  EffLen[cm]=3.849
```

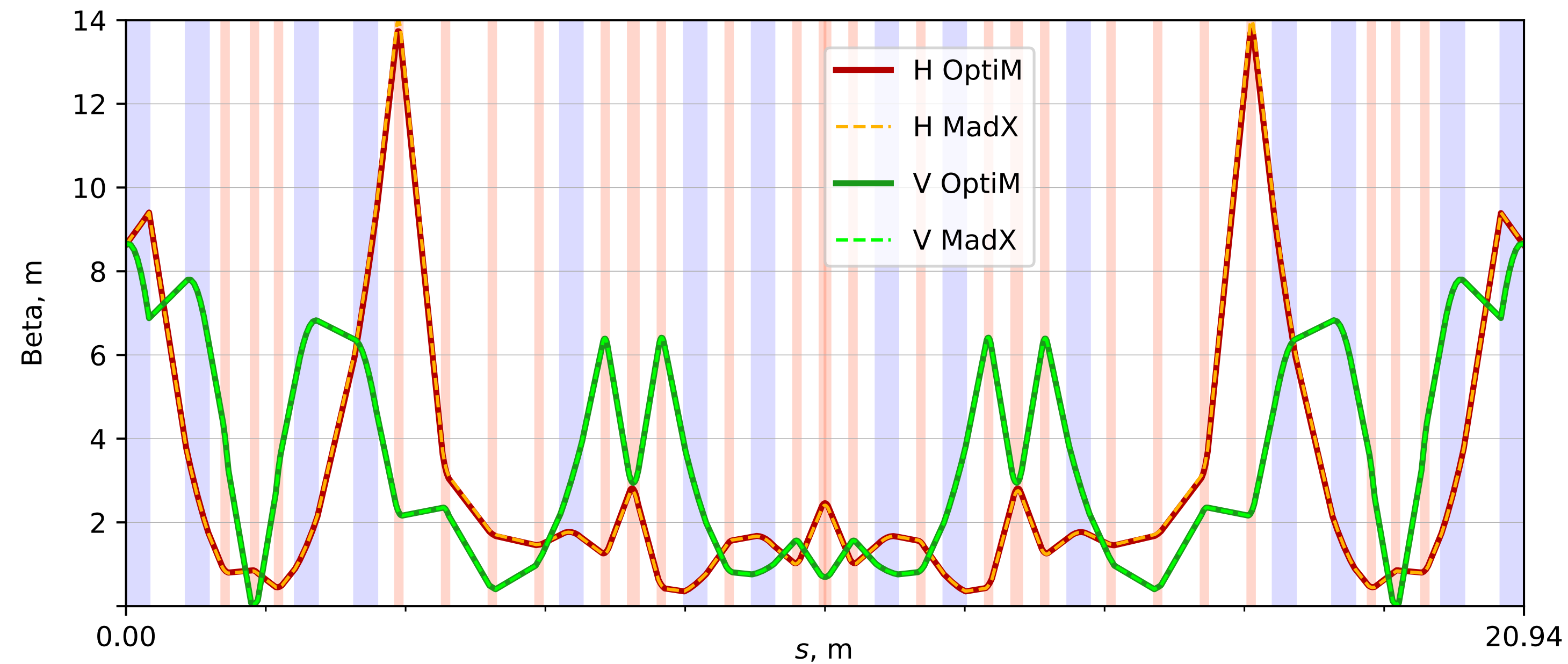
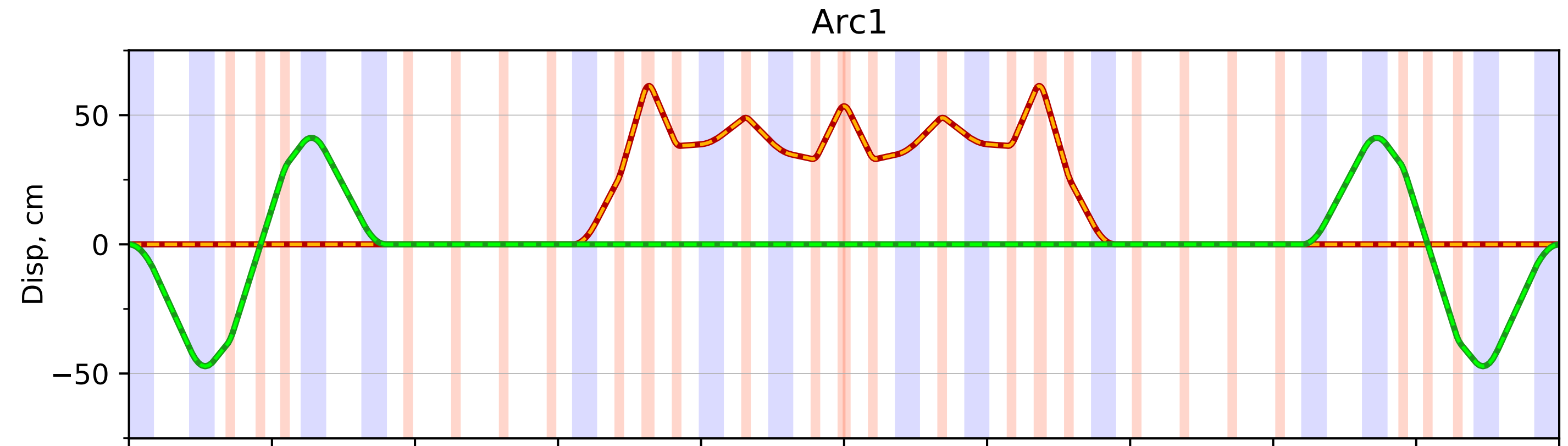
## MadX

(all in vertical plane: TILT =  $\pi/2$ )

```
b1S01a: DIPEDGE, H=1.5151515, E1=0,      FINT=0.5, HGAP=0.02;
b1S01b: SBEND,    L=0.3455752, ANGLE=- $\pi/6$ ;
b1S01c: DIPEDGE, H=1.5151515, E1=- $\pi/6$ ,  FINT=0.5, HGAP=0.02;
```

## Matching

|                        | Place  | Inital    | Matched  |
|------------------------|--------|-----------|----------|
| Field gradient,<br>T/m | qq1s01 | -4.26551  | -4.26582 |
|                        | qq1s02 | 4.87074   | 4.92812  |
|                        | qq1s03 | -4.96549  | -4.96547 |
|                        | qq1s04 | -5.28356  | -5.28686 |
|                        | qq1s05 | 4.07249   | 4.07428  |
| $\alpha_x$             | center | -0.014401 | 0        |
| $\alpha_y$             | center | 0.00017   | 0        |



also benchmarked with CODAL ( Coline Guyot )



## Lattice design of 250 MeV version of PERLE

- **compatible with the upgrade to 500 MeV version** ( the same elements used, only about 30 meters of extra beam pipes )
- **reduced immediate expenses** ( second cryo-module and 18 dipoles can be purchased later )
- **demonstration of ERL with 6 paths at high current** ( same as in 500 MeV version, but with half of the power )
- more space for experimental areas
- **additional expenses / manpower / shutdown time** ( rebuilding / recommissioning for the full power machine )

## Filling pattern (Arc optics architecture)

- the optimal filling pattern for 500 MeV version requires extra space ( 28.6 m → 30.6 m )  
but current configuration is fine ( Alex Bogacz, Peter Williams, Robert Apsimon )
- for the 250 MeV version we consider the optimal filling ( more essential at lower energies, inline with the optics )

## Benchmarking codes for lattice design and beam dynamics simulation

- small difference between Optim6 and MadX calculations of dipole fringe field effect ( ~1% correction of the quad field )
- longitudinal beam dynamic from 7MeV to 82MeV with field-map & calculation tool ( work of Coline Guyot )



500 MeV → 250 MeV ?



# Thank you



# Filling pattern



|         | Two Cryomodules (500 MeV) |  | One Cryomodule (253 MeV) |  | Filling Pattern |
|---------|---------------------------|--|--------------------------|--|-----------------|
| After   | E, MeV                    |  | E, MeV                   |  |                 |
| Pass 0  | 7                         |  | 7                        |  |                 |
| Pass 1  | 171                       |  | 89                       |  |                 |
| Pass 2  | 336                       |  | 171                      |  |                 |
| Pass 3  | 500                       |  | 253                      |  |                 |
| Pass -2 | 336                       |  | 171                      |  |                 |
| Pass -1 | 171                       |  | 89                       |  |                 |
| Dump    | 7                         |  | 7                        |  |                 |



## Dipoles and Quadrupoles names (in Arcs)

|   | Spreaders |       |        |        |         |         |         |     |        |        |        |        | Arcs |        |        |        |      |        |      |        |        |
|---|-----------|-------|--------|--------|---------|---------|---------|-----|--------|--------|--------|--------|------|--------|--------|--------|------|--------|------|--------|--------|
| 1 | b1S01     | b1S02 | qQ1S01 | qQ1S02 | qQ1S03  | b1S03   | b1S04   |     | qQ1S04 | qQ1S05 | qQ1S06 | qQ1S07 | bAA1 | qQ1A01 | qQ1A02 | qQ1A03 | bAA1 | qQ1A00 | bAA1 | qQ1A04 | qQ1A05 |
| 2 | .         | .     | .      | .      | .       | .       | .       |     | .      | .      | .      | .      | .    | .      | .      | .      | .    | .      | .    | .      | .      |
| 3 | .         | .     | .      | .      | .       | .       | .       |     | .      | .      | .      | .      | .    | .      | .      | .      | .    | .      | .    | .      | .      |
| 4 | b4S01     | b4S02 | qQ4S01 | qQ4S02 | qQ4S03  | b4S03   | b4S04   |     | qQ4S04 | qQ4S05 | qQ4S06 | qQ4S07 | bAA4 | qQ4A01 | qQ4A02 | qQ4A03 | bAA4 | qQ4A00 | bAA4 | qQ4A04 | qQ4A05 |
| 5 | b5S01     | b5S02 | b5S03  | b5S04  |         |         |         |     | qQ5S04 | qQ5S05 | qQ5S06 | qQ5S07 | bAA5 | qQ5A01 | qQ5A02 | qQ5A03 | bAA5 | qQ5A00 | bAA5 | qQ5A04 | qQ5A05 |
| 6 | b6S01     | b6S02 | b6S03  | b6S04  | qQ6S04A | qQ6S04B | qQ6S04C | iIR | qQ6S05 | qQ6S06 | qQ6S07 | qQ6S08 | bAA6 | qQ6A01 | qQ6A02 | qQ6A03 | bAA6 | qQ6A00 | bAA6 | qQ6A04 | qQ6A05 |

## Field, T and Field Gradient, T/m

|   | Spreaders |       |       |           |       |       |       |       |       |       |       |       | Arcs |       |      |       |      |      |      |       |      |
|---|-----------|-------|-------|-----------|-------|-------|-------|-------|-------|-------|-------|-------|------|-------|------|-------|------|------|------|-------|------|
|   | 10 cm     | 15 cm | 10 cm | Spreaders |       |       |       | 10 cm | 10 cm | 10 cm | Arcs  |       |      |       |      |       |      |      |      |       |      |
| 1 | -0.45     | 0.47  | -4.3  | 4.9       | -5.0  | -0.47 | 0.47  |       | 4.0   | -3.4  | -0.53 | -0.42 | 0.48 | -4.7  | 5.1  | -4.9  | 0.48 | 2.9  | 0.48 | -5.3  | 4.1  |
| 2 | -0.87     | 0.9   | -8.2  | 9.5       | -9.5  | -0.9  | 0.9   |       | 7.3   | -6.1  | -1.8  | 0.61  | 0.92 | -9.2  | 9.7  | -9.3  | 0.92 | 6.2  | 0.92 | -11.2 | 7.8  |
| 3 | -0.45     | 0.45  | -29.7 | 28.0      | -23.4 | -0.45 | 0.45  |       | -16.0 | 19.0  | -27.2 | 9.6   | 1.36 | -9.2  | 16.7 | -13.5 | 1.36 | 4.5  | 1.36 | -14.1 | 16.9 |
| 4 | -0.87     | 0.87  | -32.0 | 35.7      | -37.9 | -0.87 | 0.87  |       | -7.6  | 10.6  | -10.8 | 10.2  | 0.9  | -18.6 | 28.4 | -25.3 | 0.9  | 15.7 | 0.9  | -20.1 | 27.0 |
| 5 | -0.45     | 0.45  | 0.45  | -0.45     | 10 cm | 15 cm | 10 cm |       | -9.5  | 20.0  | -14.8 | 31.9  | 1.12 | -27.2 | 36.4 | -27.5 | 1.12 | 17.9 | 1.12 | -29.2 | 37.8 |
| 6 | -0.87     | 0.87  | 0.87  | -0.87     | -28.1 | 27.7  | -16.4 | iIR   | -54.9 | 44.4  | 30.9  | -46.2 | 1.34 | -32.6 | 43.0 | -32.5 | 1.34 | 21.2 | 1.34 | -34.1 | 44.1 |



# Beam size (in Arcs)

